

CORRECTIVE ACTION PLAN FINAL SUBMITTAL HUNTER ARMY AIRFIELD BUILDING 710 AREA CONTRACT DACA21-91-D-0001 JOB NO. 10675 CORRECTIVE ACTION PLAN
FINAL SUBMITTAL
HUNTER ARMY AIRFIELD
BUILDING 710 AREA
CONTRACT DACA21-91-D-0001
JOB NO. 10675

Corrective Action Plan Certification

I hereby certify that: this plan and all attachments have been prepared in accordance with EPD's "Requirements for Underground Storage Tank Release: Corrective Action Plan Content"; the information submitted is true, accurate and complete; and the plan satisfies all the criteria and requirements of Rule 391-3-15-.09 of the Georgia Rules for Underground Storage Tank Management.

Signature (Owner/Operator)

CORRECTIVE ACTION PLAN BUILDING NO. 710 AREA CONTRACT NO. DACA21-91-D-0001 JOB NO. 10675

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1.0 EXECUTIVE SUMMARY

In March, 1990, Tracer Research Corporation performed leak tests on two of four underground storage tanks (USTs) located at Building 710 at Hunter Army Airfield (HAAF) in Savannah, Georgia. These tests indicated that a 12,000-gallon diesel tank was leaking. Prior to the leak tests, a 10,000-gallon diesel tank was condemned in 1988 because it contained mud and water and thus was thought to be leaking. Based on this information, a preliminary contamination assessment (a shallow soil gas survey) was conducted by Tracer Research Corporation. Results of this investigation indicated that soils in the vicinity of the USTs had been impacted by the leak.

To further evaluate the vertical and horizontal extent of contamination, soil borings and monitor wells were installed and samples were collected by the U.S. Army Corps of Engineers (COE). Results of samples collected and observations made indicated that approximately 700 cubic yards of soil have possibly been highly contaminated and that phase separated product is floating on the groundwater surface. Also, dissolved hydrocarbons appear to be present in the groundwater.

Since contamination exists, a water system survey was conducted by Atlanta Testing & Engineering (AT&E) to determine required corrective action. In accordance with Rule 391-3-15-.09 of the Georgia Rules for UST Management, the extent of corrective action required is based on the location of the hydrocarbon plume with respect to nearby water withdrawal systems and surface water bodies. Based on this survey, it was determined that water withdrawal systems and surface water bodies exist within three miles of the site. However, the water withdrawal systems are all wells that receive water from aquifers other than the surficial aquifer and, therefore, are not hydraulically interconnected with the contaminant plume.

Based on these findings, it was proposed that the four USTs be removed. The contaminated soil plume will be excavated and phase separated product will be recovered during tank removal. Confirmatory soil samples will be collected and analyzed and one monitor well will be installed in the area of the former plume to evaluate the efficiency of the remedial action.

The nearest public withdrawal system within HAAF is less than 150 feet away from the contaminant plume. While this well is upgradient and not hydraulically interconnected with the contaminated plume, a confirmatory sample of the groundwater will be collected and analyzed.

Two lakes are located near the site. One lake is located just outside the HAAF's boundaries approximately 0.5 miles downgradient of the contaminated plume. The other lake is located within HAAF approximately 1,200 feet southwest and crossgradient of the contaminated plume. The dissolved hydrocarbon plume movement will be monitored to evaluate potential impacts to the water quality of the lake.

2.0 INTRODUCTION

2.1 FACILITY INFORMATION

The Corrective Action Plan (CAP) has been prepared in general accordance with Rule 391-3-15-.09 of the Georgia Rules for UST Management and "Requirements for Underground Storage Tank (UST) Release: CAP Content:" guidance document, dated July, 1991. The CAP will address the cleanup of subsurface impacts caused by leaking USTs containing diesel and gasoline at Building 710 at HAAF in Savannah, Georgia.

The subject facility and parties associated with the environmental activities being conducted at the site are presented below:

Location Name:

Building 710 Area

Location Address:

Hunter Army Airfield (HAAF) Savannah, Georgia 31409-5026

(912) 652-5675

Location County:

Chatham

Facility Contact:

Commander, 24th Infantry Division

(Mech) and Fort Stewart

Fort Stewart, Georgia 31314-5000

Directorate of Engineering and Housing (DEH),

Environmental Office (AFZP-DEV)

(912) 767-2010

Attention: Mr. Thomas D. Houston, Rep.

On-Site Environmental Consultant:

U. S. Army Corps of Engineers (COE)

Savannah District

100 W. Oglethorpe Avenue Savannah, Georgia 31402-0889

(912) 944-5675

Attention: Ms. Toni F. Nicholson

Environmental Report Consultant:

Atlanta Testing & Engineering (AT&E)

11420 Johns Creek Parkway Duluth, Georgia 30136

(404) 476-3555

Attention: Mr. Gregory R. Fischer, P.G.

Ga. Reg. No. 633

Signature

2.2 FACILITY DESCRIPTION

2.2.1 Location and Physiographic Setting

The Building 710 area, the project site, is located on the southeast corner of Douglas Street and the railroad crossing of HAAF in Savannah, Georgia. The location of HAAF is shown on Plate 1 and the site location within HAAF is shown on Plate 2 in Appendix A.

The project site is located in the Coastal Plain Province of Georgia near the coast and toward the northern end of the Barrier Island Sequence District. Area topography consists of step-like terraces with decreasing altitudes toward the Atlantic Ocean (Clark and Zisa, 1976). As shown on Plate 3, the land immediately surrounding the site is relatively flat, with elevation ranging from approximately 18 feet above mean sea level (msl) to 20 feet msl. Surface drainage across the site is directed to a storm drain located at the northwest corner of the site.

Surface water features in the area include small lakes, rivers and streams. Numerous small lakes are outside HAAF located in an area northwest of the site. The closest of these lakes is approximately 0.5 miles away. Hallstrom Lake is within HAAF and is located approximately 2.5 miles southeast of the project site. Salt Creek, a tributary of Little Ogeechee River is approximately 4 miles to the west and flows into the Little Ogeechee River to the south. Hayner's Creek, the headwaters to Vernon River, is located approximately 4 miles to the east and flows to the south.

2.2.2 Former Facility Operations

Building 710 formerly housed the base motor pool. The project site consisted of one building (710) for operators, four USTs and three pump islands. The USTs are approximately 45 years old and are constructed of steel. The two 10,000-gallon tanks which were installed around 1940, held diesel and gasoline and were managed by the 260th Quartermaster Battalion (QMBN). The two 12,000-gallon tanks, which were installed around 1941, held diesel and gasoline, and were managed by the Transportation Motor Pool. Plate 3 is a Site Plan showing the features described.

In 1988, the Directorate of DEH condemned and prohibited the use of the 260th QMBN (10,000-gallon) diesel tank because it contained a large quantity of mud and water. At this time, the 260th QMBN ceased using the other 10,000-gallon tank. The other two tanks were in operation until 1990, when it was determined that the 12,000-gallon diesel tank was leaking. At this time, the Transportation Motor Pool ceased using the other 12,000-gallon tank. Presently, the tanks are empty and the Transportation Motor Pool and the 260th QMBN are operating at other locations.

2.3 RELEASE CONFIRMATION AND INITIAL RESPONSE

As stated earlier, large amounts of mud and water were being pumped from the 10,000-gallon diesel tank in 1988. At this time, it was recommended by DFH that the two 10,000-gallon USTs be removed and that a site assessment be performed to determine the extent of contamination. It was also recommended that the two 12,000-gallon USTs be tested for leaks.

In March 1990, the COE retained the Tracer Research Corporation to perform the Tracer Tight TM Leak Test on the two 12,000-gallon USTs. The Tracer Tight method consists of introducing into the tank a very volatile tracer. Soil gas probes are then used to obtain vapor samples. If the tracer is detected, then the tank is considered to be leaking. Using this method it was determined that the 12,000-gallon diesel UST has a small or intermittent product leak of less than 0.05 gallons per hour. Hydrocarbons were also detected in the soil gas at concentrations ranging from 310,000 to 1,200,000 micrograms per liter (μ g/l). A more detailed description of the methodology used and the Tracer Tight TM Leak Test Report are included in Appendix C-1.

Based on the results of the Tracer Tight TM Leak Test and observations made in 1988, a shallow soil gas survey was conducted by Tracer Research Corporation in July, 1990, to determine the extent of contamination. In summary, 11 soil gas probes were used to collect soil gas samples in the vicinity of Building 710 and the tank pit. Samples were analyzed for benzene, toluene, ethylbenzene, and xylenes (BTEX) and total hydrocarbon. All samples collected had elevated concentrations that ranged from 4.2 to 5,500 μg/l total BTEX and 9 to 180,000 μg/l total hydrocarbons. Based upon these findings, it was determined that the hydrocarbon plume extended at least 100 feet in all directions from the northwest corner of Building 710. The Shallow Soil Gas Investigation Report is included in Appendix C-2.

Based on the results of the soil gas survey, soil borings and monitor wells were placed to further assess the vertical and horizontal extent of contamination. The contamination assessment methodology and findings are discussed in Sections 3.0 through 5.0.

2.4 PURPOSE AND SCOPE

Based on the results of the soil gas survey, the objective of the environmental program is to complete the following objectives:

- ♦ Remove the source of contamination;
- Assess the vertical and horizontal extent of hydrocarbon contamination in the soils adjacent to the pump island and petroleum USTs;
- Assess potential hydrocarbon impact to groundwater in the vicinity of the USTs;
 and
- Prepare a CAP as required by the Environmental Protection Division (EPD).

The work scope required to meet the environmental program objectives consists of the following principal components:

- ♦ UST removal:
- Installation of Soil Borings and Monitoring Wells;
- ♦ Elevation Survey/Liquid Level Measurements;

- ♦ Area and Site Hydrogeology Evaluation;
- ♦ Area Groundwater Utilization Evaluation;
- ♦ Soil and Groundwater Quality Analysis; and
- ♦ Removal of Contaminated Soil and Liquid Hydrocarbons.

Data gathering activities such as the installation of soil borings and monitor wells, the collection of liquid level measurements and laboratory analytical results are discussed in Section 3.0. Area and site hydrogeology and groundwater utilization are discussed in Section 4.0. The extent of contamination based on analytical results and aquifer properties is discussed in Section 5.0 and the CAP and its requirements are discussed in Sections 6 through 10.

2.5 SEQUENCE OF ENVIRONMENTAL INVESTIGATIONS

The following is a list of work completed.

<u>Date</u>	Work Completed
Dec. 1989	Completed auger boring (Boring T-1 (A-3) next to tanks to be leak tested using the Tracer (vapor monitoring) Method. Purpose of this boring was to determine if soil in backfill zone were sufficiently porous to allow this type of leak detection method to work. The drilling log and Hazardous and Toxic Waste (HTW) Log for Boring T-3 (A-3) are in Appendix C-3.
March 1990	- Tanks leak tested by Tracer Research Corporation. Report completed and included in Appendix C-1.
July 1990	Shallow Soil Gas Investigation conducted by Tracer Research Corporation. Report completed and included in Appendix C-2.
March 1991	- Completed topographic survey of site by Savannah District COE.
May 1991	Installed monitor wells MW-1, MW-3 through MW-6, MW-10 and MW-11 and drilled soil borings A-1 through A-7 and A-9 through A-11. Collected soil and groundwater samples to be analyzed by EPA Methods 8020 or 602, 418.1 and for lead. Conducted headspace tests on soils with organic vapor analyzer (OVA).
August 1991	The COE retained AT&E under A-E Contract No. DACA21-91-D-0001 to prepare a Corrective Action Plan.

3.0 METHODS OF INVESTIGATION AND STATEMENT OF RESULTS

3.1 DRILLING AND WELL INSTALLATION

To further assess the vertical and horizontal extent of hydrocarbon contamination in the soils and the potential impact to groundwater, soil borings and monitor wells were installed in the vicinity of the USTs. The following sections discuss the installation of soil borings (Section 3.1.1) and monitor wells (3.1.3) as well as the screening of soil for organic vapors during these installations (3.1.2).

3.1.1 Soil Borings

From May 1 through 14, 1991, 19 soil borings (MW-1, MW-3 through MW-8, MW-10, MW-11, A-1 through A-7, and A-9 through A-11) were installed at the site by the COE. Nine of these borings (MW-1, MW-3 through MW-8, MW-10 and MW-11) were completed as monitor wells. Soil boring and monitor well locations are shown on Plate 4. Soil boring construction data are summarized in Table 1 in Appendix B. Details regarding boring/well construction and soil descriptions are included in the drilling logs in Appendix D-1.

All borings were installed using 3.5 inch diameter hand augers. Borings MW-1, MW-3 through MW-8, MW-10, MW-11 and A-11 were extended further with a drill rig using 4.25 inch inner diameter hollow stem augers. Boring depths ranged from 5 feet below land surface (fbls) in A-2 and A-3 to 12.5 fbls in MW-4 with an average depth of 8.2 fbls. Initial water level depths ranged from 3.10 fbls in MW-5 to 6.41 in A-4 with an average depth of 4.28 fbls. Water levels after 24 hours ranged from 2.15 fbls in A-9 to 4.40 fbls in A-5 with an average depth of 3.58 fbls. Locations of the borings were surveyed by the COE for horizontal and vertical control. Land surface elevations ranged from 18.08 feet msl at A-9 and A-11 to 21.05 feet msl at MW-6 with an average elevation of 18.93 feet msl across the site.

3.1.2 Soil Organic Vapor Screening, Headspace Analysis

In order to preliminarily assess potential hydrocarbon impacts to soil, soil samples were collected during drilling and screened in the field for organic vapors. Soil samples were collected with a hand auger from land surface to a few feet below the water's surface at approximately 1-foot centers. Samples were then placed in a jar, filling it half full. A sheet of aluminum foil was placed over the jar before closing the jar lid. This foil was later pierced with the OVA probe to take a headspace reading.

Results of the headspace analyses are presented in the HTW Boring Logs in Appendix D-2 and summarized in Table 2. As shown on Table 2, maximum organic vapor concentrations of greater than 1000 parts per million (ppm) were detected in Borings MW-1, MW-4, MW-7, MW-8, A-5 and A-6, between 150 ppm and 740 in MW-11, A-1, A-4, A-11; and between 0 ppm to 25 ppm in MW-3, MW-5, MW-6, MW-10, A-2, A-7, A-9, A-10, in at least one sample interval.

3.1.3 Well Installation

As mentioned in Section 3.1.1, nine soil borings (MW-1, MW-3 through MW-8, MW-10 and MW-11) were completed as monitor wells. All monitor wells consist of 2-inch diameter PVC casings and screens, are finished below grade and protected by manhole structures. Monitor Wells MW-1 and MW-3 consist

of 4 feet of 0.010-inch slotted screen, MW-4 consists of 9 feet of 0.010-inch slotted screen, and Monitor Wells MW-5 through MW-8, MW-10 and MW-11 consist of 6.75 feet of 0.010-inch slotted screen. Screens were placed to bracket the liquid interface. Sand filter packs were placed in the annulus space from the bottom of the wells to approximately 1 foot above the top of the screen, then sealed with approximately 0.5 feet of bentonite in all wells. Remaining annulus space was then filled with concrete. Well locations were surveyed by the COE for horizontal and vertical control. Well construction details are presented in Appendix D-1 and summarized on Table 3.

3.2 LIQUID LEVEL MEASUREMENTS

To evaluate the presence of phase separated product and the direction of groundwater flow, liquid level measurements were taken by the COE on August 29, 1991. Water level measurements were taken with an electric tape and the presence of phase separated product was visually checked by collecting a sample at the liquid interface with a clear bailer.

Depth to water ranged from 2.31 feet below top of casing (BTOC) in MW-11 to 3.86 feet BTOC in MW-1 with an average depth of 3.04 feet BTOC. Phase separated product was observed in one well (MW-1) at a thickness of 0.61 feet. A summary of fluid level measurements is presented in Table 4.

3.3 HYDRAULIC CONDUCTIVITY TESTS

To evaluate the surficial aquifer's ability to horizontally transmit water, hydraulic conductivity of the soil is required. The hydraulic conductivity is expressed as the volume of water that will move in unit time under a unit hydraulic gradient through a unit area measured at right angles to the direction of flow (Heath, 1987).

To calculate the hydraulic conductivity, the COE conducted slug tests on September 5, 1991 in seven monitor wells (MW-1, MW-4 through MW-8, and MW-11). The methodology used, calculations and results of these tests are described in detail in Appendix E. The values of hydraulic conductivity calculated ranged from 0.9×10^{-3} feet per minute (fpm) in MW-11 to 3.1×10^{-3} fpm in MW-5 and averaged 1.9×10^{-3} fpm. The hydraulic conductivity data is summarized in Table 5.

3.4 ENVIRONMENTAL SAMPLING AND ANALYSIS

To quantitatively evaluate hydrocarbon impact to the soil and groundwater, selected soil samples and a groundwater sample from each well were analyzed for gasoline constituents - BTEX, TPH and in some cases lead, by Savannah Laboratories and Environmental Services, Inc. of Savannah, Georgia. Soil and groundwater samples were shipped to the laboratory with proper chain of custody documentation. Laboratory analytical reports and chain of custody documentation are included in Appendix F.

3.4.1 Soils

Selected soil samples collected during drilling were analyzed for BTEX and TPH by EPA Methods 8020 and 418.1, respectively. Soil samples MW-710-1-1, MW-710-3-1, MW-710-4-1, MW-710-6-1, and A-5-1 were also analyzed for lead. Soil Sample A-5-1 was analyzed on two separate occasions. The second A-5-1 soil sample was obtained by drilling next to the original A-5 boring with a hand auger. The intent

was to collect a soil sample for lead analysis only. A summary of soil quality data including date of sample collection, sample interval, OVA readings, and quantitative results are presented in Table 6.

Total BTEX concentrations ranged from below detection limits in samples MW-710-3-1, MW-710-5-1, MW-7-1-C, MW-10-1, MW-11-1, A-1-1, A-2-1, A-3-1, A-4-1, A-4-2, A-5-1, A-7-1, A-8-1, A-10-1, MW-9-1, and MW-9-2 to 8,050 ppm in MW-710-1-1. Of the seven remaining samples, only MW-710-2-1 had a total BTEX concentration (10.9 ppm) that exceeded 10 ppm.

TPH concentrations ranged from below detection limits in A-2-1 to 25,000 ppm in MW-710-1-1. TPH concentrations in MW-7-1 (990 ppm) and MW-710-2-1 (1,400 ppm) exceeded 500 ppm and TPH concentrations in MW-8-1 (310 ppm) exceeded 100 ppm. In the remaining 19 samples, TPH concentrations ranged from 12 ppm in A-4-1 to 64 ppm in MW-10-1.

Five soil samples were analyzed for lead. Lead concentrations range from 3.4 ppm in MW-710-3-1 to 18 ppm in A-5-1.

3.4.2 Groundwater

On May 29, 1991, groundwater samples were collected from all nine monitor wells and analyzed for BTEX and TPH by EPA Methods 602 and 418.1, respectively. A duplicate sample (MW-7-1C) was also collected from MW-7. Groundwater samples MW-1-1, MW-4-1, and MW-6-1 were also analyzed for lead. A summary of groundwater quality data is presented in Table 7.

Benzene concentrations ranged from below detection limits in MW-5-1, MW-6-1, MW-7-1, MW-7-1C, and MW-10-1 to 5,200 parts per billion (ppb) in MW-1-1. In the remaining four samples, benzene concentrations ranged from 9.2 ppb in MW-11-1 to 600 ppb in MW-4-1.

Total BTEX concentrations ranged from below detection limits in MW-5-1, MW-7-1, MW-7-1C, and MW-10-1 to 48,000 ppb in MW-1-1. In the remaining five samples, total BTEX concentrations ranged from 1.5 ppb in MW-6-1 to 801.8 ppb in MW-4-1.

TPH concentrations ranged from below detection limits in Samples MW-3-1, MW-4-1, MW-5-1, MW-6-1, MW-7-1C, MW-10-1, and MW-11-1 to 55 ppm in MW-1-1. Of the remaining two samples, TPH concentrations were less than 3.0 ppm.

Three groundwater samples were analyzed for lead. Lead concentrations ranged from below detection limits in MW-4-1 and MW-6-1 to 0.038 ppm in MW-1-1.

4.0 REGIONAL AND SITE HYDROGEOLOGY

4.1 REGIONAL HYDROGEOLOGY

4.1.1 Geology

This site is located in the Coastal Plain of Georgia and is approximately 18 miles west of the Atlantic Coast. Geologic formations underlying the coastal plain in this area consist of unconsolidated sand and clay, limestone and dolomite, and were deposited during the Late Cretaceous Period to the Quaternary Period (Holocene Epoch). A generalized hydrogeologic stratigraphic column is presented in Plate 5. A general discussion of the units is presented below.

4.1.1.1 Undifferentiated Surficial Sand

The undifferentiated surficial sand of late to Pleistocene to Holocene age occurs at the top of local geologic features and underlies local soil profiles. These deposits consist of massive-bedded, structureless, well to moderately-sorted, fine- to medium-grained, white to buff colored sand and range in thickness of 0 to 10 feet (Huddlestun, 1988).

4.1.1.2 Undifferentiated Alluvial Deposits

The undifferentiated alluvial deposits of Pleistocene age occur throughout the drainage systems of the Coastal Plain and consist of modern floodplain deposits and river terrace deposits. These deposits are predominantly sand with a little clay and range in thickness of 20 to 50 feet (Huddlestun, 1988).

4.1.1.3 Cypresshead Formation

The undifferentiated surficial sands and alluvial deposits are underlain by the Cypresshead Formation of early Pleistocene age. The Cypresshead Formation generally consists of quartz sand with prominent clay beds in some down dip areas. Two lithofacies are dominant in this unit. The up dip facies generally consist of fine- to coarse-grained well to poorly sorted sand with scattered gravel stringers. The down dip facies generally consist of fine-grained, well sorted sand with thin layers of clay. The Cypresshead Formation disconformably overlies the Coosawhatchie Formation of the Hawthorn Group (Huddlestun, 1987).

4.1.1.4 Hawthorn Group

The Cypresshead Formation is underlain by the Hawthorn Group of Miocene age. The Hawthorn Group generally consists of a basal calcareous unit, a middle clastic unit, and an upper unit that is a mixture of clastic and carbonate rocks (Miller, 1986). The Hawthorn Group has been divided into three formations, Coosawhatchie Formation, Markshead Formation, and the Parachula Formation, listed here from youngest to oldest (Huddlestun, 1987).

The Coosawhatchie Formation is composed predominantly of clay, but also has sandy clay, argillaceous sand, and phosphorite units and is approximately 170 thick in the Savannah area. This unit

disconformably or para-conformably overlies the Marks Head Formation and is distinguished from the underlying unit by consisting of dark phospathic clays or phosphorite in the lower part and fine-grained sand in the upper part (Huddlestun, 1987).

The Marks Head Formation is approximately 70 feet thick in the Savannah area and consists of light colored phosphatic, slightly dolomitic, argillaceous sand to fine-grained sandy clay with scattered beds of dolostone, limestone, and siliceous claystone. The Marks Head Formation disconformably overlies the Parachula Formation and is distinguished from the underlying unit by being more phosphatic, siliceous, and dolomitic and is less calcareous (Huddlestun, 1987).

The Parachula Formation consists of sand, clay, limestone and dolomite, and is approximately 10 feet thick in the Savannah area. The Parachula Formation generally overlies the Suwanee Limestone in Georgia. Huddlestun, 1987, also stated that the Parachula Formation disconformably overlies the Lazaretto Creek Formation in Chatham County, Georgia; however, other references regarding the Lazaretto Creek Formation were not located. Therefore, details of this formation have not been included in this report (Huddlestun, 1987).

4.1.1.5 Suwanee and Ocala Limestone

The Suwanee Limestone of Oligocene age consists of a cream to tan, crystalline, highly vuggy limestone and is approximately 100 feet thick in the Savannah area (Miller, 1986) and overlies the Ocala Limestone. The Ocala Limestone of late Eocene age is a gray to cream, dense, highly fossiliferous limestone (Furlow, 1969).

4.1.2 Groundwater Occurrence and Movement

The principal source of water in the coastal area of Georgia is the Floridan aquifer system. Secondary sources of water in the area are the surficial aquifer and the upper and lower Brunswick aquifers (Clark, et al, 1990). These aquifers are discussed in the following sections.

Recharge to aquifers is dependent on precipitation, evapotranspiration, and surface water infiltration. Average annual precipitation is less than 46 inches in Chatham County, Georgia. Average annual runoff is 10 inches. Evapotranspiration rates ranged from 31 to 41 inches per year in the Coastal area of Georgia (Clarke, et al, 1990).

Discharge from aquifers occurs naturally as flows to streams, springs, and adjacent aquifers. Groundwater is also discharged off shore and to wells in the area (Clark, et al, 1990).

4.1.2.1 Surficial Aquifer

The surficial aquifer consists of interlayered sand and clay of the undifferentiated deposits, Cypresshead Formation, and the Coosawhatchie Formation. A dense phosphatic silty clay of the Coosawatchie Formation acts as a basal confining unit. Locally, layers of clay that are really extensive act as confining units and at that location, the aquifer is under confined or artesian conditions (Clark, et al, 1990).

Generally, the aquifer is under water table conditions and is recharged by infiltration throughout the area of its occurrence. Water in the aquifer flows east to the coast and the water level near the coast

is influenced by the tidal changes. The thickness of this aquifer ranges from 65 feet to 230 feet and is approximately 100 feet thick in the Savannah area (Clarke, et al, 1990).

Wells in the aquifer reportedly yield 2 to 180 gallons per minute (gpm). In Chatham County, wells yield 10 to 40 gpm, and the aquifer has an estimated hydraulic conductivity of 2 to 65 feet per day (fpd) and transmissivity of 14 to 1,100 square feet per day (ft²/d) in the unconfined water bearing zone, and a hydraulic conductivity of 40 to 400 fpd and a transmissivity of 150 to 6,000 ft²/d in the lower semiconfined water bearing zone (Clarke, et al, 1990).

The lower confining unit ranges in thickness of 15 feet to 90 feet and is approximately 30 feet in the Savannah area. In the Brunswick area, the vertical hydraulic conductivity of the confining unit ranges from 5.3×10^{-5} to 13.0×10^{-5} feet per day (Clark, et al, 1990).

4.1.2.2 Upper Brunswick Aquifer

The upper Brunswick aquifer consists of poorly sorted, fine-to-coarse-grained, slightly phosphatic and dolomitic quartz sand of the Markshead Formation. Silty clay and dense, phosphatic dolomite of the Markshead Formation and the Parachula Formation acts as a basal confining unit. The lower Brunswick aquifer is not evident in the Savannah area; therefore, it is not discussed in this report (Clark, et al, 1990).

The aquifer is under confined conditions and is recharged where Miocene sediments outcrop northwest of the site in Screven and Bulloch Counties, Georgia. Water levels in the aquifer respond to seasonal climatic changes and fluctuations are similar to those in the Upper Floridan aquifer. The thickness of the aquifer ranges from 20 to 150 feet and is approximately 25 feet in the Savannah area (Clark, et al, 1990).

Reported well yields for the upper and lower Brunswick aquifer range from 3 to 180 gpm. There are no available data on the hydraulic properties of the upper Brunswick aquifer. Based on data from the lower Brunswick aquifer, an average hydraulic conductivity of 38 ft/d and a transmissivity of 680 ft²/d to 5,700 ft²/d have been estimated (Clark, et al, 1990).

The lower confining unit ranges in thickness of 14 feet to 120 feet and is approximately 90 feet in the Savannah area. In the Brunswick area, the vertical hydraulic conductivity in the lower half of the confining unit ranges from 5.3 x 10⁻⁵ to 1,300 x 10⁻⁵ fpd (Clark, et al, 1990).

4.1.2.3 Upper Floridan Aquifer

The Upper Floridan aquifer consists of limestone of the Suwanee Limestone formation and limestone and dolomite of the Ocala Limestone formation. Dense dolomitic limestone of the Ocala Limestone acts as a semi-confining basal unit (Clark, et al, 1990).

The aquifer is under confined conditions and is recharged northwest and west of the coastal area of Georgia. Water levels in the aquifer respond to seasonal climatic changes and in the Savannah area groundwater flows toward the pumping center created by water withdrawal from wells for the City of Savannah. The thickness of the aquifer ranges from 200 feet to 700 feet and is approximately 250 feet thick in the Savannah area (Clark, et al, 1990).

Withdrawal from the Upper Floridan aquifer during 1986, was approximately 73 million gallons per day. The average transmissivity for the Savannah area ranges from 28,000 to 33,000 ft²/d (Clark, et al, 1990).

The lower confining unit ranges in thickness of 160 to 280 feet. In the Brunswick area, the vertical hydraulic conductivity ranges from 0.4×10^{-5} to 5.3×10^{-5} fpd. Joints and fractures in this unit have produced zones of higher secondary vertical hydraulic conductivity.

4.2 SITE HYDROGEOLOGY

4.2.1 Geology

From 19 soil borings, soil samples were collected and their lithology is described and recorded on boring logs in Appendix D-1. Lithology beneath the site consists predominantly of brown and tan, loose, fine to very fine sand with 10 percent silt (silty sand). Layers of sand, silt, and clayey sand have also been observed. A poorly graded, tan, loose, fine to very fine-grained sand layer approximately 1 foot thick is located in the vicinity of Well MW-4. A poorly graded, white, loose, very fine-grained sand layer, approximately 0.5 feet thick is located from 3 (Boring A-3) to 5.5 (A-9) fbls in the north-northeast corner of the site and an inorganic, black, soft, fat, organic silt layer approximately 0.5 feet thick and containing roots is located from 2 (Boring MW-1) to 4 (Boring A-9) fbls north of the pump island area. Soils appear to be finer to the east-southeast. At Boring MW-8, a gray, medium- to fine-grained clayey sand layer, approximately 0.5 feet thick is located 1.5 fbls and is underlain by a 3-foot thick black, organic-rich silt. At approximately 5.5 fbls in this area, a tan, very fine- to medium-grained clayey sand layer exists. A subsurface cross-section of the area showing lithology is presented in Plate 6. Surficial lithology beneath the site is consistent with undifferentiated alluvial deposits.

4.2.2 Groundwater Occurrence and Movement

Groundwater beneath the site is present at a depth of less than 5 feet and flows to the northwest. A water table contour map is presented in Plate 7. As previously mentioned, the hydraulic conductivity of the aquifer ranges from 0.9×10^{-3} to 3.1×10^{-3} feet per minute and averages 1.9×10^{-3} feet per minute (fpm) which corresponds to silty sand (Heath, 1987). Using the average hydraulic conductivity (k), a hydraulic gradient (dh/dl) of 0.01 ft/ft, and an assumed effective porosity (n) of 0.20 for a silty sand (Heath, 1987), an average groundwater seepage velocity (v) of 1.0×10^{-4} fpm for the movement of groundwater across the site has been calculated using the following equation:

$$V = \frac{ki}{n}$$

As stated in Section 4.2.1, the lithology is finer in grain size to the southeast. With the exception of MW-6, the hydraulic conductivity value calculated for each well increases in value from the east to the west. This information supports data indicating that the lithology is finer in grain size to the east. As shown in Plate 5, the surficial aquifer extends to approximately 100 fbls.

4.3 GROUNDWATER UTILIZATION

According to EPD UST Regulations Chapter 391-3-15-.09, target cleanup concentrations for soil and groundwater are dependent on the site's location with respect to nearby water supply systems. In accordance with the above mentioned regulations, an attempt was made to locate points of withdrawal from public drinking water systems within a 3-mile radius of the site and points of withdrawal for non-public water systems within a 0.5-mile radius of the site. Information was obtained from HAAF, the City of Savannah, and U.S. Geological Survey, and from a windshield survey conducted within a 0.5-mile radius of the site. Information obtained from HAAF, the City of Savannah, and the U.S. Geological Survey (U.S.G.S.) are included in Appendix G. The Chatham County Health Department was also visited; however, no relevant information was obtained.

HAAF has 11 groundwater supply wells. Locations of these wells are shown on Plate 8 and well details are presented in Table 8. Of these 11 wells, eight are located within 3 miles of the site and four of the eight are used for drinking water. Casing depths of the drinking water wells range from 259 to 324 fbls with an average depth of 278 fbls. Flow rates range from 30 to 1,400 gpm of water, and averages 713 gpm. Where discrepancies occur between the U.S.G.S. data and HAAF data regarding well construction details, U.S.G.S. data were used for depth of well and bottom of casing data in the preparation of Table 8. HAAF data were used for well usage.

HAAF Well No. 1, a public supply well, is nearest to the site and is located approximately 170 feet southeast (water tank) of the UST area. This well is cased from the surface to approximately 259 fbls; has the capacity to discharge 1,300 gpm; and is located hydraulically upgradient of the UST area. This is shown on Plate 8. HAAF receives its water from the Upper Floridan aquifer, which is separated from the surficial aquifer by two confining units and the upper Brunswick aquifer. This stratigraphic relationship is shown in Plate 5.

Seven public supply wells were located within 3 miles of the site, but outside HAAF. Locations of these wells are shown on Plate 9 and well details are presented in Table 8. All information obtained from the owner(s) were used on Table 8 when applicable. These wells were located through the U.S.G.S. Water Well Survey and their locations were verified in the field. Casing depths to these seven wells range from 146 to 290 fbls with an average depth of 250 fbls. Flows range from 150 gpm to 3,500 gpm (of known discharges), and average 1,321 gpm.

Four of the seven public water supply wells, located outside HAAF, are owned and operated by the City of Savannah. All well construction information received from the City of Savannah was consistent with data from the U.S.G.S. The only discrepancies were discharge rates and usage of some wells. Rates and well usage provided by the City of Savannah were used in Table 8.

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According to Harry Jue, City of Savannah's Water Director, the only surface water withdrawal point is located on the Wilmington River. This river is more than 3 miles away from the site. HAAF receives all its water from on-wells located at the base.

5.0 EXTENT OF CONTAMINATION

5.1 HYDROCARBONS IN THE SOIL

Soil samples collected from boreholes and during well installation indicate that soil in the vicinity of the site has been impacted by petroleum product. BTEX concentrations above method detection limits were detected in eight of the 24 samples analyzed. TPH concentrations above method detection limits were detected in 23 of 24 samples analyzed. Lead concentrations were detected in all five samples analyzed.

As shown on Plate 10, the highest concentrations of total BTEX (8,050 ppm at MW-1) and TPH (25,000 ppm at MW-1) are in the vicinity of the USTs.

Concentrations decrease with increasing distance from this area. However, the concentration decrease is not proportional to distance. There are some localized high concentration areas like MW-7 that suggest past spills unrelated to tank releases. However, for a conservative estimate of contaminated soil one continuous hydrocarbon plume of soils with concentrations exceeding EPD's most liberal clean up criteria for BTEX and TPH concentrations have been drawn. Based on the areal extent of this plume (5,920 square feet) and the average depth to water (3.04 feet), approximately 700 cubic yards of soil appears to be grossly contaminated.

Lead concentrations in the samples analyzed ranged from 3.4 ppm to 18 ppm. In general, soil consists of an abundance of chemical elements including lead that are naturally occurring. Naturally occurring lead concentrations for soil within the Savannah area generally ranges from 20 to 30 ppm (Hansford, et al, 1971). These concentrations are higher than lead concentrations detected at the site; therefore, the lead concentrations alone detected at the site do not clearly indicate that a petroleum release has occurred.

5.2 LIQUID HYDROCARBON OCCURRENCE

Phase-separated product was observed at a thickness of 0.61 feet in Well MW-1. As shown in Plate 11, MW-1 is located approximately 5 feet west of the western-most UST. For this reason, it is assumed the phase-separated product is localized as shown in Plate 11. No evidence of phase-separated product has been observed in any of the other wells.

5.3 DISSOLVED HYDROCARBON OCCURRENCE

The presence of phase-separated product in MW-1 and elevated concentrations of BTEX and TPH in groundwater samples collected indicate that groundwater in the vicinity of the site has been impacted by petroleum product. BTEX concentrations above method detection limits were detected in six of the ten samples analyzed. TPH concentrations above method detection limits were detected in three of ten samples analyzed.

As shown on Plate 11, the highest concentration of total BTEX (28,200 μ g/l) and TPH (55 μ g/l) were detected in the well containing phase separated product. Concentrations decrease with increasing

distance from the UST area. However, as with the soil concentrations, the concentration decrease is not proportional to distance because of localized areas of elevated concentrations.

5.4 CONCEPTUAL MOVEMENT OF HYDROCARBONS

The case scenario at this site consists of leaking USTs that are partially submerged below the water table. In this instance, one would expect to find:

- 1. Contaminated soil in the immediate vicinity of the tank because of the leak;
- 2. Contaminated soil spreading laterally from the tank area because vertical movement of contaminants has been impeded by denser layers and extends laterally on top of these layers while moving vertically;
- 3. Phase-separated product in the immediate vicinity of the UST as well as downgradient to the UST; and
- 4. Dissolved hydrocarbons in the groundwater surrounding the leaking USTs and downgradient of the UST area.

Localized "hot" areas with respect to soil and groundwater are common in areas near tanks and pump islands because releases associated with the handling of the product have accumulated over time.

Soil and groundwater quality data, along with field observations, have indicated that the "hottest" area at the site is in the immediate tank area. Phase-separated product and high concentrations of dissolved hydrocarbon occurred in MW-1 (downgradient to the tanks). Considerably lower concentrations occurred in MW-3 and MW-4 (upgradient of the tanks). This indicates that the contaminants are stationary or migrating in the direction of groundwater flow.

With the exception of MW-6, elevated concentrations of BTEX and TPH in samples collected throughout the site, except in the area of the tank, can be attributed to releases occurring during the product handling. The location of MW-6 is upgradient and away from the work area at Building 710. The source of elevated concentrations of BTEX and TPH on the soil and BTEX in the groundwater is not known.

6.0 REMEDIAL ACTION PLAN

6.1 CORRECTIVE ACTION COMPLETED OR IN PROGRESS

At this time, correction action is in the planning stage. To date, no remediation of contaminated soil and groundwater has occurred, nor has any phase-separated product been recovered.

6.2 OBJECTIVES OF CORRECTIVE ACTION

The objective of the corrective action is to remediate soil contamination and to recover phase-separated product in general accordance with EPD Regulations Chapter 391-3-15-.09.

6.2.1 Proposed Remedial Action Levels

It is proposed that all soil in the vicinity of the USTs with concentrations exceeding 100 ppm total BTEX and 500 ppm TPH be remediated to lower concentrations. Visible phase-separated product will be removed from the subsurface and the movement of dissolved hydrocarbons in groundwater will be monitored.

6.2.2 Basis for Proposed Remedial Action Levels

According to EPD Regulations Chapter 391-3-15-.09(2), one of the following clean up objectives must be proposed:

- At UST corrective action sites where a point of withdrawal for a public drinking water system exists within 3 miles of the contaminant plume boundary or a point of withdrawal for a non-public water system exists within 0.5 miles of the contaminant plume boundary, the UST owner or operator will:
 - 1. Remediate soil contamination that exceeds 100 ppm TPH, or 20 ppm total BTEX;
 - 2. Remove visible phase separated product; and
 - 3. Remediate groundwater contamination that exceeds federal and state Maximum Contaminant Levels (MCLs) or alternate concentration limits as established by the Director.
- ♦ At other UST corrective action sites, the UST owner or operator will:
 - 1. Remediate soil contamination that exceeds 500 ppm TPH or 100 ppm total BTEX;
 - 2. Remove visible phase separated product; and
 - 3. Delineate the full extent of groundwater contamination.

Below Chapter 391-3-15-.09(b), the regulations state that the remediation of soil contamination that exceeds 100 mg/kg TPH or 20 mg/kg total BTEX, the remediation of groundwater contamination that exceeds federal and state MCLs or alternate concentration limits as established by the Director, and delineation of the extent of groundwater contamination may not apply if it can be demonstrated that existing public or non-public water systems or surface waters are upgradient from the contaminant plume or are not hydraulically interconnected with the contaminant plume.

As shown on Plates 8 and 9 and Table 8, 14 public wells are within 3 miles of the contaminant plume and the nearest well is located within 150 feet of the plume. Of these 14 wells, only three lie to the north-northwest in the direction of groundwater flow. The remaining wells lie in various directions and are considered crossgradient and upgradient with the nearest well being upgradient of the site.

None of the above wells are cased off in the surficial aquifer. All but one well receives its water from the Upper Floridan aquifer. This well receives its water from the Upper Brunswick aquifer. The top of the Upper Floridan aquifer is approximately 230 fbls and the top of the Upper Brunswick is approximately 130 fbls in the Savannah area. The confining unit between the surficial aquifer and the Upper Brunswick aquifer is approximately 30 feet thick with a range of vertical hydraulic conductivity values consistent with that of a clay. The confining unit between the Upper Brunswick aquifer and the Upper Floridan aquifer is approximately 80 feet thick and the lower half of the unit has a range of vertical hydraulic conductivity values that are consistent with that of silt to clay. As indicated by the hydraulic properties of the two confining units, existing public water systems are not hydraulically interconnected with the contaminant plume.

As mentioned earlier, surface water bodies are located in the area. The closest surface water body is within HAAF and is located crossgradient approximately 1,200 feet to the southwest. A lake is located approximately 0.5 miles northwest of the site just outside HAAF's boundaries. The lakes, while being crossgradient and downgradient of the site, are located sufficient distances away to not be affected by contamination of this magnitude. However, additional monitor wells will be installed to monitor the movement of dissolved hydrocarbons once the USTs, contaminated soil, and phase-separated product are removed.

6.3 PROPOSED REMEDIAL ACTION AND IMPLEMENTATION

6.3.1 Underground Storage Tank Closure

To eliminate the source, the four USTs and associated piping will be removed and disposed of properly by a licensed contractor. This UST closure plan is in accordance with EPD's UST closure guidelines, "So You Want to Close an UST?", dated April, 1992.

Notification

EPD will be notified at least 30 days prior to the removal of the USTs and be furnished with the following information:

- ♦ Owner(s) of the tanks;
- ♦ The tank location (street address);

- ♦ The capacity and liquid stored in each tank; and
- ♦ The date that on-site closure activity is scheduled to begin; and
- ♦ Method of contaminated soil disposal.

Within 30 days after the tank has been removed and the excavation backfilled, EPD will be notified that the closure has been completed. An amended version of the original EPA Form 7530-1 "Notification for USTs" will be submitted by Fort Stewart, DEH, Environmental Office at this time.

Prior to tank removal, DEH, the military division equivalent to the Fire Marshall will be notified.

Confirmatory Sampling

Since it is already known that contaminated soil and phase-separated product exists, confirmation samples will be collected after the removal of all contaminated soil and phase-separated product. One water sample will be collected from the base of the tank pit and analyzed for BTEX and TPH by EPA Methods 602 and 418.1, respectively. Six to eight soil samples will be collected from the sidewalls of the tank pit and pump island area to be analyzed for BTEX and TPH by EPA Methods 8020 and 418.1, respectively. Results of the confirmatory sampling will be known within 24 hours and excavation activities can proceed as needed.

Backfill Procedures

The tank pits will be backfilled with "clean" material.

6.3.2 Soil Excavation

During the removal of the USTs, the known contaminated soil plume as shown on Plate 10 will be excavated. The estimated volume to be removed is calculated by using 5,920 square feet for surface area and 5 feet (approximately 2 feet below the water table). Based on this in-place volume, it is estimated that approximately 1,000 cubic yards of contaminated soil will be removed. Soils from borrow areas within HAAF will be used to backfill the excavation.

If contaminated soil is temporarily stored on site, it will be placed on and covered with plastic. Contaminated soil will either be bioremediated and aerated on base, thermally treated using a mobile incinerator unit, or transported to an asphalt plant or to an acceptable landfill. Disposal of the soil will be handled by a permitted treatment/storage/disposal facility. Soil samples will be obtained from the stockpile for laboratory analyses. The type of analyses performed will be based upon the method of remediation that is selected.

6.3.3 Liquid Hydrocarbon Recovery

After the tanks are removed, contaminated soil will be removed as discussed in the previous section. Soil will be removed from 1 to 2 feet below the water table in areas of the pit where phase-separated product is observed. If phase-separated product is observed in any appreciable thickness, a sump(s)/trench(es) will be excavated in order to facilitate its removal. The product will be skimmed off

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the top of the water, stored in a tank and transported off site for proper disposal, or if the thickness of product is relatively small, absorbent pads may be sufficient to effect its removal. This work will be performed by an outside contractor.

7.0 RECOVERY SYSTEM DESIGN

7.1 LIQUID HYDROCARBON RECOVERY

7.1.1 Monitor Well Design and Installation

During tank closure and excavation of contaminated soil, Monitor Wells MW-1 and MW-2 will be destroyed. These wells will be replaced by one well located in the area of the now existing MW-1. One to two more wells will be installed northwest (downgradient) of the exiting plume area.

The newly installed wells will consist of 2-inch diameter PVC casing and screen and will be sealed with a watertight locking cap. Five feet of No. 0.010 slotted screen will be placed to bracket the water table. A sand filter pack will be placed in the annulus space and will extend from the bottom of the well to approximately 1 foot above the top of the screen. A bentonite seal, approximately 0.5 feet thick will be placed on top of the filter pack. The remainder of the annular space will be filled with cement. The well will be completed below grade and protected by a manhole structure.

7.1.2 Product Recovery

If phase-separated product is detected in the monitor wells after the initial remedial action, product bail down tests will be performed to evaluate relative quantity. These data will be used to determine what action should be taken to enhance product recovery, such as the installation of recovery wells, trenches, etc.

7.2 Dissolved Hydrocarbon Plume Assessment

One or two more monitor wells will be installed northwest (downgradient) of the existing plume area. These wells, along with existing wells, will be used to observe the movement of the dissolved hydrocarbon plume in the groundwater. Monitor well design will be as described in Section 7.1.1.

The wells will be installed using hollow-stem augers and soil samples will be collected with split-spoon samplers at continuous intervals. Lithology will be described, and samples will be screened with an OVA.

If any OVA readings exceed 10 ppm above background for a given well, a sample from the "hottest" interval will be sent to a laboratory to be analyzed for BTEX and TPH by EPA Methods 8020 and 418.1.

One soil sample from each of the downgradient wells will be collected from the screen interval for sieve analysis. This data will be used to design a recovery well if needed.

7.3 MONITORING AND MAINTENANCE PROGRAM

This program will address monitoring for the absence or presence of phase-separated product and the movement of dissolved hydrocarbons after the initial remediation. It does not cover additional

remediation activities. If additional remediation is required, an amended monitoring and maintenance program will be addressed in the appropriate status report.

7.3.1 Monitoring

Quarterly fluid level measurements from all monitor wells will be taken to evaluate the direction of groundwater flow. Wells will also be checked for the presence of phase-separated product. Groundwater samples will be collected from all wells and analyzed for BTEX and TPH by EPA Method 602 and 418.1, respectively. Based on the direction of groundwater flow, selected upgradient wells will be eliminated from the monitoring program if product is not evident after three events. The monitoring will continue until it is evident that the water quality of the nearby surface water bodies will not be affected.

Since one drinking water well is located within 150 feet of the plume, a water sample will be obtained and analyzed for BTEX and TPH by EPA Methods 602 and 418.1, respectively. If BTEX and/or TPH concentrations are detected above method detection limits, the well will immediately be resampled. A rinse water blank, equipment blank, and trip blank will also be analyzed for BTEX by EPA Method 602.

If it is determined that water from the supply well has been contaminated by the plume, a groundwater remediation system will be designed and implemented.

7.3.2 Maintenance

To maintain the integrity of the monitor wells, all sampling equipment will be decontaminated prior to and after sampling each well. Decontamination procedures will be as follows:

- Alconox/tap water wash;
- Deionized water rinse;
- Pesticide propanol rinse; and
- ♦ Then allowed to air dry.

During sampling, all wells will be inspected for missing or damaged parts. Observations will be recorded and parts will be replaced or repaired. Wells will be inspected for:

- ♦ Missing locks. All wells are to be locked when not being sampled.
- Standing water in the manhole. Standing water will be removed prior to sampling.
- Wells not sealed. Faulty seals will be replaced.

8.0 OVERALL CORRECTIVE ACTION IMPLEMENTATION

8.1 SCHEDULE

The tank closure and initial remediation activities will be conducted after completion of the remedial design and award of a contract. Award of a contract is expected to be accomplished by September, 1993. Laboratory turnaround time for the confirmatory samples will be expedited to 24-hour turnaround time. See Section 6.3.1 for the confirmation sampling plan. If additional remediation is not required, the monitor wells will be installed at that time. If needed, monitor wells will be installed approximately two weeks after the second excavation. Monitor wells will be sampled one to two weeks after their installation. This will allow time for stabilization. The nearby drinking water supply well (HAAF #1) will be sampled at this time.

Assuming that all contaminated soil and phase separated product has been removed, and the drinking water well is not contaminated, quarterly sampling of wells will be conducted until it is evident that the nearby lake's water quality will not be affected. At this time sufficient information is not available to estimate the duration of the sampling program. If contamination, as stated above, still exists at the site, then the schedule will be modified to include new remedial activities. Modifications will be made in the appropriate status reports.

8.2 STATUS REPORTS

8.2.1 Final Completion Report

After completion of the tank closure and initial remedial activities, the final completion report will be submitted to EPD by the 24th Infantry Division (Mech) and Fort Stewart, Environmental Office, Fort Stewart, Georgia. This report will contain a section summarizing remedial activities. Remedial activities will be divided into three sections:

- 1) Tank removal;
- 2) Soil excavation and disposal; and
- 3) Phase separated product recovery and disposal.

The report will also include a section on confirmatory sampling and analysis. This section will include details on sample collection and a rationale on sample locations. A plate showing sample locations and soil concentrations will be provided. Analytical results for soil and groundwater samples will also be included. Conclusions and recommendations will close out the report.

It is envisioned that the Table of Contents will consist of the following:

CONTENTS

- 1.0 Summary of Remedial Activities
 - 1.1 Tank Removal

- 1.2 Soil Excavation and Disposal
- 1.3 Phase Separated Product Recovery and Disposal
- 2.0 Confirmatory Sampling and Analysis
 - 2.1 Sample Collection
 - 2.2 Analytical Results
- 3.0 Conclusions
- 4.0 Recommendations

The Appendices will contain a map showing sample locations and sample concentrations, a summary table of analytical results, if needed, and laboratory reports.

8.2.2 Quarterly Progress Reports

Status reports will be submitted to the State on a quarterly basis. These reports will include liquid level and groundwater flow information and groundwater sample collection and analysis information. The report will also summarize changes in the monitoring plan and planned actions. The Table of Contents will consist of the following items:

CONTENTS

- 1.0 Summary
 - 1.1 Activities
 - 1.2 Results
- 2.0 Liquid Levels and Groundwater Flow
- 3.0 Groundwater Quality
 - 3.1 Sample Collection
 - 3.2 Analytical Results
- 4.0 Planned Actions

The Appendices will contain maps showing 1) water table elevations and contours; and 2) sample locations and concentrations. Hydrographs of selected wells will also be included. Analytical reports will be provided along with a summary.

If additional remediation is needed, a plan including design and implementation will be included in a "stand alone" Appendix.

9.0 PUBLIC NOTICE REQUIREMENTS

The project site is located within the boundaries of HAAF, with the closest property boundary being 0.4 miles away. Since no private property is contiguous to the UST site, public notification of the Corrective Action Plan is not required.

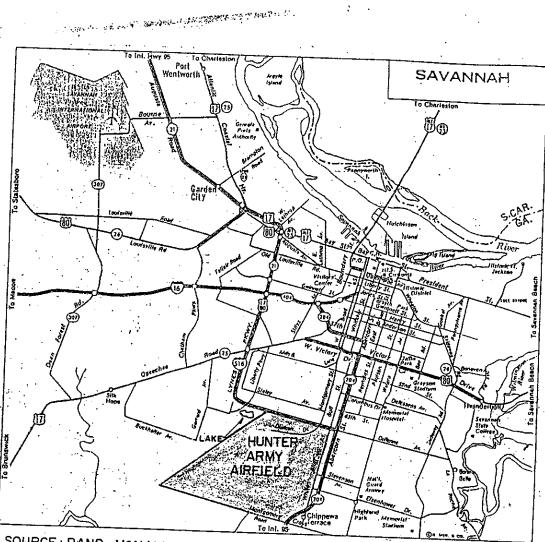
10.0 CLAIM FOR REIMBURSEMENT

Claims for reimbursement will not be made at this time.

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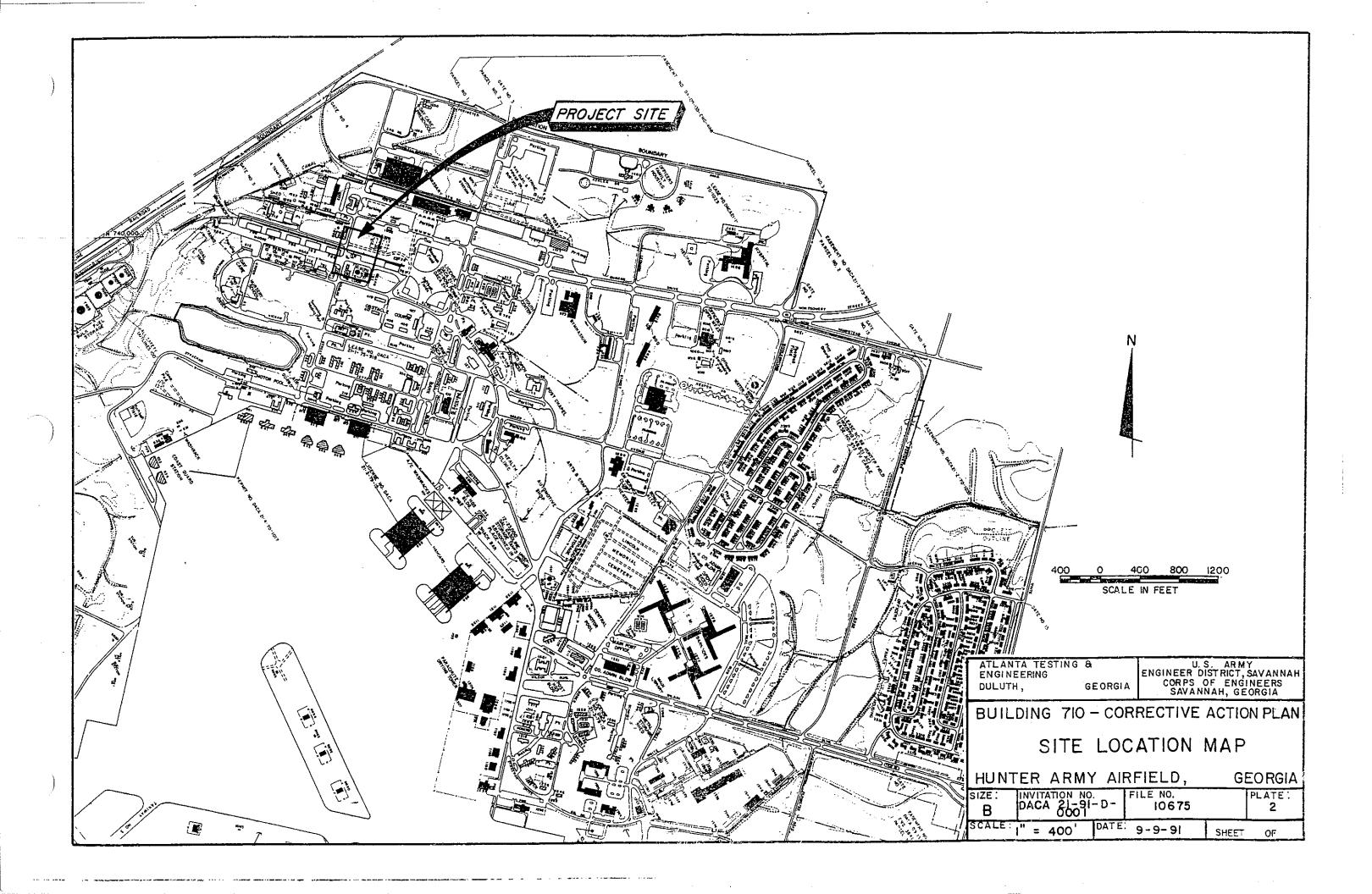
PLATES

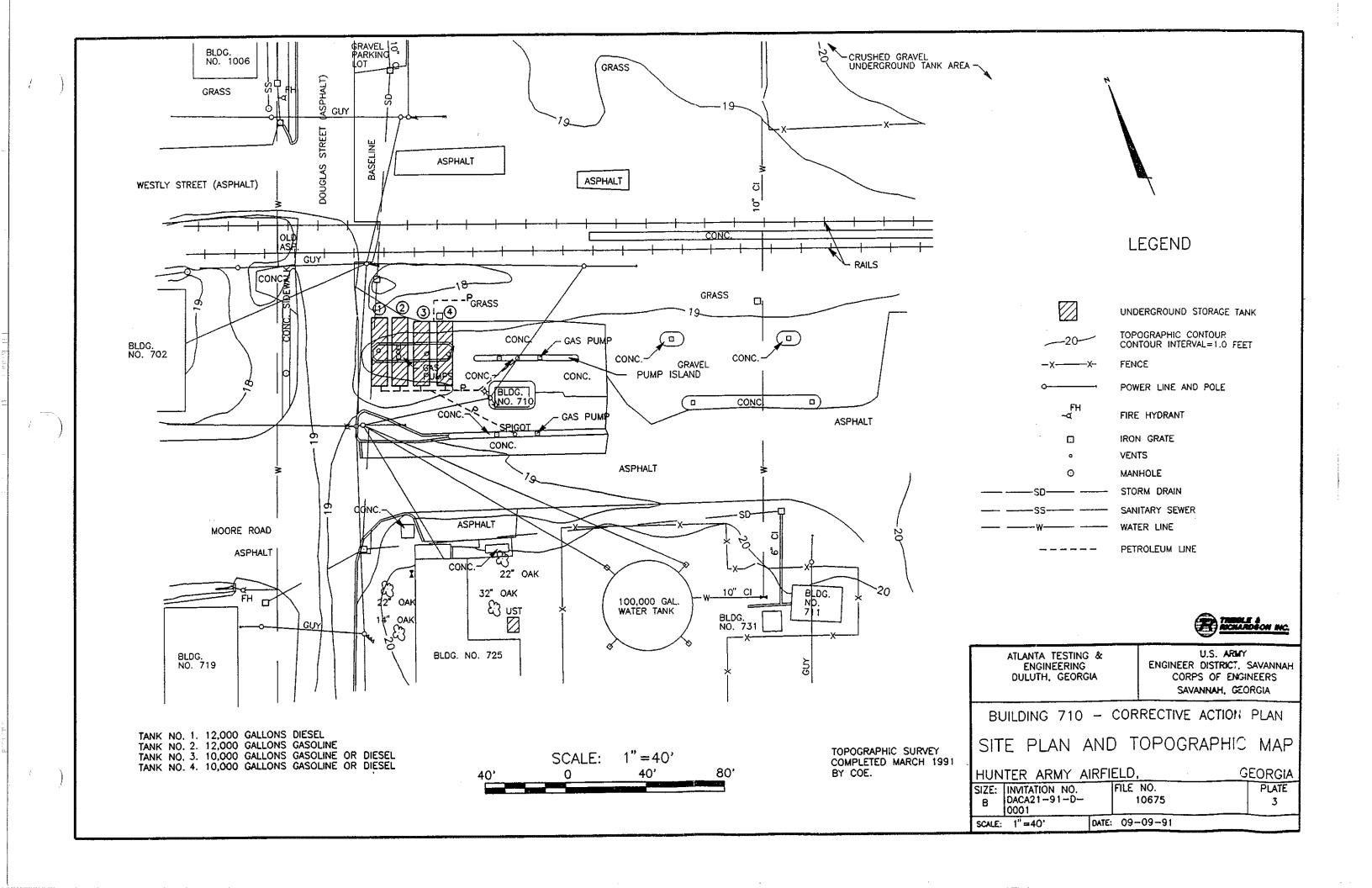


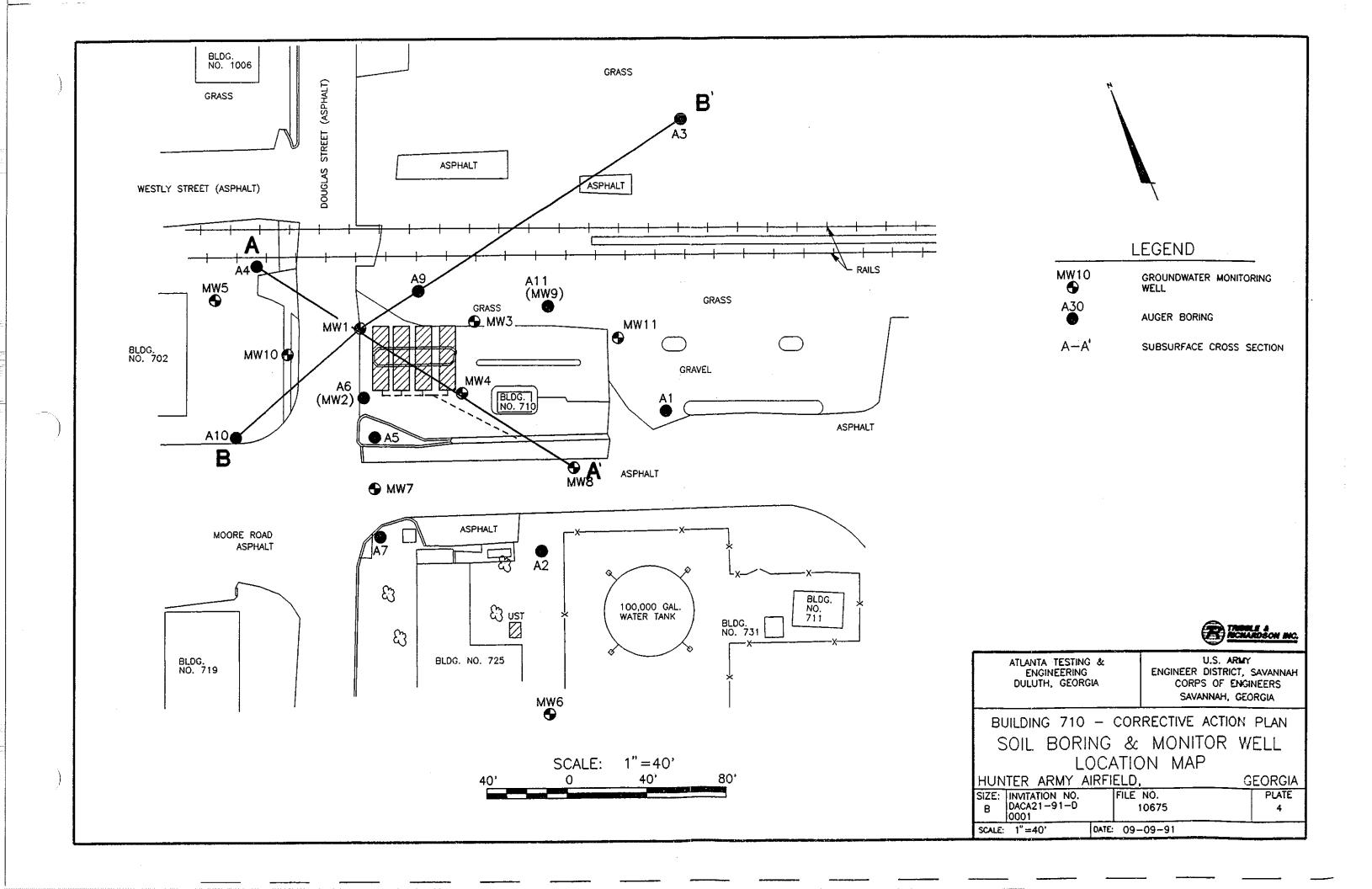
SOURCE: RAND MCNALLY GEORGIA STATE ROAD MAP

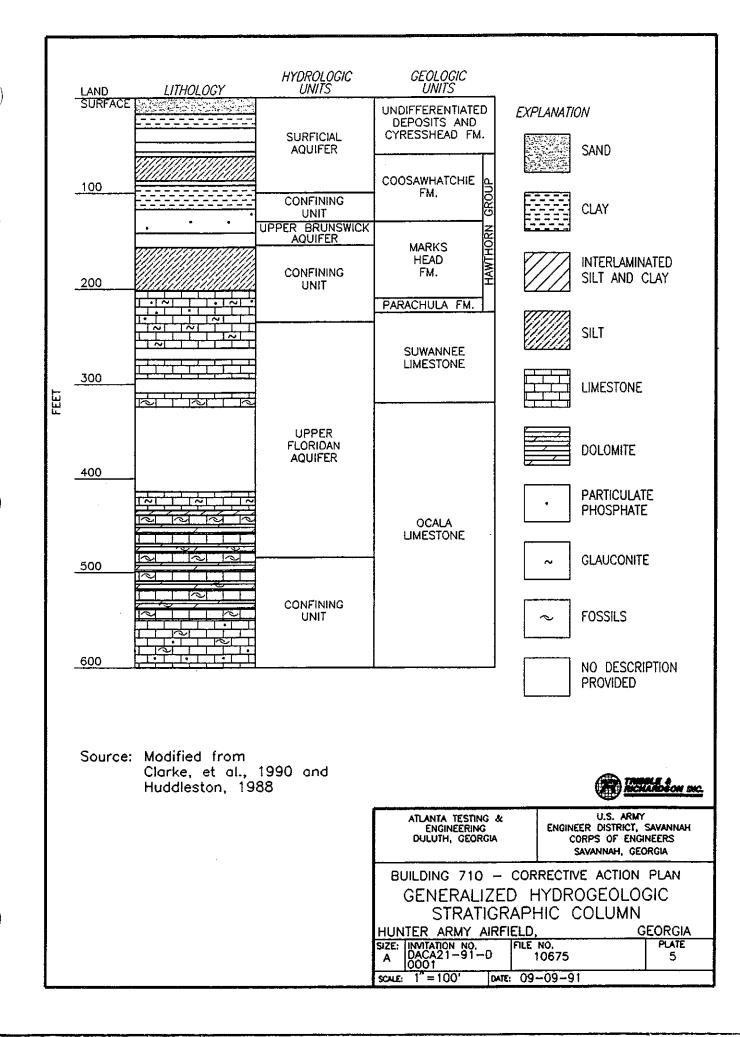
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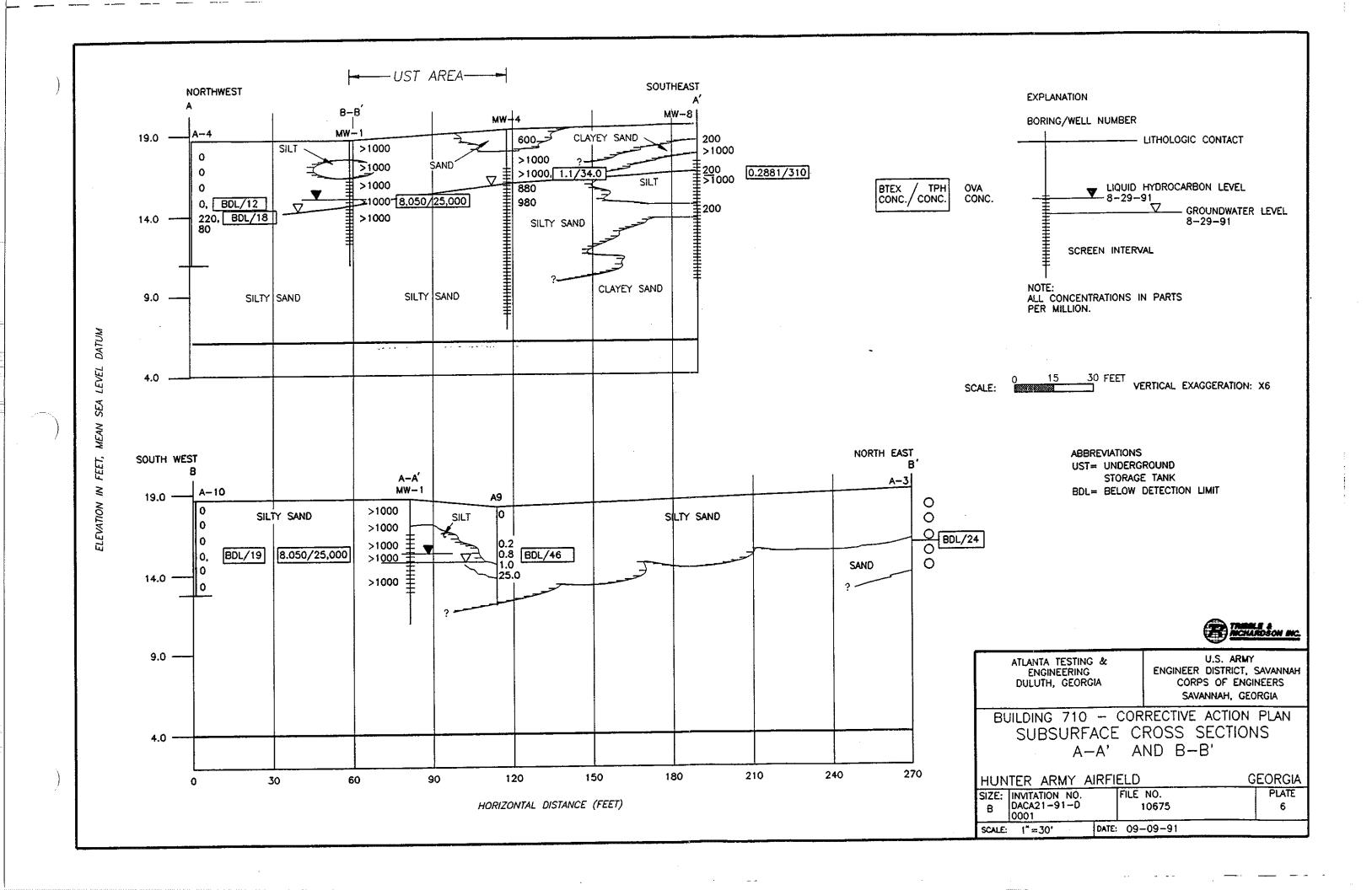
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	DACA 21-	7 I	LE NO. 10675		PLATE I
ľ	SCALE I"= 2.6MILES	DATE 9	9-91	SHEET	OF

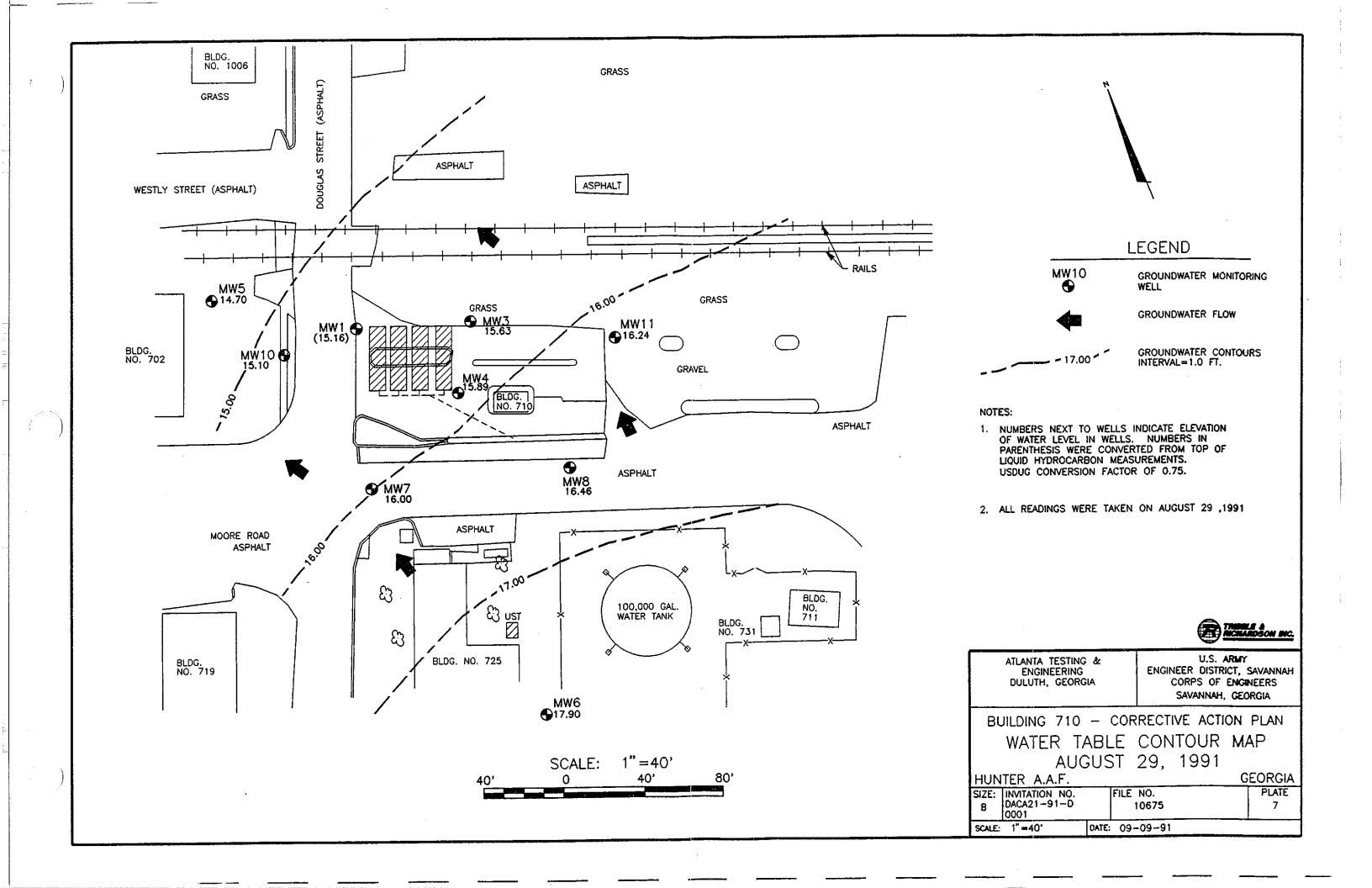


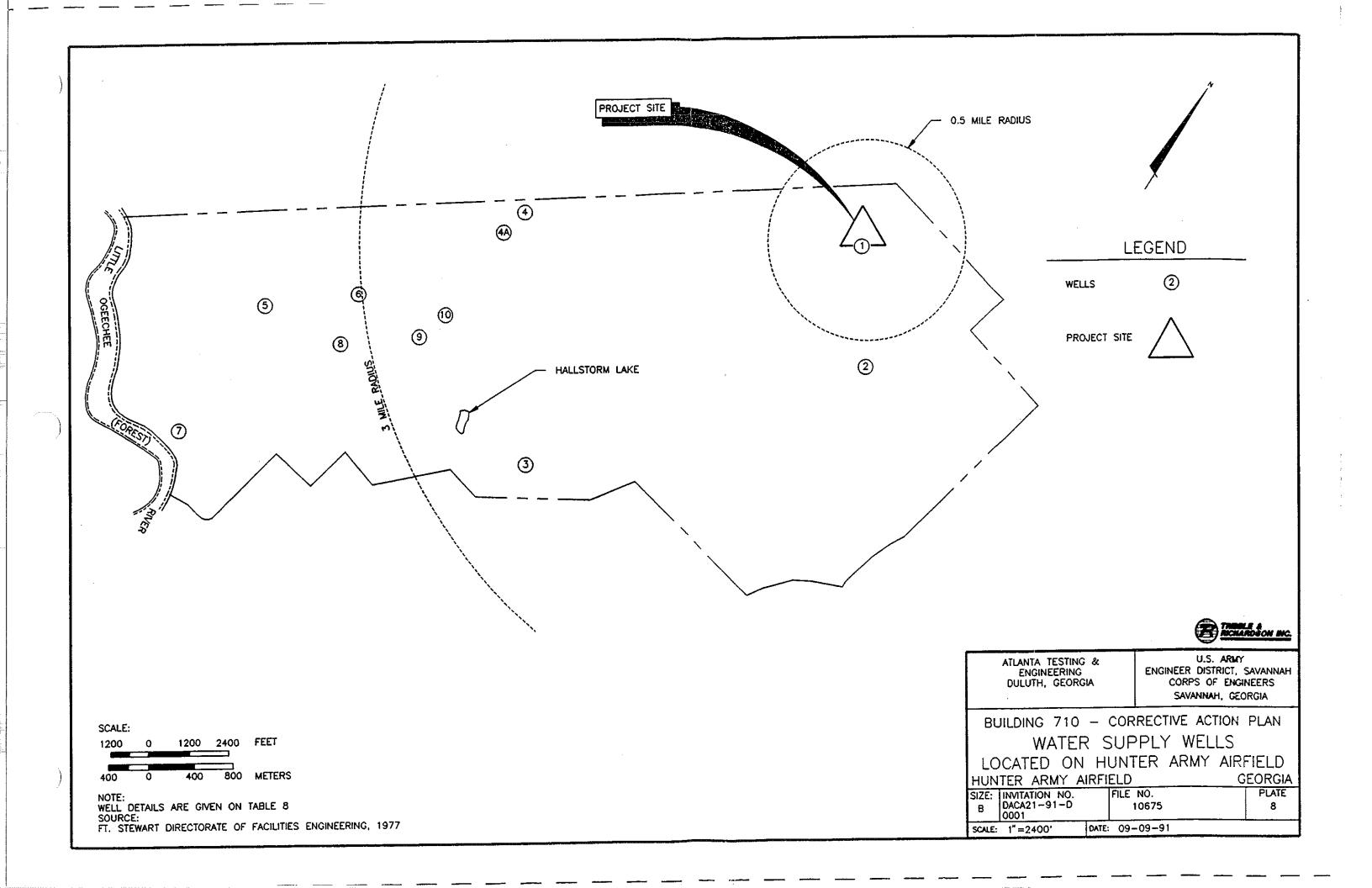


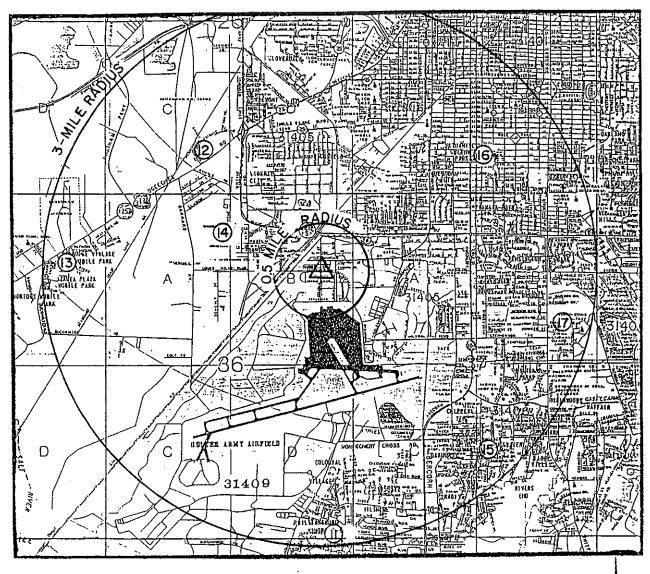












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LEGEND

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WELLS

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PROJECT SITE

NOTE: WELL DETAILS ARE GIVEN ON TABLE 8.

ATLANTA TESTING & ENGINEERING DULUTH, GEORGIA

U.S. ARMY
ENGINEER DISTRICT, SAVANNAH
CORPS OF ENGINEERS
SAVANNAH, GEORGIA

BUILDING 710 - CORRECTIVE ACTION PLAN
WATER SUPPLY WELLS
LOCATED OUTSIDE HUNTER ARMY
AIRFIELD BOUNDRIES

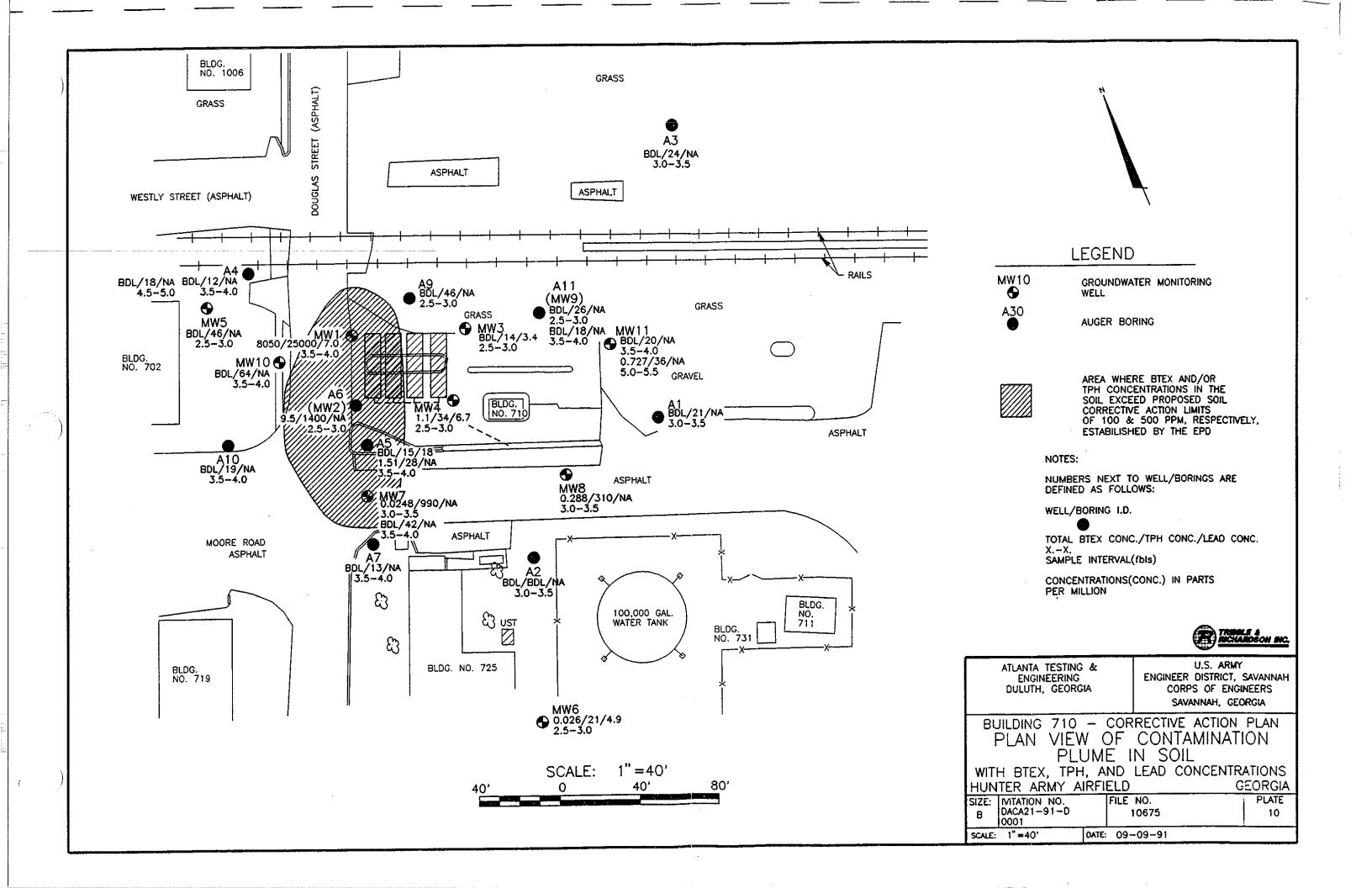
HUNTER A.A.F. GEORGIA

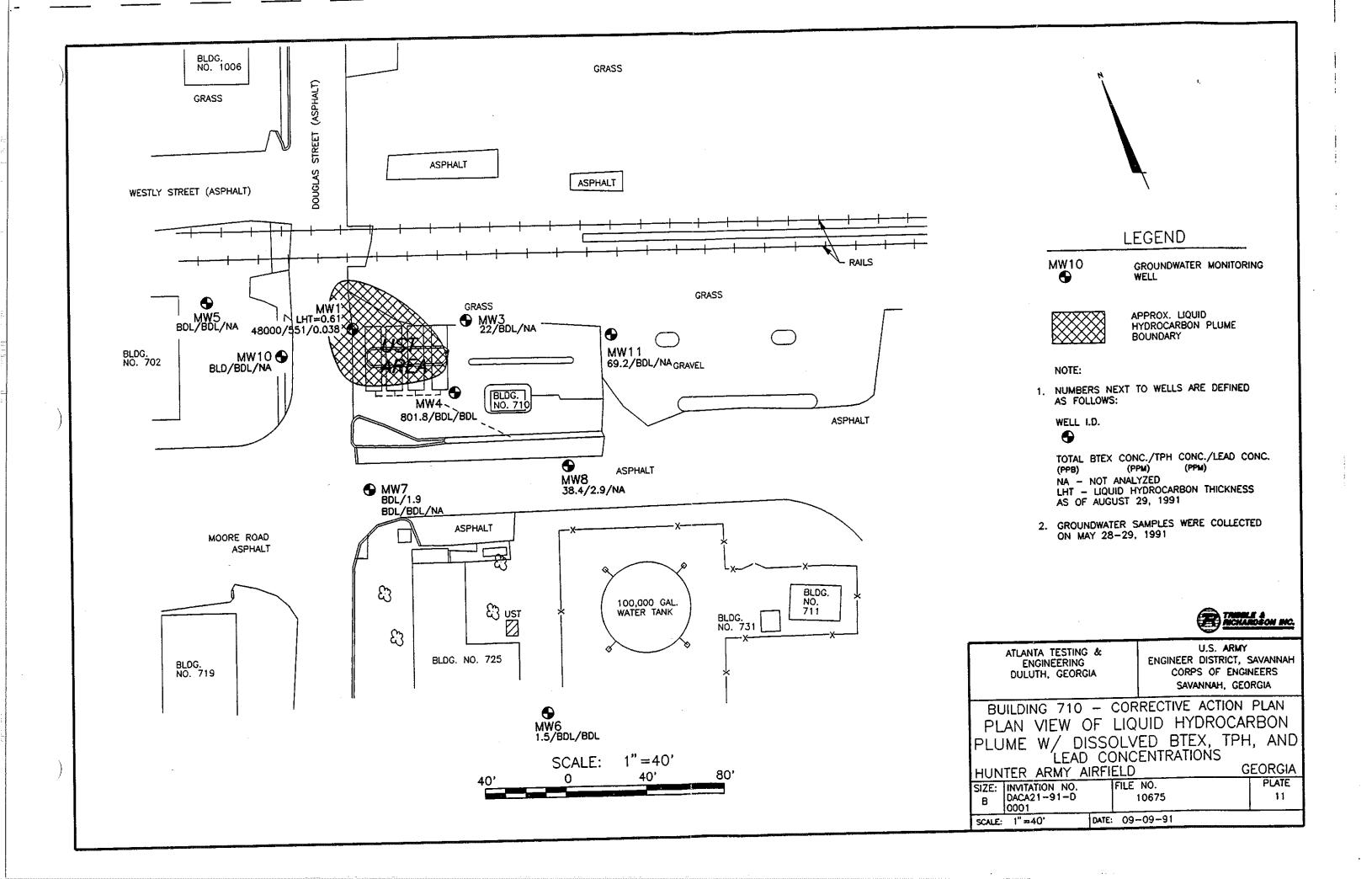
SIZE: INVITATION FILE NO. PLATE

A DACA21-91-0 10675 9

SCALE: 1" = 5556"

DATE: 09-09-91





TABLES

				IABLE I				
			Summary of S Hu Bui Sa Job No.]	Summary of Soil Boring Construction Data Hunter Army Airfield Building No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855	struction Data ield trea ia vo. 53855			Page 1 of 2
Boring No.	Date	Elevation Land Surface (R - MSL)	Driller	Drill	Initial Depth to Water (ft)	24-Hour Water Level Reading (ft)	Boring Depth (ft)	Comments
MW-710-1 (MW-1) 5	5/1/91	18.76	COE	HSA HA	4.80	3.57	8.0	well installed
MW-710-3 (MW-3) 5	5/2/91	19.13	COE	HSA HA	3.85	3.15	8.0	well installed
MW-710-4 (MW-4) 5	5/2/91	19.15	COE	HSA HA	3.15	3.30	12.5	well installed
MW-710-5 (MW-5) 5/	5/3-6/91	17.85	COE	HSA HA	3.10	3.87	11.0	well installed
/S 9-WM	5/14/91	21.05	COE	HSA/HA	5.61	4.29	11.0	well installed
MW-710-7 (MW-7) S/	5/13/91	18.18	COE	HSA HA	4.54	3.73	11.0	well installed
/S 8-MM	5/14/91	19.35	COE	HSA/HA	3.61	3.47	11.0	well installed
MW-10 5/7	5/7-13/91	19.00	COE	HSA/HA	4.34	4.34	11.0	well installed
MW-11 5/	5/14/91	18.95	COE	HSA/HA	3.98	3.40	11.0	well installed
A-1 5	5/6/91	19.35	COE	НА	5.00	3.63	6.0	
A-2 5	5/6/91	19.62	COE	HA	3.55	3.31	5.0	
A-3 5,	5/6/91	18.97	COE	НА	4.00		5.0	hole caved
A-4 S	16/1/5	18.79	COE	НА	6.41		8.0	hole caved

				TABLE 1				
			Summary of S Hun Buil	of Soil Boring Constru Hunter Army Airfield Building No. 710 Area	Summary of Soil Boring Construction Data Hunter Army Airfield Building No. 710 Area			
		7 / H	Job No. 1	Savannan, Georgia Job No. 10675, Report No. 53855	na Vo. 53855			Page 2 of 2
	Date	Elevation Land Surface (ft - MSL)	Driller	Drill Method	Initial Depth to Water (ft)	24-Hour Water Level Reading (ft)	Boring Depth (ft)	Comments
-	5/7/91	19.10	COE	HA	4.38	4.40	6.0	
	5/2/91	18.58	COE	НА	-	I	8.0	hole caved; well not installed
\rightarrow	5/8/91	19.06	COE	ЧY	3.56	3.75	6.0	
	5/7/91	18.08	COE	HA	4.15	2.15	6.0	
	5/8/91	18.66	COE	HA	4.78	4.27	6.0	
	5/7/91	18.08	COE	HSA HA	4.15	2.61	6.0	well not installed

ABBREVIATIONS:

Fea Mean Sea Level Corps of Engineas Hollow Stem Auger Hand Auger FT MSL COE HSA HA

TABLE 2

Organic Vapor Concentrations Hunter Army Airfield Building No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855

Page 1 of 3

Boring Number	Date	Depth (feet)	Organic Vapor Concentrations (ppm)
MW-710-1 (MW - 1)	5/1/91	0.4 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	>1000 >1000 >1000 >1000 >1000
MW-710-3 (MW - 3)	5/2/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0 5.5 - 6.0	0.0 0.0 0.0 0.0 0.0 5.0
MW-710-4 (MW - 4)	5/2/91	0.6 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	600 >1000 >1000 880 980
MW-710-5 (MW - 5)	5/3/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	0.2 0.0 0.0 0.0 0.0
MW - 6	5/14/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	0.2 6.0 22.0 6.2 10.0
MW - 7	5/13/91	0.4 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	1.0 300.0 >1000 250.0 20.0
) MW - 8	5/14/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	200 >1000 200 >1000 200

TABLE 2

Organic Vapor Concentrations Hunter Army Airfield Building No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855

Page 2 of 3

Boring Number	Date	Depth (feet)	Organic Vapor Concentrations (ppm)
MW - 10	5/7/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	0.0 0.0 0.0 0.0 0.0
MW - 11	5/15/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	0.0 0.0 0.0 0.0 740.0
) A - 1	5/6/91	1.0 1.5 2.0 - 2.5 3.0 - 3.5 4.0 - 4.5 5.0 - 5.5	150.0 40.0 10.0 2.0 0.0
A - 2	5/6/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.0 - 4.5	0.0 0.0 0.0 0.0 0.0
A - 3	5/6/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	0.0 0.0 0.0 0.0 0.0
A - 4	5/7/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0 5.5 - 6.0	0.0 0.0 0.0 0.0 220.0 80.0
) A - 5	5/7/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0 5.0 - 6.0	0.0 0.0 >1000 800.0 30.0 30.0

TABLE 2

Organic Vapor Concentrations Hunter Army Airfield Building No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855

Page 3 of 3

Boring Number	Date	Depth (feet)	Organic Vapor Concentrations (ppm)
A - 6 (MW-710-2) [MW - 2]	<i>5/2/</i> 91	0.4 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	>1000 >1000 >1000 >1000 >1000 740.0
A - 7	5/8/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	0.0 0.0 0.0 0.0 0.2
) A-9	<i>5/7/</i> 91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	0.0 0.2 0.8 1.0 25.0
A - 10	5/8/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0 5.5 - 6.0	0.0 0.0 0.0 0.0 0.0 0.0
A - 11	5/7/91	0.5 - 1.0 1.5 - 2.0 2.5 - 3.0 3.5 - 4.0 4.5 - 5.0	0.0 0.0 3.0 500.0 85.0

NOTE:

Organic vapors detected with an organic vapor analyzer.

ABBREVIATIONS AND SYMBOLS:

ppm

Parts Per Million

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Greater Than

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[2]	
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Summary of Well Construction Data Hunter Army Airfield Building No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855

Elevation Elevation, Casing Casing Casing Casing Casing Cit - MSL) Drill Casing Casing Cit - MSL) Casing Casing Cit - MSL) Method Cit - MSL) Cit - MSL) (finches) (fit) 18.76 18.56 HSA/HA 2 8.0 8.0 19.13 18.85 HSA/HA 2 8.0 12.5 1 17.85 17.65 HSA/HA 2 11.0 11.0 1 17.85 17.65 HSA/HA 2 11.0 11.0 1 18.18 18.68 HSA/HA 2 11.0 11.0 1 19.35 19.11 HSA/HA 2 11.0 11.0 1 19.35 19.11 HSA/HA 2 11.0 11.0 1 19.00 18.80 HSA/HA 2 11.0 11.0 1 19.35 19.11 HSA/HA 2 11.0 11.0 1 19.00 HSA/HA 2 11.0 11.0 11.0 1 19.55											
5/1/91 18.76 18.56 HSA/HA 2 8.0 5/2/91 19.13 18.85 HSA/HA 2 8.0 5/2/91 19.15 19.00 HSA/HA 2 12.5 5/3-6/91 17.85 17.65 HSA/HA 2 11.0 5/14/91 21.05 20.79 HSA/HA 2 11.0 5/14/91 19.35 19.11 HSA/HA 2 11.0 5/14/91 19.00 18.80 HSA/HA 2 11.0 5/14/91 19.00 18.80 HSA/HA 2 11.0	Well No.	Date	Elevation Land - Surface (ft - MSL)	Elevation, Top of Casing (ft - MSL)	Drill Method	Casing Diameter (inches)	Boring Depth (ft)	Well Depth (ft)	Screened Interval (ft)	Driller	Comments
5/2/91 19.13 18.85 HSA/HA 2 8.0 5/2/91 19.15 19.00 HSA/HA 2 12.5 5/3-6/91 17.85 17.65 HSA/HA 2 11.0 5/14/91 21.05 20.79 HSA/HA 2 11.0 5/14/91 19.35 19.11 HSA/HA 2 11.0 5/14/91 19.00 18.80 HSA/HA 2 11.0 5/14/91 19.00 18.80 HSA/HA 2 11.0	MW-1	5/1/91	18.76	18.56	HSA/HA	2	8.0	7.5	2.5-6.5	COE	
5/2/91 19.15 19.00 HSA/HA 2 12.5 5/3-6/91 17.85 17.65 HSA/HA 2 11.0 5/14/91 21.05 20.79 HSA/HA 2 11.0 5/13/91 18.18 18.68 HSA/HA 2 11.0 5/14/91 19.35 19.11 HSA/HA 2 11.0 5/14/91 19.00 18.80 HSA/HA 2 11.0 5/14/91 18.95 HSA/HA 2 11.0	MW-3	5/2/91	19.13	18.85	HSA/HA	2	8.0	7.5	2.5-6.5	COE	
5/3-6/91 17.85 HSA/HA 2 11.0 5/14/91 21.05 20.79 HSA/HA 2 11.0 5/13/91 18.18 18.68 HSA/HA 2 11.0 5/14/91 19.35 19.11 HSA/HA 2 11.0 5/14/91 19.00 18.80 HSA/HA 2 11.0 5/14/91 18.95 HSA/HA 2 11.0	MW-4	5/2/91	19.15	19.00	HSA/HA	2	12.5	12.5	25-11.25	COE	
5/14/91 21.05 20.79 HSA/HA 2 11.0 5/13/91 18.18 18.68 HSA/HA 2 11.0 5/14/91 19.35 19.11 HSA/HA 2 11.0 5/14/91 19.00 18.80 HSA/HA 2 11.0 5/14/91 18.95 HSA/HA 2 11.0	MW-5	5/3-6/91	17.85	17.65	HSA/HA	2	11.0	10.0	2.5-9.25	COE	
5/13/91 18.18 18.68 HSA/HA 2 11.0 5/14/91 19.35 19.11 HSA/HA 2 11.0 5/14/91 19.00 18.80 HSA/HA 2 11.0 5/14/91 18.95 HSA/HA 2 11.0	MW-6	5/14/91	21.05	20.79	HSA/HA	2	11.0	10.0	2.5-9.25	COE	
5/14/91 19.35 19.11 HSA/HA 2 11.0 5/7-13/91 19.00 18.80 HSA/HA 2 11.0 5/14/91 18.95 18.55 HSA/HA 2 11.0	MW-7	5/13/91	18.18	18.68	HSA/HA	2	11.0	10.0	2.5-9.25	COE	
5/7-13/91 19.90 18.80 HSA/HA 2 11.0	MW-8	5/14/91	19.35	19.11	HSA/HA	2	11.0	10.0	25-9.25	COE	
5/14/91 18.95 18.55 HSA/HA 2 11.0	MW-10	5/7-13/91	19.00	18.80	HSA/HA	2	11.0	10.0	25-9.25	COE	
V. 11.0	MW-11	5/14/91	18.95	18.55	HSA/HA	2	11.0	10.0	2.5-9.25	COE	

ABBREVIATIONS:

Feet
Mean Sea Level
Corps of Engineers
Hollow Stem Auger FT MSL COE HSA HA

TABLE 4

Summary of Fluid Level Measurements Hunter Army Airfield Building No. 710 Area Savannah, Georgia

Job No. 10675, Report No. 53855

Well No.	Date	Elevation Top of Casing (ñ - MSL)	Depth to Water (ft)	Liquid Hydrocarbon Thickness (ft)	Water Level Elevation (π - MSL)	Corrected* Water Level Elevation (ft - MSL)
MW - 1	8/29/91	18.56	3.86	0.61	14.70	15.16
MW - 3	8/29/91	18.85	3.22	0.00	15,63	15.63
MW - 4	8/29/91	19.00	3.11	0.00	15.89	15.89
MW - 5	8/29/91	17.65	2.95	0.00	14.70	14.70
fW - 6	8/29/91	20.79	2.89	0.00	17.90	17.90
MW - 7	8/29/91	18.68	2.68	0.00	16.00	16.00
MW - 8	8/29/91	19.11	2.65	0.00	16.46	16.46
MW - 10	8/29/91	18.80	3.70	0.00	15.10	15.10
MW - 11	8/29/91	18.55	2.31	0.00	16.24	16.24

NOTE: *

Corrected groundwater level elevation equation: water level elevation + (0.75 x liquid hydrocarbon thickness). 0.75 = specific gravity of gasoline.

ABBREVIATIONS:

ft

Feet

MSL

Mean Sea Level

TABLE 5

Summary of Hydraulic Conductivity Data Hunter Army Airfield Building No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855

Well Number	Soil Type	K-Hydraulic Conductivity (ft/min)
MW - 1	Silty Sand	2.5 x 10 ⁻³
MW - 4	Silty Sand	1.7 x 10 ⁻³
MW - 5	Silty Sand	3.1 x 10 ⁻³
MW - 6	Silty Sand	2.2 x 10 ⁻³
MW - 7	Poorly Graded Sand	1.8 x 10 ⁻³
MW - 8	Clayey Sand	1.4 x 10 ⁻³
MW - 11	Inorganic Silt	0.9 x 10 ⁻³

Average: 1.9 x 10⁻³

) [TABLE 6			41	
			Summai Hui Buli Sa Job No. 1	Summary of Soil Quality Data Hunter Army Airfield Building No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855	ty Data eld rea ia io. 53855			Page 1 of 3
				SAMPLE ID	LE ID			
	MW-710-1-1	MW-710-3-1	MW-710-4-1	MW-710-5-1	MW-6-1	MW-7-1	MW-7-1-C	MW-8-1
BORING NO.	WW-I	MW-3	MW-4	MW-5	9-WW	MW-7	7-WW	MW-\$
PARAMETERS*								
Depth (feet)	3.5 - 4.0	2.5 - 3.0	2.5 - 3.0	2.5 - 3.0	2.5 - 3.0	3.0 - 3.5	3.5 - 4.0	3.0 - 3.5
Date	5/1/91	5/2/91	5/2/91	16/6/5	5/14/91	5/13/91	5/13/91	5/14/91
OVA Reading	> 1,000	0.0	> 1,000	0.0	22.0		250.0	1
Benzene	150	BDL	0.200	BDL	BDL	BDL	BDL	0.0410
Toluene	2,200	BDL	0.073	BDL	0.015	0.0180	BDL	0.1600
Ethylbenzene	1,200	BDL	BDL	BDL	BDL	BDL	BDL	0.0091
Xylenes	4,500	BDL	0.830	BDL	0.011	0.0068	BDL	0.0780
Total BTEX	8,050	BDL	1.103	BDL	0.026	0.0248	BDL	0.2881
ТРН	25,000	14	34	46	21	066	42	310
Lead	7.9	3.4	6.7		4.9	1		

NOTE: * All parameter concentrations reported in mg/kg (ppm), unless otherwise stated.

ABBREVIATIONS:

Below Detection Limit
Parts Per Million
Total Petroleum Hydrocarbon
Benzene, Toluene, Ethylbenzene, & Xylenes BDL ppm TPH BTEX

Greater Than Not Analyzed

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SYMBOLS:

)			SALE SALES S	TABLE 6				
			Summa Hu Bui Si Job No.	Summary of Soil Quality Data Hunter Army Airfield Building No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855	ity Data ield krea ia vo. 53855			Page 2 of 3
				SAMP	SAMPLE ID			
	MW-10-1	MW-11-1	MW-11-2	A-1-1	A-2-1	A-3-I	A-4-1	A-4-2
BORING NO.	MW-10	MW-11	MW-11	A-1	A-2	A-3	V-7	V-V
PARAMETERS*								
Depth (feet)	4.5 - 5.0	3.5 - 4.0	5.0 - 5.5	3.0 - 3.5	3.0 - 3.5	3.0 - 3.5	3.5 - 4.0	45-5.0
Date	5/1/91	5/15/91	5/15/91	5/6/91	5/6/91	5/6/91	57/91	5/1/91
OVA Reading	0.0	0.0		10.0			0.0	220.0
Benzene	BDL	BDL	0.048	BDL	BDL	BDL	BDL	BDL
Toluene	BDL	BDL	0.019	BDL	BDL	BDL	BDL	BDL
Ethylbenzene	BDL	BDL	BDL	BDL	BDL	BDL	BDL	BDL
Xylenes	BDL	BDL	0.660	BDL	BDL	BDL	BDL	BDL
Total BTEX	BDL	BDL	0.727	BDL	TOB	BDL	BDL	BDL
ТРН	49	20	36	21	BDL	74	12	18
Lead		desirab	ı	-	• 11			

NOTE: * All parameter concentrations reported in mg/kg (ppm), unless otherwise stated.

ABBREVIATIONS:

SYMBOLS:

Greater Than Not Analyzed ٨٦

Below Detection Limit
Parts Per Million
Total Petroleum Hydrocarbon
Benzene, Toluene, Ethylbenzene, & Xylenes

BDL ppm TPH BTEX

)				TABLE 6	JE 6			
			·	Summary of Soil Quality Data Hunter Army Airfield Building No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855	il Quality Data ny Airfield b. 710 Area Georgia eport No. 53855			Page 3 of 3
					SAMPLE ID			
	V	A-5-1	MW-710-2-1	A-7-I	A-9-1	A-10-1	MW-9-1	MW-9-2
BORING NO.		A-5	A-6	A-7	6-Y	A-10	A-11	A-11
PARAMETERS.								
Depth (feet)	3.5	3.5 - 4.0	2.5 - 3.0	3.5 - 4.0	2.5 - 3.0	3.5 - 4.0	2.5 - 3.0	3.5 - 4.0
Date	5/1/91	5/14/91	5/2/91	5/8/91	5/7/91	5/8/91	5/1/91	5/7/91
OVA Reading	800.0	ı	> 1,000.0	0.0	0.8	0.0	3.0	200.0
Веплепе	1.10	BDL	1.4	BDL	BDL	BDL	BDL	BDL
Toluene	0.41	BDL	1.6	BDL	BDL	BDL	BDL	BDL
Ethylbenzene	BDL	BDL	4.9	BDL	BDL	BDL	BDL	BDL
Xylenes	BDL	BDL	3.0	BDL	BDL	Тая	BDL	BDL
Total BTEX	1.51	BDL	10.9	BDL	BDL	TOS	BDL	BDL
ТРН	28	15	1,400	13	46	19	26	18
Lead	-	18		a.i.a.		1	-	1

NOTE: * All parameter concentrations reported in mg/kg (ppm), unless otherwise stated.

ABBREVIATIONS:

SYMBOLS:

۰.،

Greater Than Not Analyzed

Below Detection Limit
Parts Per Million
Total Petroleum Hydrocarbon
Benzene, Toluene, Ethylbenzene, & Xylenes

BDL ppm TPH BTEX

TABLE 7	Summary of Water Quality Data Hunter Army Airfield	Dunding No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855
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					SAMPLE ID	LE ID				
	MW-1-I	MW-3-1	MW-4-1	MW-5-1	MW-6-1	1-1-MW	MW-7-1C	MW-8-1	MW-10-1	MW-11-1
WELL NO.	MW-1	MW-3	MW-4	MW-5	MW-6	MW-7	MW-7	MW-8	MW-10	MW-11
PARAMETERS*										
Date	5/29/91	5/28/91	5/29/91	5/28/91	5/28/91	5/29/91	5/29/91	5/29/91	16/87/5	5/29/91
Benzene	5,200	22	009	TOE	BDL	BDL	BDL	38	BDL	9.2
Toluene	22,000	BDL	5.8	TOS	BDL	BDL	BDL	2.4	BDL	16.0
Ethylbenzene	3,800	BDL	26	IDE	BDL	BDL	BDL	BDL	BDL	17.0
Xylenes	17,000	BDL	170	BDL	1.5	BDL	BDL	BDL	BDL	27.0
Total BTEX	48,000	22	801.8	TOS	1.5	BDL	BDL	41.3	BDL	69.2
TPH (ppm)	55	BDL	BDL	BDL	BDL	1.9	BDL	2.9	BDL	BDL
Lead (ppm)	0.038		BDL	-	BDL	ı	ı	-	i	

NOTE: • All parameters reported in parts per billion, unless otherwise stated.

ABBREVIATIONS:

Below Detection Limits Total Petroleum Hydrocarbons Parts Per Million BDL TPH ppm

TABLE 8

Summary of Water System Survey Data Hunter Army Airfield Building No. 710 Area Savannah, Georgia Job No. 10675, Report No. 53855

Map Number	Well Owner and Number	Information Source	Depth of Well (ft)	Bottom of Casing (ft)	Discharge (GPM)	Primary Use of Water	Comments
1	Hunter Army Airfield #1	HAA/USGS	504	259	1300	Public	
2	Hunter Army Airfield #2	HAA/USGS	555	260	1440	Public	
3	Hunter Army Airfield #3	HAA/USGS	370	324	30	Public	
4	Hunter Army Airfield #4	HAA/USGS	300	90		Not Used	
4A	Hunter Army Airfield #4A	HAA/USGS	360	267	80	Public	
5	Hunter Army Airfield #5	НАА	380	85	30	Public	Outside 3-mile radius
)	Hunter Army Airfield #6	HAA/USGS	180			Not Used	
7	Hunter Army Airfield #7	НАА	450	330	70	Public	Outside 3-mile
8	Hunter Army Airfield #8	HAA/USGS	375	255	80	Public	Outside 3-mile
9	Hunter Army Airfield #9	HAA/USGS	623	270	1000	Emergency	
10	Hunter Army Airfield #10	HAA			180	Vehicle Wash	
11	City of Savannah #15	USGS/C of S	414	252	1000	Public	USGS has well listed as #36
12	Mrs. McCallan	USGS	341	146		Public	
13	Biltmore Gardens Mobile Home Park	USGS/Owner	380	290	150	Public	
14	City of Savannah #25	USGS/C of S	540	287	1100	Public	
15	City of Savannah #13	USGS/C of S	1000	270	1300	Public	
16	City of Savannah #9	USGS/C of S	710	267	1600	Public	
17	City of Savannah #6	USGS/C of S	750	240	1400	Public	

NOTE: Map Well Numbers correspond to Plates 8 and 9.

ABBREVIATIONS AND SYMBOLS:

Ft Feet

GPM Gallons Per Minute HAA Hunter Army Airfield United States Geological Survey

USGS C of S City of Savannah C-1 - TRACER TIGHT™ LEAK TEST REPORT
 C-2 - SHALLOW SOIL GAS INVESTIGATION REPORT
 C-3 - DRILLING LOGS AND HTW LOG FOR BORING T-1 (A-3)

C-1 - TRACER TIGHT TM LEAK TEST REPORT

Tracer Research Corporation

Tracer TightTM LEAK TEST
FOUR UNDERGROUND STORAGE TANKS
HUNTER ARMY AIR FIELD
SAVANNAH, GEORGIA

MARCH 1990



TRACER TIGHT TANK TESTS

Tracer Tight leak testing is performed by mixing a tracer, a volatile chemical concentrate, with the product inside of a tank or pipe. If the product leaks out of the system the tracer escapes from the liquid product by evaporation. The tracer vapors are released into the soil and migrate in all directions from the leak through the soil porosity. Special probes or tubing are placed in the soil near the tanks and pipes to collect the tracer vapors that will appear in the soil in the event of a leak. The vapors are collected from the soil and analyzed for the presence of tracer by means of an extremely sensitive chromatographic measurement. The tracer is added to the product in very low concentrations typically only a few ppm. Thus, it has no impact on the physical properties of the product. The tracer vapors can be detected in the low parts per trillion level in the soil. For this reason the method is capable of detecting very small leaks in the tanks and pipes.

The tracer chemical, being highly volatile, distributes itself into both the fuel and the vapor space above the fuel inside the tank. Because of its ability to escape through leaks in the vapor space of a partially full tank, there is no requirement to top-off tanks with fuel before testing.

There are several fundamental advantages to the non-volumetric Tracer Tight test over the volumetric testing approach. First, the use of the Tracer Tight method will provide leak testing with a much greater degree of convenience and assurance. For example, the tracer method is completely non-disruptive to normal operations involving the tanks. Two weeks prior to testing, a tracer is released into the product inside the tank. Only normal fuel usage is required to distribute the tracer throughout the entire system. No addition of fuel to top off the tank is required. No additional personnel are required to coordinate the day to day activities of the leak detection operations. All leaks are typically identified and located without any tank modifications or digging. As a sult the Tracer Tight method is much more convenient to both the tank users and contract administrators than volumetric tank testing.

The Tracer Tight method will also bring much greater assurance of quality than volumetric testing. The TRC method, like other vapor detection methods, is known to be a quantum leap beyond volumetric methods in terms of sensitivity. For example, when the U.S. Army Corps of Engineers evaluated the Tracer Tight method along with several volumetric methods at March AFB in June 1986, TRC detected and quantified leakage simulated as low as 0.0003 gallons per hour.

Because variables such as tank size, thermal expansion of fuel, air pockets, or other variables that effect volumetric methods, do not impact the tracer testing method, the results are far less ambiguous. Therefore, the greater sensitivity coupled with absence of potentially misleading variables makes the tracer method the most accurate and most quality assured method available.

EQUIPMENT

TRC has designed and built a fleet of field vehicles that are capable of sampling and performing all chemical analyses on-site. The TRC analytical field vehicles are normally operated by a two-person crew consisting of a GC operater and a field assistant. A list of equipment used by TRC in a leak detection investigation is given below.

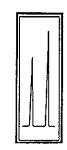
(A) General Equipment

- . One ton Ford E350 chassis, van or flatbed
- . Onan 5 kW gasoline powered generators (110 volt/AC)
- . Hydraulic pusher/puller/pounder mechanism capable of driving probes 20 feet deep in some soils
- . Evacuation probes fabricated from a galvanized pipe
- . Safety Equipment: first aid, fire, hazardous chemical protection
- . Two vacuum pumps
- . A pneumatic rock drill capable of drilling through asphalt and concrete pads



(B) Gas Chromatographic Equipment In Each Van

- . Two (2) Varian 3300 gas chromatographs
- . Two Spectra-Physics model SP4270 computing integrators
- . Electron capture, flame ionization, photo ionization and thermo conductivity detectors on the various GCs.
- . Analytical standards for tracers and petroleum hydrocarbons, pure compounds obtained from Chemservice Inc. of West Chester, Pennsylvania
- . Glass syringes ranging from 10 ul to 10 ml in volume
- . Various packed and capillary gas chromatographic columns
- . Gas cylinders containing compressed nitrogen, air and hydrogen
- . 40 ml glass sampling vials in which the chemical standards are prepared
- . Various fittings and tools required for normal operation



PREPARED FOR:

Card Smith Army Corps of Engineers 100 W. Oglethorde Savannah, Georgia 31401 (912)944-5674

Tracer TightTM LEAK TEST FOUR UNDERGROUND STORAGE TANKS HUNTER ARMY AIR FIELD SAVANNAH, GEORGIA

MARCH 1990

SUBMITTED BY:

TRACER RESEARCH CORPORATION

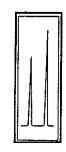
COEHAAF.REP 1-90-156-T

Tracer Research Corporation



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INTRODUCTION

Tracer Research Corporation (TRC) performed Tracer TightTM leak testing of four underground storage tanks at Hunter Army Air Field located in Savannah, Georgia. Tracer was added to the tanks in February 1990 and testing was conducted on March 14, 1990. Testing was performed under contract to the Army Corps of Engineers, Savannah District.

CONCEPT OF OPERATION AND IMPLEMENTATION

The tracer leak detection method relies upon the addition of a highly volatile liquid chemical to the fuel. If a leak occurs in the underground fuel system, fuel is released into the surrounding soil. The tracer escapes from the fuel by vaporization and disperses into the soil by molecular diffusion. Various means are used to sample the soil vapors in the immediate vicinity of the underground tanks and pipes. In this case, sampling was performed by driving probes into the ground in the vicinity of the tanks and pipes. Each probe has an effective detection radius of approximately 10 to 12 feet. This means that a given probe should detect a leak anywhere within the area described by the 10 foot radius around the probe. The tracer is placed in the tank at least two weeks prior to the probe sampling for this method to be effective. This process of leak detection by placing a liquid tracer in a liquid product followed by detection of the tracer underground in the vapor phase is protected under TRC patents.

BACKGROUND ON VAPOR LEAK DETECTION METHODS

TRC has developed several different tracer methods for leak testing underground fuel systems. These include rapid tests for all sizes of tanks that require circulation of tracer with fuel inside the tank and high volume evacuation of air from the backfill around the tank. The rapid tests are relatively costly because they are labor and equipment intensive. However, the method has the advantages of providing relatively fast and sensitive leak location and quantification.



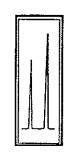
As priorities and requirements for tank testing have evolved in the past five years, the need to quantify the leak rate has been deemphasized and both "passive" and "aspirated" vapor leak detection systems have been gaining acceptance, particularly in the western United States. Passive leak detection refers to methods where the vapors move to the sensor or pick-up probes entirely by molecular diffusion. Aspirated leak detection refers to methods where soil air is continuously drawn or evacuated through the pick-up probe to aid transport of vapors. Both methods are equally sensitive but more probes are required to cover the same area using the passive method as compared to the aspirated method. However, the installation cost of the passive method is much lower.

Vapor methods are typically much more sensitive than the volumetric methods for leak detection. With the exception of the TRC leak detection method, all other vapor methods are dependent on product vapors themselves to detect leakage. This means that low volatility fuels such as kerosene, diesel or heating oil present problems due to their low vapor pressures. Conventional vapor methods that rely on product vapors commonly encounter problems distinguishing between existing leaks and previous spills. By adding tracer to the tank, the volatility of the product becomes unimportant because the tracer becomes the volatile component used to detect leakage.

The tracer is present in the product only in very low part per million concentrations. For this reason the tracer does not impact the physical properties or use of the product. The method requires extremely selective and sensitive detection ability for the tracer. Typically, the tracers are detected in the low part per trillion range. Due to the sensitivity of the detection, the tracer can be used economically to test even multimillion gallon tanks with no reduction in sensitivity.

Tracer is not normally present in or around the tank before the leak test begins. As a result, there is no potential confusion between present leakage and previous spills. Several tracers are available for general use. This means that a given tank or system can be retested several times, each time with a different tracer to resolve special problems and provide completely unambiguous conclusions about the system integrity.

Tracer Research Corporation



TRC has emphasized development of the passive leak detection technology because of the simplicity and reliability of this approach.



TESTING RESULTS

Testing was performed on two underground storage tanks at Hunter Army Air Field Fire Station. One 1,500 gallon diesel tank (Tank A) was inoculated with DDM tracer and one 1,000 gallon gasoline tank (Tank B) was inoculated with 114B2 tracer. The target concentration of tracer in each of the four tanks was approximately 10 ppm.

A total of two vapor samples were collected next to each tank. Samples were collected at depths ranging from three to six feet. A map showing the orientation of the tanks and sampling locations is included in Appendix A (Figure 1). Samples were analyzed for DDM, 114B2, and total petroleum hydrocarbons, which are reported C4-C9 aliphatic, alicyclic and aromatic compounds. Data from the sample analyses are reported in Appendix B. The tracers were not detected in any of the four sampling locations. The hydrocarbon concentrations were non-detectable except for sampling location A-1 which had a concentration of 0.9 ug/L. These data indicate that Tanks A and B do not leak.

Testing was also performed on two 12,000 gallon tanks at Hunter Army Air Field Building 710. The gasoline tank (Tank C1) was inoculated with DDM tracer and the diesel tank (Tank C2) was inoculated with 114B2 tracer. A total of six vapor sampling locations were placed in the vicinity of Tanks C1 and C2 as shown in Figure 2. Samples were collected at depths ranging from two to three feet below grade. Vapor samples were not collected below three feet due to the presence of water.

Low concentrations of 114B2 tracer were detected in vapor collected at sampling locations C-1,2,3,4 and 6 at depths of two to three feet below grade. Samples could not be collected at greater depths due to the presence of groundwater below two feet. The DDM tracer was not detected in any of the sampling locations placed in the vicinity of the tanks. Hydrocarbons were detected at very high concentrations ranging from 310,000 to 1,200,000 ug/L. The distribution of hydrocarbons is greater than 200 square feet total area. The tracer data indicates that Tank C2 has a small or intermittent product leak. Due to the excessively high levels of hydrocarbons detected, the tanks should be closely monitored.



CERTIFICATION

Location:

Hunter Army Air Field

Savannah, Georgia

Date: March 1990

<u>Tank</u>	Capacity (gal)	Product	<u>Tracer</u>	Pass/Fail	Leak Status
Tank A	1,500	diesel	DDM	Pass	1
Tank B	1,000	gasoline	114B2	Pass	1
Tank C1	12,000	gasoline	DDM	Pass	1
Tank C2	12,000	diesel	114B2	Fail	3

Tracer Research Corporation certifies that the tanks and pipe systems listed in the above table have been tested by means of Tracer TightTM, which meets the criteria set forth in NFPA 329 for a precision leak test.

Submitted by:

Tracer Research Corporation

The following criteria are used for the classification of leaks when tracer is detected.

LEAK STATUS

- NO LEAKAGE Rate less than 0.005 gallons per hour.
- 2 <u>VAPOR LEAK</u> Maximum tracer concentration less than 1 ug/L in soil vapor diminishing at depths below three feet. Total volatile hydrocarbon concentrations less than 20,000 ug/L in soil vapor (if diesel is the only fuel present, substitute 100 ug/L in place of 20,000 ug/L).
- 3 SMALL OR INTERMITTENT PRODUCT LEAK less than 0.05 gph -Maximum tracer concentration less than 1 ug/L in soil vapor, sustaining or increasing at depths below three feet or to the top of the groundwater table. Hydrocarbon concentrations approximately equal to or greater than 20,000 ug/L in soil vapor (100 ug/L for diesel) sustaining or increasing below three feet. Distribution of elevated hydrocarbons is less than 200 square feet total area.
- SIGNIFICANT PRODUCT LEAK 0.05 gph or greater Maximum tracer concentration greater than 1 ug/L near source, increasing or sustaining concentration below three feet or to the top of the groundwater table. Hydrocarbon concentrations greater than 20,000 ug/L in soil vapor (100 ug/L for-diesel) sustaining or increasing below three feet. Distribution of elevated hydrocarbons is equal to or greater than 200 square feet total area.

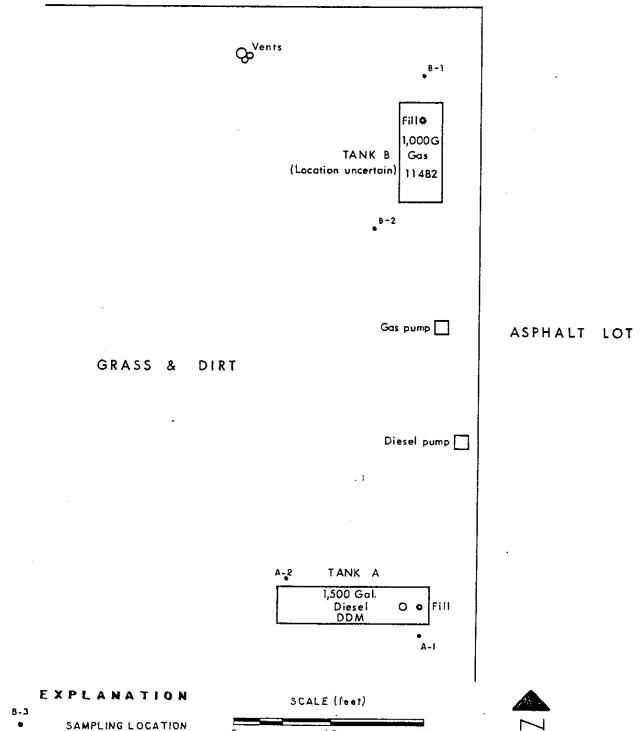
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APPENDIX A: FIGURES

FIGURE 1 SAMPLING LOCATIONS AIRFIELD FIRE STATION PUMPS

Army Corps Of Engineers Ft. Stewart Savannah, Georgia

ASPHALT ROAD



10

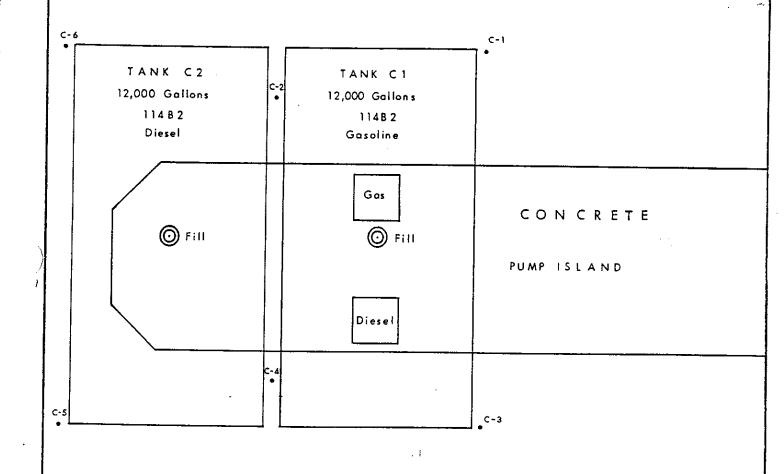
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FIGURE 2
SAMPLING LOCATIONS
BUILDING No. 710

Army Corps Of Engineers Ft. Stewart Savannah, Georgia

CONCRETE

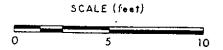


CONCRETE

EXPLANATION

C-3

SAMPLING LOCATION





Tracer Research Corporation



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APPENDIX B: ANALYTICAL RESULTS

CORPS OF ENGINEERS/HUNTER FIELD-FT.STEWART/SAVANNAH, GEORGIA	J08#1-90-156-T
CONDENSED DATA	

<u>:--</u>

ž.

THC ug/1	<0.2 0.9 0.4	0.2 0.2 0.2	<0.2 496000 642000	1210000 632000 328000	312000 N/A N/R	E E
114B2 ug/1	<0.00005 <0.00005 <0.00005	<0.00005 <0.00005 <0.00005	<0.00005 0.005 0.006	0.006 0.004 <0.00005	0.0001 <0.0002 0.009	17 0.04
DDM ug/1	<0.00004 <0.00004 <0.00004	<0.00004 <0.00004 <0.00004	<0.00004 <0.00004 <0.00004	<0.00004 <0.00004 <0.00004	<0.00004 5 0.1 5 <0.0002	0.004
SAMPLE	AIR A-1-4' A-1-6'	A-2-3, B-1-3, B-2-3,	B-2-6, C-1-3, C-2-2,	C-3-2, C-4-3, C-5-3,	C-6-2' TANK C-1-HS TANK C-2-HS	TANK B-HS TANK A-HS

. 1

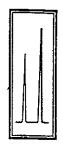
N/A not analyzed

Analyzed by: K. Ptak Checked by: A. Hooper Proofed by: C-2 - SHALLOW SOIL GAS INVESTIGATION REPORT

Tracer Research Corporation

SHALLOW SOIL GAS INVESTIGATION HUNTER ARMY AIR FIELD BUILDINGS 133 AND 710 SAVANNAH, GEORGIA

JULY 1990



PREPARED FOR:

U.S. Army Corps of Engineers Savannah District 100 West Oglethorpe Avenue Savannah, Georgia 31402-0889 (912)944-5674

> SHALLOW SOIL GAS INVESTIGATION HUNTER ARMY AIR FIELD BUILDINGS 133 AND 710 SAVANNAH, GEORGIA

> > **JULY 1990**

SUBMITTED BY:

Tracer Research Corporation

384HAAFMSG 1-36-384**-S**

Tracer Research Corporation



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ANALYTICAL PROCEDURES	4
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INTRODUCTION

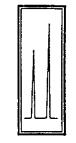
A shallow soil gas investigation was performed by Tracer Research Corporation (TRC) at Hunter Army Air Field located in Savannah, Georgia. The investigation was conducted on July 11-12, 1990 under contract to the Army Corps of Engineers, Savannah District. The purpose of the investigation was to delineate the areal extent of hydrocarbon contamination in the subsurface at two site locations (Building 133 and 710).

During this survey, a total of twenty-one soil gas samples were collected and analyzed. Samples were analyzed for volatile organic compounds from the following suite:

benzene
toluene
ethylbenzene
xylenes
total hydrocarbons (THC)

Xylenes are reported as the total of the three xylene isomers and total hydrocarbons are reported as gasoline range compounds consisting of approximately C_4 - C_9 aliphatic, alicyclic and aromatic compounds.

The compounds in this suite were chosen as target compounds because of their suspected presence in the subsurface and amenability to soil gas technology. Soil gas samples were screened on a gas chromatograph equipped with a flame ionization detector (FID).



SHALLOW SOIL GAS INVESTIGATION - METHODOLOGY

Shallow soil gas investigation refers to a method developed by TRC for investigating underground contamination from volatile organic chemicals (VOCs) such as industrial solvents, cleaning fluids and petroleum products by looking for their vapors in the shallow soil gas. The method involves pumping a small amount of soil gas out of the ground through a hollow probe driven into the ground and analyzing the gas for the presence of volatile contaminants. The presence of VOCs in shallow soil gas indicates the observed compounds may either be in the vadose zone near the probe or in groundwater below the The soil gas technology is most effective in mapping low molecular weight probe. halogenated solvent chemicals and petroleum hydrocarbons possessing high vapor pressures and low aqueous solubilities. These compounds readily partition out of the groundwater and into the soil gas as a result of their high gas/liquid partitioning coefficients. Once in the soil gas, VOCs diffuse vertically and horizontally through the soil to the ground surface where they dissipate into the atmosphere. The contamination acts as a source and the above ground atmosphere acts as a sink, and typically a concentration gradient develops between the two. The concentration gradient in soil gas between the source and ground surface may be locally distorted by hydrologic and geologic anomalies (e.g. clays, perched water); however, soil gas mapping generally remains effective because distribution of the contamination is usually broader in areal extent than the local geologic barriers and is defined using a large data base. The presence of geologic obstructions on a small scale tends to create anomalies in the soil gas-groundwater correlation, but generally does not obscure the broader areal picture of the contaminant distribution.

Soil gas contaminant mapping helps to reduce the time and cost required to delineate underground contamination by volatile contaminants. The soil gas investigation does this by outlining the general areal extent of contamination. Conventional bore holes or observation wells are used to verify both the presence and extent of the subsurface contamination as indicated in the soil gas survey. In this manner, soil gas contaminant mapping can assist in determining the placement of monitoring wells. Thus, the likelihood



of drilling unnecessary monitoring wells is reduced. The soil gas survey is not intended to be a substitute for conventional methodology, but rather to enable conventional methods to be used efficiently.

EQUIPMENT

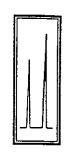
Tracer Research Corporation utilized a one ton Ford analytical field van that was equipped with one gas chromatograph and two Spectra Physics computing integrators. In addition, the van has two built-in gasoline powered generators that provide the electrical power (110 volts AC) to operate all of the gas chromatographic instruments and field equipment. A specialized hydraulic mechanism consisting of two cylinders and a set of jaws was used to drive and withdraw the sampling probes. A hydraulic hammer was used to assist in driving probes past cobbles and through unusually hard soil.

SAMPLING PROCEDURES

Sampling probes consist of 7 foot lengths of 3/4 inch diameter hollow steel pipe that are fitted with detachable drive tips. Soil gas probes were advanced 4-5 feet below grade. Once inserted into the ground, the above-ground end of the sampling probes were fitted with a steel reducer and a length of polyethylene tubing leading to a vacuum pump. Gas flow is monitored by a vacuum gauge to insure that an adequate flow is obtained.

To adequately purge the volume of air within the probe, 2 to 5 liters of gas is evacuated with a vacuum pump. During the soil gas evacuation, samples are collected in a glass syringe by inserting a syringe needle through a silicone rubber segment in the evacuation line and down into the steel probe. Ten milliliters of gas are collected for immediate analysis in the TRC analytical field van. Soil gas is subsampled (duplicate injections) in volumes ranging from 1 uL to 2 Ml, depending on the VOC concentration any particular location.

Sample probe vacuums ranged from two to eleven inches Hg. The maximum pump vacuum was measured at twenty-three inches Hg.



ANALYTICAL PROCEDURES

A Varian 3300 gas chromatograph, equipped with a flame ionization detector (FID), was used for the soil gas analyses. Compounds were separated on a 6' by 1/8" OD packed column with OV-101 as the stationary phase in a temperature controlled oven at 100°. Nitrogen was used as the carrier gas.

Hydrocarbon compounds detected in soil gas were identified by chromatographic retention time. Quantification of compounds was achieved by comparison of the detector response of the sample with the response measured for calibration standards (external standardization). Instrument calibration checks were run periodically throughout the day and system blanks were run at the beginning of the day to check for contamination in the soil gas sampling equipment. Air samples were also routinely analyzed to check for background levels in the atmosphere.

Detection limits for the compounds of interest are a function of the injection volume as well as the detector sensitivity for individual compounds. Thus, the detection limit varies with the sample size. Generally, the larger the injection size the greater the sensitivity. However, peaks for compounds of interest must be kept within the linear range of the analytical equipment. If any compound has a high concentration, it is necessary to use small injections, and in some cases to dilute the sample to keep it within linear range. This may cause decreased detection limits for other compounds in the analyses.

The detection limits for the selected compounds were approximately 0.07 ug/L depending on the conditions of the measurement, in particular, the sample size. If any component being analyzed is not detected, the detection limit for that compound in that analysis is given as a "less than" value (e.g. <0.1 ug/L). Detection limits obtained from GC analyses are calculated from the current response factor, the sample size, and the estimated minimum peak size (area) that would have been visible under the conditions of the measurement.



QUALITY ASSURANCE/QUALITY CONTROL PROCEDURES

Tracer Research Corporation's normal quality assurance procedures were followed in order to prevent any cross-contamination of soil gas samples.

- . Steel probes are used only once during the day and then washed with high pressure soap and hot water spray or steam-cleaned to eliminate the possibility of cross-contamination. Enough probes are carried on each van to avoid the need to reuse any during the day.
- Probe adaptors (TRC's patented design) are used to connect the sample probe to the vacuum pump. The adaptor is designed to eliminate the possibility of exposing the sample stream to any part of the adaptor. Associated tubing connecting the adaptor to the vacuum pump is replaced periodically as needed during the job to insure cleanliness and good fit. At the end of each day the adaptor is cleaned with soap and water and baked in the GC oven.
- . Silicone tubing (which acts as a septum for the syringe needle) is replaced as needed to insure proper sealing around the syringe needle. This tubing does not directly contact soil gas samples.
- . Glass syringes are usually used for only one sample per day and are washed and baked out at night. If they must be used twice, they are purged with carrier gas (nitrogen) and baked out between probe samplings.
- Injector port septa through which soil gas samples are injected into the chromatograph are replaced on a daily basis to prevent possible gas leaks from the chromatographic column.
- Analytical instruments are calibrated each day by analytical standards from Chem Service, Inc. Calibration checks are also run after approximately every five soil gas sampling locations.
- Subsampling syringes are checked for contamination prior to sampling each day by injecting nitrogen carrier gas into the gas chromatograph.



- Prior to sampling each day, system blanks are run to check the sampling apparatus (probe, adaptor, 10 cc syringe) for contamination by drawing ambient air from above ground through the system and comparing the analysis to a concurrently sampled ambient air analysis.
- All sampling and subsampling syringes are decontaminated each day and no such equipment is reused before being decontaminated. Microliter size subsampling syringes are reused only after a nitrogen carrier gas blank is run to insure it is not contaminated by the previous sample.
- . Soil gas pumping is monitored by a vacuum gauge to insure that an adequate gas flow from the vadose zone is maintained. A reliable gas sample can be obtained if the sample vacuum gauge reading is at least 2 inches Hg less than the maximum pump vacuum.

RESULTS

A total of twenty-one soil gas samples were collected and analyzed in the field. Analytical data is condensed in Appendix A. Isoconcentration contour maps with sampling locations and compound concentrations (Figures 1-4) are in Appendix B. Figures 1 and 3 are maps showing the sampling locations.

Ambient air samples were collected during the course of the investigation to help evaluate the level of significance for the selected VOC's. The level of significance is simply the level above which concentrations are considered to be significant in terms of groundwater or soil contamination. None of the selected compounds were detected in the ambient air samples. The level of significance for each target compound is based on several factors; concentrations in ambient air, background levels, and TRC's past experience. Based on the evaluation of these factors, the level of significance for the selected target compounds was determined to be approximately 1 ug/L. In other words, soil gas concentrations of benzene, toluene, ethylbenzene, xylenes and THC greater than 1 ug/L may indicate possible VOC contamination in the vicinity.



Benzene, toluene, and THC were detected in nine of the ten soil gas samples collected at Building 133. Benzene concentrations ranged from non-detect (<0.08 ug/L) at sampling locations SG-8 and SG-9 to 38,000 ug/L at SG-6. Toluene concentrations ranged from non-detect (<0.07 ug/L) at SG-8 and SG-9 to 18,000 ug/L at SG-6. Only the THC concentrations were contoured because no additional information would have been gained by contouring benzene and toluene concentrations. THC concentrations ranged from non-detect (<0.08 ug/L) at sampling location SG-8 to 750,000 ug/L at SG-6. The hydrocarbon plume extends at least 325 feet to the east and 100 feet to the north of SG-6. The western and southern boundaries can not be defined due to insufficient data.

At Building 710, toluene, xylenes, and THC were detected in the collected soil gas samples. Toluene concentrations ranged from 4 ug/L at sampling location GS-8 to 5,500 ug/L at GS-9. Xylene concentrations ranged from 0.2 ug/L at GW-6 to 4 ug/L at GW-1. Xylenes could not be detected at concentrations lower than 30 ug/L at GW-9, 37 ug/L at GW-11 and 150 ug/L at GW-10 due to elevated concentrations of the other selected compounds which required small injection sizes of the samples. Again, only THC concentrations were contoured for Building 710. The hydrocarbon plume extends at least 100 feet in all directions from the northwest corner of Building 710. Hydrocarbon concentrations were detected above the level of significance (1 ug/L) at all of the sampling locations.

CONCLUSIONS

Significant concentrations of benzene, toluene, xylenes, and THC were detected in the soil gas near Buildings 133 and 710 at Hunter Army Air Field. The isoconcentration contours for total hydrocarbons indicate possible source areas, for subsurface contamination, to the west of Buildings 133 and 710. These areas may coincide with the location of underground storage tanks at these sites. Further investigations are needed to better define the source and extent of subsurface contamination.

Tracer Research Corporation

APPENDIX A: ANALYTICAL DATA

) Tracer Research Corporation

ARMY CORPS OF ENGINEERS/HUNTER AAF/SAVANNAH, GEORGIA JOB#1-90-384-T 07/11/90 CONDENSED DATA

Ç.	ug/l	<0.2	40	32	1600	36	4	750000	120000	<0.08	0.8	14
SWE CVY		<0.1	<0.07	<0.07	<0.7	<0.1	<0.1	<35	<35	<0.07	<0.07	<0.07
ETHYL	ug/l	<0.2	<0.08	< 0.08	× 0.8	<0.2	< 0.2	<42	<42	< 0.08	< 0.08	< 0.08
TOTHENE	ng/l	<0.1	4	4	14	4	8.0	18000	14000	< 0.07	< 0.07	2
HFNZENE	l/gu	<0.2	*7	44	27	. 9		38000	26000	<0.08	< 0.08	2
	SAMPLE	AIR	SG-1-4'	SG-2-4'	SG-3-4'	SG-4-4°	SG-5-4*	SG-6-4'	SG-7-4"	SG-8-4.	SG-9-5'	SG-10-5'

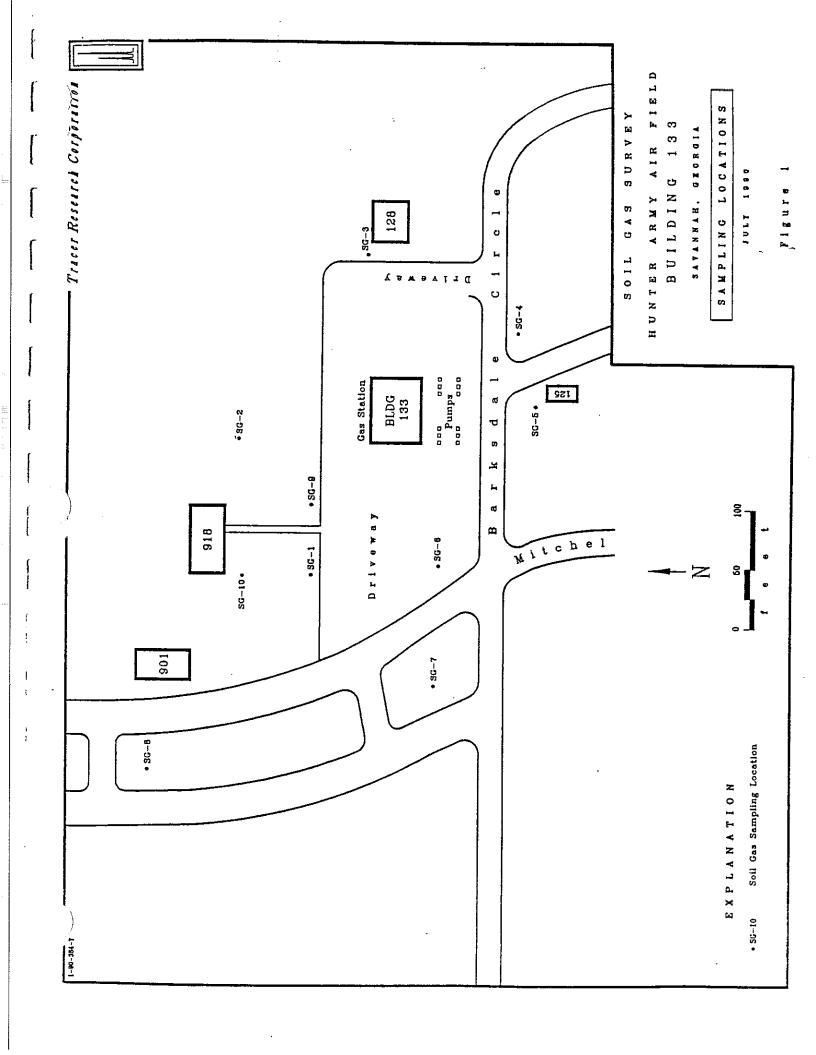
Analyzed by: K. Ptak Checked by: M. Flack Proxifed by: M. On planel ARMY CORPS OF ENGINEERS/HUNTER AAF/SAVANNAH, GEORGIA JOB#1-90-384-T 07/12/90 CONDENSED DATA

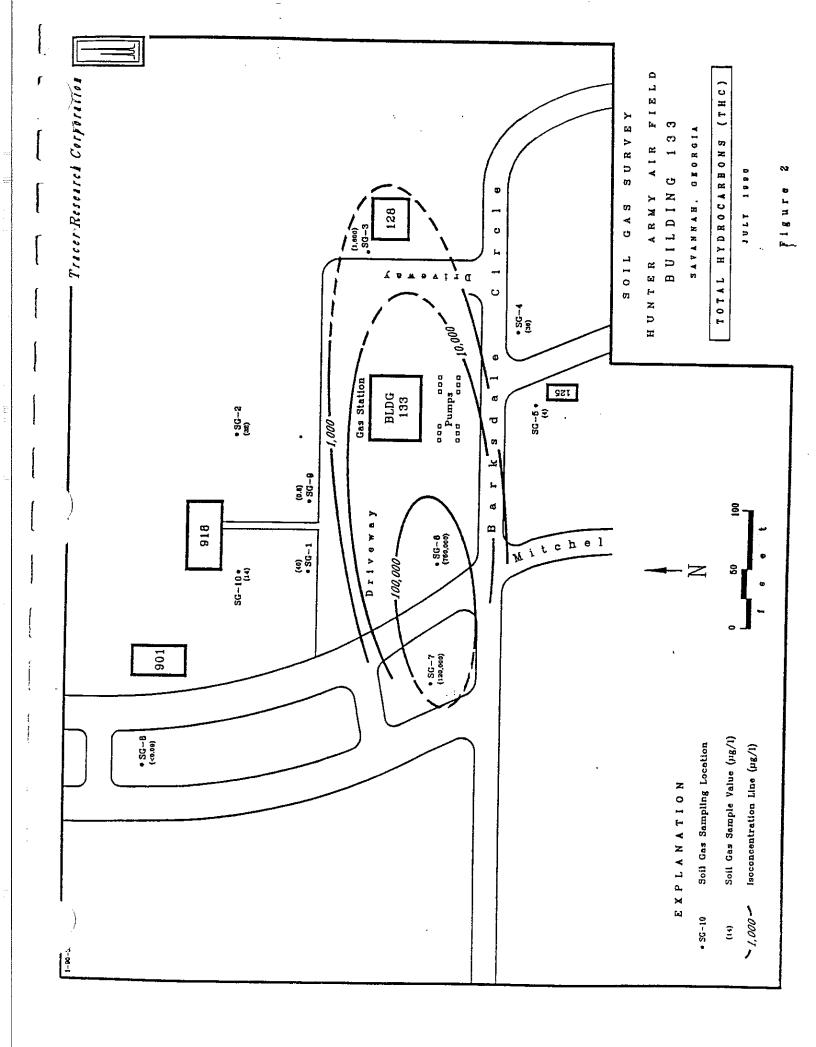
TIIC	<0.3	29	12	œ	, 5	41	14	27	٥	180000	160000	3800
XYLENE ug/l	< 0.07	4	9.0	03	9.0	0.3	0.2	0.3	0.5	× 30	×150	<37
ETHYL BENZENE ug/l	< 0.08	<0.4	< 0.1	< 0.2	<0.08	<0.2	<0.08	<0.08	<0.08	<31	<150	<39
TOLUENE ug/l	< 0.07	70	9	'n	9	10	4	80	4	5500	1800	<37
BENZENE ug/l	< 0.08	4	<0.1	<0.3	<0.2	<0.3	<0.2	<0.2	<0.2		-	<78
SAMPLE	AIR	GS-1-4'	GS-2-4'	GS-3-4'	GS-1-4,	GS-5-4'	GS-6-4'	GS-7-4"	GS-8-4'	68-9-5	GS-10-5	GS-11-4'

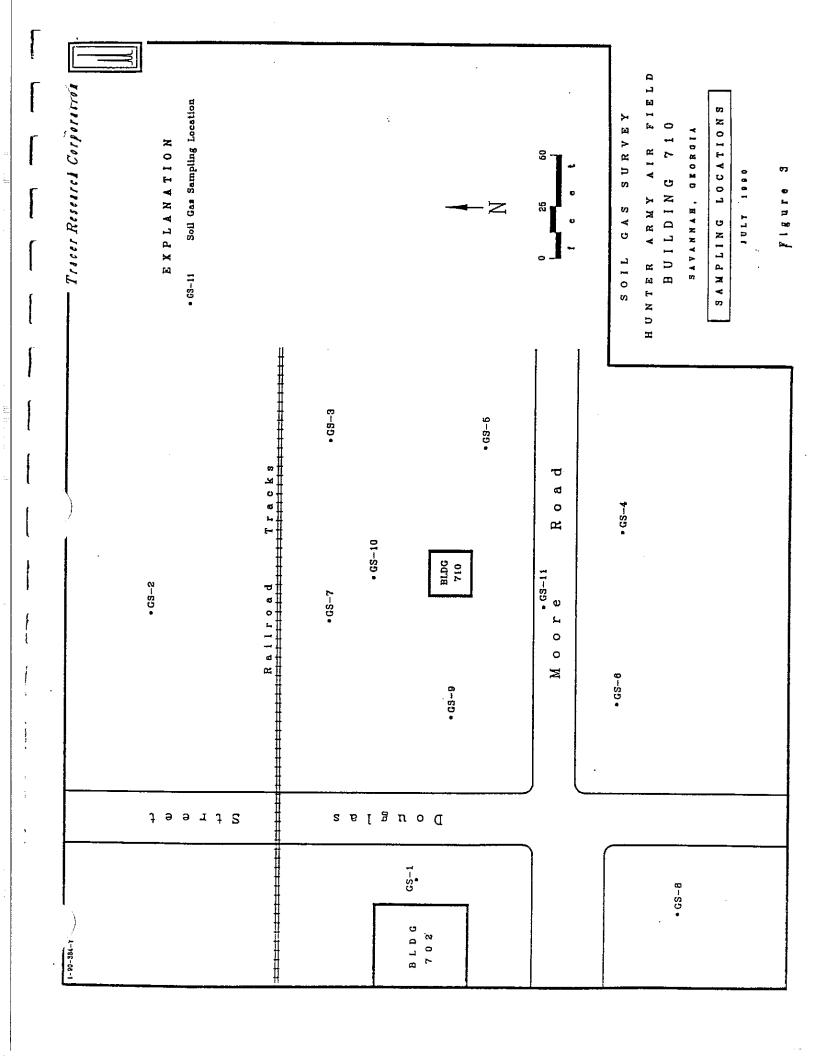
interference with adjacent peaks

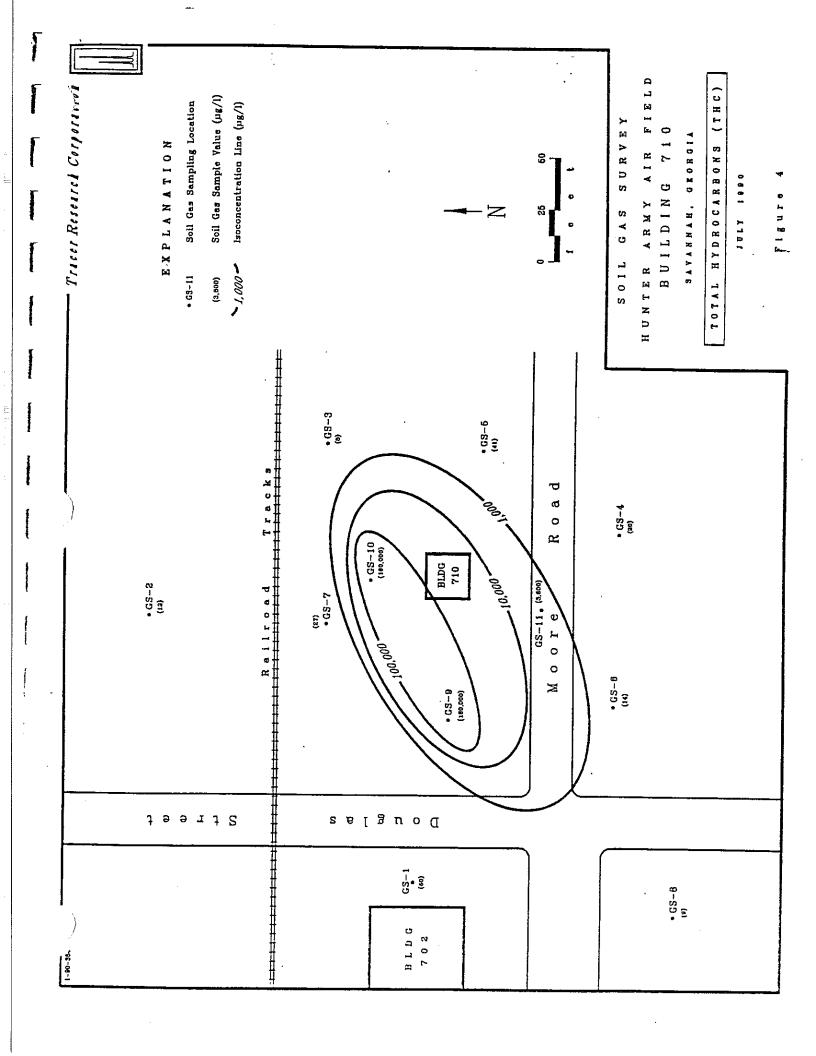
Analyzed by: K. Ptak Checked by: M. Flack Proofed by: A. Agolandes

APPENDIX B: FIGURES









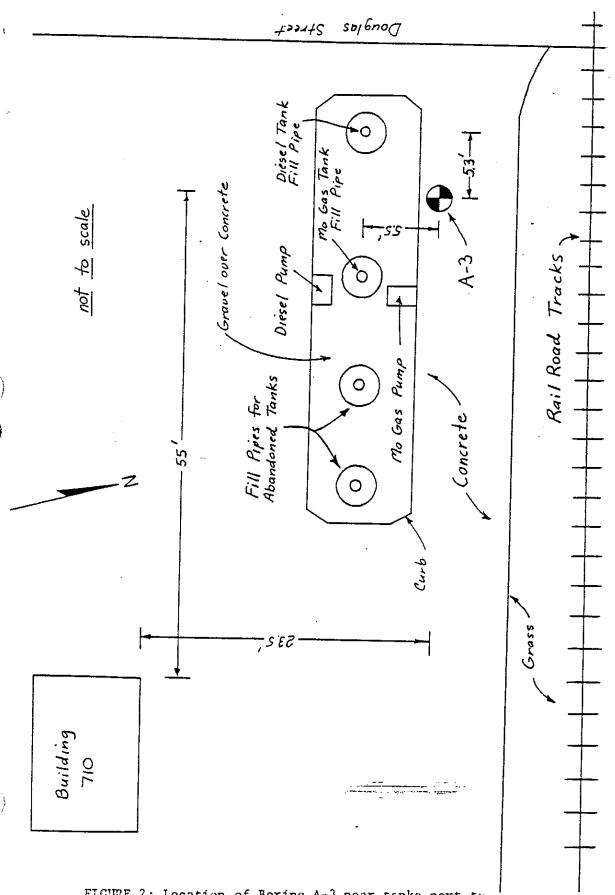


FIGURE 2: Location of Boring A-3 near tanks next to Building 710, Hunter AAF, Ga.

C-3 - DRILLING LOGS AND HTW LOG FOR BORING T-1 (A-3)

				·			Hole No.		<u>-3)</u>
DRILL	ING LO	XG D	IVISION		LATION ter AAI			SHEET 1	
. PROJECT			South Atlantic				Hand Auger	ofl s	HEET
Underg	round (Coordin	Stora	ge Tank Testing	11. DAT	UM FOR E	LEVATION MSL	n shown (TBM or MSL)	
	as pur	mp at	Building 710	12. MAN			IGNATION OF DRILL		
. HOLE NO.	(As show	n on draw	ina titla	13. TOT	AL NO. OF DEN SAMP		DISTURBED	UNDISTU	RBED
and tile num	10 BC		T-1 (A-3)		AL NUMBE		<u>. i </u>	0	
James			:		VATION G			 	
DIRECTION	OF HOL	E		16. DAT	E HOLE			MPLETED	
			DEG. FROM VERT.	17. ELE	VATION TO		LE 20'± (from		7
THICKNESS			7.1				Y FOR BORING		
TOTAL DE			9.7	19. SIGN	ATURE OF	INSPECT	TOR		
I TOTAL DE	FIN OF I	HOLE	· · · · · · · · · · · · · · · · · · ·				son, Geologist		
20 g0 t	DEPTH	LEGEND c	CLASSIFICATION OF MATERIA (Description) d	LS	% CORE RECOV- ERY	BOX OR SAMPLE NO.	REMAR (Drilling time, water, weathering, etc.,	w Inne, dent	h of
					1			 .	·
	=	,	Concrete				Water level of drilling: 4.		
19.0'		111	(SM)SILTY SAND, light	grey,	1	1	ATTACTING: 4.3	,	
	╡	†I†I	fine to med., silty. O				24 hour water		
	2 -∃	$\dagger I \dagger I I$	see note l.				reading: Not		
	日	†I†I	Brownish-tan.				hole backfill drilled.	led afte	≘r
ľ	_=	I	DIOWHISH-LAH.				arilled.		
1	\exists	† [† [Note 1: See H	ITW log	for
1	\exists	 					further infor		
].	4 🚽	+I+I		_					
	\exists	 	Dark grey,wet.						
	=	†]†][
	\exists	†I †I[Saturated.			2	LOCATIO	N MAP	
Ī	\exists	†I†II			ĺ	·			
	6 🚽	† [†]					- 	 	₩.
	∃'	∮ ┇∮┇┆			Ì		T-1	rail	, J
		† ↓†↓					(À-3)		ο •
	∃'	ţ↓ţ∐						Fill I	ripe
	= 1	♦↓♦ [ˈÌ				ļ	(00)
1	8 ㅡ '	↑ ↓↑↓├						\ /	•
		<u></u>	Dark brown-grey.			ļ	Gas Pum	P	
		 			Į		L	not to sc	ما ۾.
	= 1	[[]		3		אל פר זפוי	415
0.3'	10	- 	Bottom of Boring = 9.	7,			<u> </u>		
ł	\exists		_	ļ	-				
		İ	NOTE:Soils visually f:						
	\exists		in accordance with the Classification System		ied Sd:	11			
	\exists	ĺ	orassiticación system	.	1				٠
	\exists								
	\exists				-				• •
	_=	Ì				-			
	\exists				-	l			
		ļ		1					
l			• <u> </u>			- 1			

)

HTW BORING LOG

			· <u></u>	111	44	2011	40						. <u></u>	
PROJE	CT:		NG 710 GROUND	STORA	GE TA	NK LE	AK TE	STING			BORING	NO.	T-	1 (A-3)
LOCAT	ION:	HUN	ITER ARM	IY AIRF	iELD,	GEORGI	A				ELEVAT		' <u>+</u> (FR	OM TOPO)
WATER	LEV	/EL DUR	RING DR	ILLING	4.	5'	2.	4-HOU	IR WATER LE	EVEL	READING	<u> </u>		TAKEN BACKFILLED
WEATH		45 DE	GREES, C	OLD, S	UNNY,	WINDY			DRILLER:	JA	MES E. BO	DLEN		
REMAR		HERE WA	S 1.0' OF	CONC	RETE	AT SU	RFACE		GEOLOGIST	,	TONI F. NIC	CHOLS	ON	
					0.	ENT			SAM OVA	PLES	HNU	AT	TOP	OF HOLE
Š.		ſ	PTH T.)		7 F00T	CONTENT	TION		(ppm)	1	opm)		:GI	<u> </u>
SAMPLE	ODOR	V.	1.7	E (1991)	WS PER	MOISTURE	CLASSIFICATION	OR	FIELD HEADSPACE	1	ELD DSPACE	LEL	02	OVA / HNU
U)		FROM	то	DATE	BLOWS	MOIS	CLA	COLOR	ANALYSIS	ANA	LYSIS	%	%	(ppm)
1	ST	1.0	1.5	12/15	•	DAMP	SM	LIGHT TAN	410	,				
•	ST	2.0	2.5	12 / 15	_	DAMP	SM	BRN/ IAN BRN/	1000+					
	ST	3.0	3.5	12/15	-	DAMP	SM	TAN	1000+		_			
	ST	4.0	4.5	12/15		WET	SM	DK. GRA	1000+					
2	ST	5.0	5.5	12/15	-	SAT.	SM	DK. GRA	1000+					
	ST	6.0	6.5	12 / 15	-	SAT.	SM	DK. GRA	1000+		-			
	ST	7.0	7.5	12/15	-	SAT.	SM	DK. GRA DK.BR	1000+					
	М	8.0	8.5	12/15	-	SAT.	SM	I GRA I	1000+					
3	М	9.0	9.5	12 /15	-	SAT.	SM	DK. BRN	1000+					
	М	9.4	9.7	12/15	-	SAT.	SM	DK. BRN	1000+	!				
	Ш	_												
			<u> </u>				·							
														· <u>.</u>
														<u> </u>
:														
			_											
											<u>_</u>			
											-			

BORING LOGS AND WELL CONSTRUCTION DETAILS

D-1 - DRILLING LOGS

D - 2 - HTW BORING LOGS

D-1 - DRILLING LOGS

		1.	DIVISION	T			Hole No	. MW-710-1
	LING L	oc ˈ	South Atlantic	Hun	LATION ter AA]	F. Geor	gia	SHEET I
I. PROJECT				1				
2. LOCATIO	N (Coordin	- 51t	e Investigation	11. DAT	UM FOR E	CEVATIO	4"ID Hollow N SHOWN (TEM a M	1/2"Hand_
See	Plan			12. MAN	MSI	ER'S DESI	GNATION OF DRILL	Auger
3. DRILLING Savai	nnah D		:t		CME	45		
4. HOLE NO. and file mu	(As show ember)	m on draw	ring title MW-710-1	13. TOT BUR	AL NO. OI DEN SAMF	LES TAK	EH 1	UNDISTURBED
5. NAME OF Dougla	DRILLER AS LaR	•			AL NUMBI			ow
6. DIRECTIO			DEG. FROM VERT.	16. DAT	E HOLE		ARTED	COMPLETED 1 May 91
7. THICKNES				17. ELE	VATION T	OP OF HO	LE 18.76'(TO	<u>-</u>
B. DEPTH DE				18. TOT	AL CORE	RECOVER	Y FOR BORING	
. TOTAL DE			8.0'		ATURE OF		or , Geologist	
ELEVATION	DEPTU	LEGENS	CLASSIFICATION OF MATERIA		Well	BOX OR	DEM	ARKS
g g	b	c	(Description)		Const- ruction	SAMPLE NO.	(Drilling time, we	iter loss, depth of, if significant)
ĺ		1	Manhole Cov		ļ			
18.76'	0 —		Mannote Cov	ver			Depth to w during dri	
18.36'		1010	Concrete & gravel.		7 0	}	i i i i i i i i i i i i i i i i i i i	1
		╏┿╁┿╁	(SM) SILTY SAND, brow		P P		Water leve 24 hours a	_
			tan,loose,fine to ver grained SAND. 10% sil]	completion	
	\exists		Moist. Strong fuel od		 [] [] [-	<u> </u>	-	
16.76'	2 —	* 1						g for more
16.26'	\exists	9 9	(MH) INORGANIC SILT, bl soft, fat, organic rich				informatio	
	ᆿ	111	some roots.	`,"'	.: 目 :::		l.O'	onite Seal:
ł	_	†	(SM) SILTY SAND, brow	m 254	· 目···		·	. 1 5 7
·	, =	† †	tan, loose, fine to ver		<u>.</u> [=] ``	MW-710	Top of Sand	1: 1.5
Ì	4 —		grained w/10% silt.	-	·:\[=]::\	-1-1		
}	7	 	7/	•	.: E].::	ļ f	Screened in	iterval:
	\dashv	 	Very moist.	.			2.5'-6.5'	
	\dashv]	Brown, saturated.	ĺ	:' <u>⊟</u> ;.	ļ	Screen Size	
	_ = =	I	30% silt.	-	· [] ·	ľ	Well Point	Set at
	٥٦	[<u> </u>				7.5	
İ	\exists	IfI	Some clay.		· [-]			
ł	\exists	ItItl						
1	\exists	[Grey	- ·	$\cdot \cdot \cdot V_{\cdot} \cdot $	1		
10.76	8 = =	<u> </u>		:				
20.70	Ĭ		Bottom of Hole = 8.0'	1				<u> </u>
	_	İ			ļ	}		•
	=	,						
.	Ⅎ			-	Ì	l		
		ļ		}		ļ		
	\exists	.	NOTE CALL	,	ĺ			
	\exists		NOTE:Soils visually fie classified in accordance	eld	İ			
ĺ	\dashv		with the Unified Soil.	:e				
	\exists		Classification System.		İ			
	=		J = 2 3 m t		[
	\exists	1			1			•
]				1	1	1		
1		1						

	 						Hole No.	11W-710-4
DRIL	LING LO	oc P	South Atlantic	Hun	LATION ter AAF	. Geor	reia	SHEET!
1. PROJECT		_ 0:+:	2 Investigation	 			/ 11 7 7 7 7 7	
2. LOCATION	N (Coorder	- SILE	e investigation	11. DAY	UN FOR E	LEVATIO:	4"ID HOLLOW St N SHOWN (TBM or MSL 3 1/2" Har	nd Auger
See I							GNATION OF DRILL	
Savar	nnah D	istric		13. TOT	AL NO. OF	OVER-	DISTURBED	UNDISTURBED
4. HOLE NO. and file nu	(As show mbec)	m on draw	MW-710-4	BUR	DEN SAMP	LES TAK	EN]	0
NAME OF	DRILLER Las La				AL NUMBE			
. DIRECTIO	N OF HO	LE		 				MPLETED
VERTI	CAL _	INCLINED	DEG. FROM VERT.	16. DAT			May 91 2	May 91
7. THICKNES	S OF OVE	ERBURDE	14.2	ł			LE19.15!(TOH)	19.00'(TOR)
A. DEPTH DR			•	19. SIGN	ATURE OF	INSPECT	Y FOR BORING	1
. TOTAL DE	PTH OF	HOLE	12.5'				, Geologist	<u> </u>
ELEVATION	DEPTH b	LEGEND c	CLASSIFICATION OF MATERIA (Description)	LS	Well Const- ruction	BOX OR SAMPLE NO.	REMAR (Drilling time, wate weathering, etc.,	r loss, death at
			V1- (1					
19.15'	0 —		Manhole Cove	· ——	7		Depth to war	
İ			Concrete and gravel.	······································	7 1 A	•		1
18.55			(SP)POORLY GRADED SA	,	0 0		Water level 24 hours af	
18.15'] •] •	tan,loose,fine to ver fine grained. Moist	ry [7/3/7/		completion:	
-	_ =] •] •	(SM)SILTY SAND, brown			:	-	
j	2		tan,loose,fine to ve	ry fin	e (7)		See HTW log	
	\equiv	+ [+ [grained, w/10% silt.	Strong		MW-710		
		+I+I	fuel odor.		∷	-4-1	1.0'	Juice Beat:
	7	† † 	Saturated				Top of Sand:	: 1.5'
	4	1+1++	Wood				Screened Int	erval:
	ᆿ	$I \bullet I \bullet I$					2.5'-11.5'	
ļ	ᆿ	 	Brown	İ			Screen Size:	
ĺ	\exists	†I†I					Well Point S	Set at
	6	†] †]]]			12.5	
	\exists	†						
	\exists	1		İ	: = : :			
	크] † [†		ľ	`.∃.:I			·
	\Box	 			: El l		Interval fro	- 201
. [° ±	• [• []	•	ľ			12.5' was n	
l	╡	ţŢţŢŢ	·					00
	\exists	1 1 1						
•	⇉	Ĭ ∳Ĭ∳∜		ŀ		Ì		
	10			[.		ļ		ļ
	\exists	 []	NOTE: Soils visually fide classified in accordance	eld				
		<u> </u>	with the Unified Soil	-e				
	======================================	† ↓ † ↓ │	Classification System.	ļ,	.目.1	İ		
	12	1 1 1		:				Ė
6.65'	3		Bottom of Hole = 12.5	7	:.V:			-
1	4	1		Į.	1	1		. [

DRILL	INC LO	<u></u>	VISION	INSTAL			Hole No.	SHEET
1. PROJECT	ING EC	<u> </u>	South Atlantic	. !		AF, Geor		of 1 she
	710	- Site	Investigation	10. SIZE	UN FO	ELEVATION	4"ID Hollow S shown (TBN & ASI 3 1/2" Hand	tem Auger
See P.	lan		mioru .	L			GNATION OF DRILL	
3. DRILLING A		lstric		1		E 45		
4. HOLE NO. (As show			13. TOT	AL NO.	OF OVER-	DISTURBED	UNDISTURB
and file mum	bed .		MW-710-5	}		ABER CORE		0
–		Roche		1			TER See Belo	w
6. DIRECTION				1		STA	RTED C	OMPLETED
VERTIC.	AL 🗀	NCLINED	DEG. FROM VERT.			3 I		6 May 91
7. THICKNESS	OF OVE	RBURDE	11.0				LE 17.85'(TOH)	17.65'(1
8. DEPTH DRI	LLED IN	TO ROCK		19. SIGN	ATURE	OF INSPECT	Y FOR BORING	
9. TOTAL DEP	THOF	IOLE	11.0	Da	vid	C. Leeth	, Geologist	
ELEVATION d	DEPTH Ь	LEGEND ¢	CLASSIFICATION OF MATERI (Description)	ALS	Well Cons ruet	- SAMPLE	REMA (Drilling time, we weathering, etc.	er ices, deuth
					 		- 9	
	\exists		Manhole Cover —		<u> </u>		Depth to wa	
17.85'	0 -	1411	(0) (0)				during dril	lling:3.10
	⇉	† [†]	(SM)SILTY SAND, brown fine to very fine gr	,loose	7	7	Water level	readino
		† † 	w/10% silt.		1	<i>b</i>	24 hours af	ter hole
	ゴ	*	Dark brown w/30% sil	t.	13		completion	3.87
,, ,,	\downarrow	1+1+1	Black.		. ' !	<u>. </u>	See HTW log	for more
15.85'	2	7,7	(SC)CLAYEY SAND, blac	k,soft	., 0		information	
	\exists	757	very fine grained, w/		∷⊨	MW-71)	
	<u> </u>	اوووو	clay.	-		:\ 	Top of Bent	onite Sea
	∃,		Very moist.	- i	: =		Top of Sand	: 1.5'
	4	999	Saturated.		· [<u>=</u>]	$ \vec{A} = 1$	Screened In	
13.35'	7	222			: =	•	2.5'-9.25	
		IţĬţĬ	(SM)SILTY SAND, black	,loose	, [=]			
	\exists	Ĭ∳Ĭ∳ſ	very fine grained,w/	30%	: =	:.		
	⇉.	ĮţĬţ	Tan and black.		11111111			
	6 -	╻ ┍╻	ran and DIACK.	_		.]		
	\exists	∳ ∳∳∳	Tan.		[비]	•		
		 				'i		
	\exists	∳Ĭ∳Ĭŀ			; [=]			
	s →	<u> </u>			: 🗐			
'	=	<u> </u>	•		· [=]			
	_ ≓'							
	7				. [=]			
	7			İ				
10	o —]'		Bottom of Hole = 11.0	,	; V.			•
			NOTE: Soils visually fi	eld	1			
C 051]		classified in accordar	ice		.		
6.85'	\exists		with the Unified Soil.	*		-		
	\exists		Classification System.	ļ				
	=							
				. }				

Hole No. MW-6 DIVISION INSTALLATION SHEETI DRILLING LOG South Atlantic Hunter AAF, Georgia OF I SHEETS 10. SIZE AN' TYPE OF BIT 4"ID Hollow Stem Auger, Building 710 - Site Investigation 11. DATUM FOR ELEVATION SHOWN (TBM or MSL)
MCT 3 1/2" Hand Auger 2. LOCATION (Coordinates or Station) See Plan 12. MANUFACTURER'S DESIGNATION OF DRILL 3. DRILLING AGENCY CME 45 Savannah District 13, TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN DISTURBED UNDISTURBED 4. HOLE NO. (As shown on prawing title) 0 and file number) MW-6S. NAME OF DRILLER 14. TOTAL NUMBER CORE BOXES 15. ELEVATION GROUND WATER See Below Douglas LaRoche 6. DIRECTION OF HOLE STARTED COMPLETED 16. DATE HOLE TYERTICAL | INCLINED. DEG. FROM VERT. 14 May 91 14 May 91 17. ELEVATION TOP OF HOLE 21.05 (TOH) 20.79 (TOR) 7. THICKNESS OF OVERBURDEN 11.0' 18. TOTAL CORE RECOVERY FOR BORING 8. DEPTH DRILLED INTO ROCK 0.0' 19. SIGNATURE OF INSPECTOR
David C. Leeth, Geologist 9. TOTAL DEPTH OF HOLE 11.0' well BOX OR Const-ruction HO. CLASSIFICATION OF MATERIALS (Description) ELEVATION DEPTH LEGEND REMARKS (Driffing time, water loss, depth of weathering, etc., if significant) Manhole Cover -Depth to water 21.05' during drilling: 5.61' (SM) SILTY SAND, Black, loose, very fine grained, w/10% Water level reading 24 hours after hole silt. Moist. completion: 4.29' Brown. Black. 19.05' See HTW log for more information. (MH) INORGANIC SILT, black, loose, fat silt, w/20% sand. Top of Bentonite Seal: 18.05' 1.0' Roots. Top of Sand: 1.5' (SM) SILTY SAND, brown, loose, MW-6very fine grained,w/25% Screened Interval from silt. 2.5'-9.25'. Very moist. Well Point Set at 10.0' Roots, saturated. Some clay. Approximately 25%! Bottom of Hole = 11.0' 10 NOTE:Soils visually field classified in accordance 10.05 with the Unified Soil. Classification System.

j

		Trus	VISION	INSTALL	ATION		LIDIA LO	MW-710-7
DRILL	ING LO	3_	South Atlantic	Hunt	er AAl	Georg		OF 1 SHEETS
1. PROJECT	710	C d b a	T	10. SIZE	AND TYP	E OF 8174	"ID Hollow St	tem Auger,
Building 2. LOCATION	-		Investigation	III. DATU	im for E MSI	FEAVION	3 1/2 Hand	Auger
See P	lan			12. MAN	JF ACTUR	ER'S DESIG	GNATION OF DRILL	
3. DRILLING	AGENCY nah Di	c++4.*		<u> </u>	CME	45	-	
Savan 4. HOLE NO. and Me mus				13. TOTA	AL NO. O	F GVER-	DISTURBED	O
		F	MW-710-7			ER CORE B		<u> </u>
L NAME OF		. 1					TER See Belo	
Dougla	S LAKO	cne E				107.4	eren la	OMPLETED 13 May 91
••			DEG. FROM VERT	16. DATI		,		
7. THICKNES	E OF OVE	9911005	n 11.0'	17. ELE	VATION T	OP OF HO	LE 18.88' (TOH))18.68'(TOR)
8. DEPTH DR							Y FOR BORING	
9. TOTAL DE			11.0'	19. SIGN Da	ATURE O	FINSPECT Leeth	or , Geologist	
9. TOTAL DE	PINOFA	OCE	· · · · · · · · · · · · · · · · · · ·		Well	BOX OR		ARKS
ELEVATION	DEPTH 1	LEGEND c	CLASSIFICATION OF MATERI (Description) d	ALS	Const-	SAMPLE	(Drilling time, we	iter loss, depth of ., if eignificens) 9
	\exists		16-1-10 Com	ar	_		Depth to w	ater
	╛		Manhole Cov	CT	—	1	during dri	ater 11ing: 4.54'
18.88'			Asphalt and gravel.			1		a·
	井	111	(SM)SILTY SAND, black	£ +c=		7	Water leve	
		† [†]	loose, very fine grain	-		믹	24 hours a	
	⇉	∳ Ĭ ∳ Ĭ	w/10% silt.	,	$\mathbb{Z}_{\mathbb{Z}}$	1	completion	:5./5
	Ⅎ	†I†I	25% silt. Moist.		: = :		See HTW 10	g for more
	2 —	$\phi I \phi I$	ZJ/o SIIC. HUISC.				informatio	•
	Ⅎ	†I†I	Dark brown,organic r	ich.	: E	1	i	tonite Seal:
		†I†I			[: l타·	<u> </u>	1.0'	
	\exists	 	Very moist.		=		MW-7-1	•
	\exists	1111	· ·		:: <u>=</u> .	MWīć-	<u>MW-7</u> -1A	
	4 —		D (50 - • • •		: 三 .		†	•
	\exists	 	Brown & tan,45% silt Saturated.	•	,	;[Top of San	
12 221	-	4141	Daturateu.]: []:	.	2.5'-9.25'	nterval from
13.88'	\dashv	: :	(SP)POORLY GRADED SA	ND, tan,]::[=]:	1	Well Point	Set at
	7		loose, very fine grai		[:]=		10.0'.	→ <u></u>
	6 —				=	.]	ŀ	
	⇉				I∴∏.			
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		', .(·			; <u> </u>	:		
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	8 —	, ,			: =	<u>:</u> }	1	
							1	
					· <u>-</u>	1	1	
	\exists							
	<u>, </u>		Bottom of Hole = 11	Ut 1	[· V			·
	10				,,,,,,,	.		
	二		NOTE:Soils visually to classified in accordance.			.		
7.88'		` · · .	with the Unified Soi		1	:		
'			Classification System					
			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	-				
1					1	1		
					1		i	

							Hole No. MW-8	
DRILL	ING LO	G DI	South Atlantic	1	ter AAF	, Geor		TS
Buildin	g 710 -	- Site	Investigation	10. SIZE	UM FOR E	E OF BIT	4'ID Hollow Stem Auger, SHOWN / 2"Hand Auger	
2. LOCATION See I		tes or St	Mion)	1	1,10 F	,	GNATION OF DRILL	
3. DRILLING Savar	AGENCY mah Di	strict		12. 700	CME		GRATION OF DRILL	
4. HOLE NO.	(As shown			13. TOT BUA	AL NO. OF DEN SAMP	OVER- LES TAKE	N 1 0	D
5 NAME OF Douglas		he				R CORE E		
6. DIRECTION			DEG. FROM VERT.	16. DAT	E HOLE	i	RTED COMPLETED 4 May 91 14 May 91	\dashv
7. THICKNES				17. ELE	VATION TO		료9.35'(TOH)19.11(TOR)	コ
8. DEPTH OR	ILLED IN	TO ROCK				RECOVER	Y FOR BORING	z
, TOTAL DE	PTH OF H	OLE	11.0'	Da	avid C.	Leeth	Geologist	
ELEVATION 4	DEPTH I	LEGEND	CLASSIFICATION OF MATERIA (Description)	LS	Well Const- rustion	BOX OR SAMPLE NO.	REMARKS (Drilling time, water loss, depth of weathering, etc., if significant)	
			Manhole Cov	er				-
19.35'	0 =				1		Depth to water during drilling: 3.6	ı!t
	<u></u>	<u> </u>	Asphalt & gravel. (SM)SILTY SAND,black,1	0050	D A		Water level reading	Ė
	=======================================	! !	T'ery fine grained, w/l		0 0		24 hours after hole completion: 3.47'	Ė
		1	silt. Moist. Tan & brown.	— Г			•	E
17.35'	2	771	(SC)CLAYEY SAND, grey, m	ed - tra	્ય		See HTW log for more information.	E
1	3		fine grained ,w/40%cla		, <u> </u>		Intoimation.	E
	<u> </u>	111+	(MH)INORGANIC SILT,bla			MW-8-1		-
	Ξ,		organic rich,soft,fat w/10% sand.	silt,			Top of Bentonite Seal	. E
	4 —		Very moist.	-		,	1.0'	Ė
	3		Roots.	_			Top of Sand: 1.5' Screened Interval fro	<u>.</u> E
14.35	-7	9 9 1	Saturated.				2.5'-9.25'.	F
}	<u> </u>		(SM) SILTY SAND, black, lo				Well Point Set at 10.0'.	E
	6 - 1		very fine grained, w/403 silt.	8				F
	$\exists j$				$ \cdot $			E
		199	(SC)CLAYEY SAND, tan, med very fine grained, w/40%		·			E
	_ ∃⁄2		clay.	-	· [] : []			E
	8 -				<u>: [] </u>			F
	∄;		·		-[티]			E
İ	<u> </u>				:[]:1	1.		F
.	\exists']	$[\cdot]$			E
ļ .			Bottom of Hole = 11.0']	: V:	•		F
, in the second	= 1/2	799	NOTE: Soils visually fide classified in accordance	eld				E
8.35'		9.7	with the Unified Soil.	e	15 - 5-6-			上
	\rightrightarrows		Classification System.	ĺ		-		
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								E
1		1		ı	· H	₹		—

	1 1 1 2 2	IVISION	INSTALL		·	Hole No. MW-10				
DRIL	LING LOG	South Atlantic	<u> </u>	er AAF						
Buildin	ng 710 - Sit	e Investigation	10. SIZE	AND TYPE UN FOR EI MSL	EVATION	"ID Hollow Stem Auger, SHOWN (TOW & MSL) 3 1/2"Hand Auger				
See 3. DRILLING		·	12. MAH	UFACTURI	ER'S DESI	GNATION OF DRILL				
Sava	nnah Distric		13 707		luger/C					
	. (As shown on grass anbes)	ring stile MW-10	13. TOTAL NO. OF OVER-BURDEN SAMPLES TAKEN I UNDISTURBE							
S. NAME OF Dougla	oriller as LaRoche	- 	L L			TER See Below				
6. DIRECTIO	N OF HOLE	D DEG. FROM VER	T. 15. DATE HOLE STARYED COMPLETED 7 May 91 13 May 91							
7. THICKNE	SS OF OVERBURDE	EN 11.0'	17. ELE	VATION TO	P OF HO	LE 19.0'(TOH)18.8'(TOR)				
	RILLED INTO ROC	····				Y FOR BORING				
9. TOTAL D	EPTH OF HOLE	11.0'	19. SIGN	ATURE OF	Leeth	, Geologist				
ELEVATION a	DEPTH LEGENS	CLASSIFICATION OF MATER	IIALS	Well Const- ruction	BOX OR SAMPLE NO.	REMARKS (Drilling time, weier loss, depth of weathering, etc., it significant)				
19.0'	0	Manhole Cov		1		Depth to water during drilling: 4.34'				
·	= 1111	(SP)POORLY GRADED SA loose, very fine grai	ned.	4 4		Water level reading 24 hours after hole completion: 4.88'				
16.00'	2	(SM) SILTY SAND, broen of orange, loose, very grained, w/10% silt. Black & brown. Black, 30% silt w/traclay. (MH) INORGANIC SILT, bfat silt, w/trace of (5%).	fine ce of	od 3		See HTW log for more information. Top of Bentonite Seal: 1.0' Top of Sand: 1.5' Screened Interval from 2.5'-9.25'. Well Point Set at				
15.00'	= 111	Saturated.			-1					
8.00'	8	Bottom of Hole = 11. NOTE:Soils visually classified in accord with the Unified Soi Classification Syste	0' field ance	/y:						

i								Hole No.	MW-11				
		LING LO	NG DI	vision South Atlantic		LATION ter.AAI	, Geor		SHEET I				
)	1. PROJECT		C	T	10. SIZE	AND TYP	E OF BIT	4"ID HOllow S	tem Auger.				
,	2. LOCATION	N (Coorden	- 5116	Investigation	11, DAY	UM FOR E	LEVATION	3 1/2" Hand	.) Auger				
	See 3. DRILLING	Plan			1			GNATION OF DRILL					
	Savar	nnah D:	istrict		<u> </u>	AL NO. 01		DISTURBED	UNDISTURBED				
	4. HOLE NO.	(As show enbed)	n on ptrawi	ng title MW-11	BUR	0							
	5. NAME OF						R CORE B						
=	Dougla	N OF HOL	.E		15. ELEVATION GROUND WATER See Below								
	VERT	CAL []	NCLINED	DEG. FROM VERT.									
	7. THICKNES	S OF OVE	RBURDE) 18.55 (TOR)				
	8. DEPTH DE	RILLED IN	TO ROCK	0.0'	18. TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSPECTOR								
	9. TOTAL DE	EPTH OF	HOLE	11.0				, Geologist					
	ELEVATION	DEPTH 6	LEGEND c	CLASSIFICATION OF MATERIA (Description)	LS	Well Const- rustion	BOX OR SAMPLE NO.	REMA (Drilling time, wer weathering, etc.,	er loss, depth of				
				•		 •	 ' ' 	9					
	18.95'			Manhole Cove	r —	<u> </u>		Depth to wa					
	1	~ -		Gravel (Parking Lot)									
	18.50'		4141	(SM)SILTY SAND, light h	rown,	V D	,	Water level					
			1111	loose, very fine grains			, 1	24 hours af	E E				
			 	w/10% silt. Moist.			1	completion:	3.40				
) .		2 -	† ‡†‡}	Tan.	_	2",		See HTW log					
			Įţţţ	Very moist.				information Top of Bento	į.				
			+ 🕽 + 🕽	·				1.01	. [
	,,	, \exists	1+1+1				MW-11.	Top of Sand	ţ				
	14.95'	*=		(MH) INORGANIC SILT, bla	ick,soi			Screened Int 2.5'-9.25'.	erval from				
		=======================================	.	fat silt, w/trace of sa saturated.	ınd,								
		\exists					MW=1 I -2	Well Point S	Set at				
•		6 —		,				10.0'.					
		=		Some 2-3 CM silty sand	lense	8			}				
			: 			[·:							
]	\exists					,						
		8			,	·" - -;*,			. ‡				
		=				- : 			ļ				
						()			ļ.				
	.]	\exists	·										
		10		Bottom of Hole =11.0	 	À : :			·				
		=		NOTE:Soils visually fi	eld				<u> </u>				
)	7.95'			classified in accordan	ce								
	,,,,,	\exists		with the Unified Soil. Classification System.					7				
		コ		oracorrection system.									
		\dashv			ĺ	Ì							
		\exists							<u> </u>				
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							Hole No.	A-1	
	ING LO	C DI.	vision South Atlantic	Hunt	ATION er.AAF	, Geor	gia	SHEET OF 1	I SHEETS
h PROJECT	g 710	- Site	Investigation	10. SIZE	AND TYPE	OF BIT	3 1/2" Hand A	uger	
2. LOCATION See P		stee or Sta	dion)		MSL				
3. DRILLING				IZ. MANI			GNATION OF DRILL		
		strict		13. TOT	HADO AL NO. OF DEN SAMPI	Auger over-	DISTURBED	UNDIST	URBED
4. HOLE NO.	nb=c)	on prawi	A-1	ļ	DEN SAMPI			0	
5. NAME OF Douglas		ho			VATION GE			٠	
6. DIRECTION				-				MPLETE	.D
VERTIC	AL	NCLINED	DEG. FROM VERT.	16. DATI				May 9	1
7. THICKNES	OF OVE	RBURDE	5.0				LE 19.35		
a. DEPTH DR	LLED IN	TO ROCK	0.0	L	AL CORE F		Y FOR BORING		
S. TOTAL DE	PTH OF I	IOLE	6.0	Da	vid C.	Leeth	, Geologist		
ELEVATION	DEPTH b	LEGEND	CLASSIFICATION OF MATERIA (Description)	LLS	Well Const- ruction	BOX OR SAMPLE NO.	REMAI (Drilling time, well weathering, etc.,	er loss, de	epth of canú
						,	9		
			•				Depth to wa		5.01
19.35'			Gravel fill material.				1	6.	٠.٧ ١
18.85'	⇉		(SM)SILTY SAND, brown	and +			Water level	readi	ing
:		1212	loose, fine-very fine				24 hours af	ter ho	ole
	コ		w/20% silt & 5% clay.				completion:	3.63	•
1.	_ =	75/2	(SC) CLAY SAND, grey, st:				Continui 1	fa= -	noro
17.35'	2	ŢŢŢŢ	very fine grained, w/5		_		See HTW log		mor e
16.85'	⇉	Ĭ ┪┦┪╏	clay.				THEOTIMACTON	•	
		:	(SM)SILTY SAND, grey, lo	oose.		<u> </u>			
1	=	:[][]	fine-very fine graine		_	A-1-1			•
			15% silt. Moist.						
] .	4 —	: 	(ML) INORGANIC SILT, dan		m/				
		. 	black, med lean, w/trace	e of					
			sand.						
<u> </u>	\exists	11115	Saturated.						
13.85	\exists		Roots.						
13.35'	6	11114	10% sand.	ㅓ		- 			
	\exists		Black, loose, very fine	grain	-				
	\exists		ed sand w/40% silt.						
	=		Bottom of Hole = 6.0'						
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	\exists	l		ļ					
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	\exists								
	3	ĺ						÷	
	\exists		NOTE CAST	, ,	į				
[. [\exists		NOTE:Soils visually fi classified in accordan	erq					
	4		with the Unified Soil.			.			
	\exists	ł	Classification System.						
	크	į		·		•			
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Det	LING LOG	DIVISION		LATION			No. A-2
1. PROJEC		South Atlantic		ter AAI			OF, 1 SH
Buildi 2. LOCATIO	ng 710 - Si	te Investigation	10. SIZI	e and typ Tum for E MSI	CEAYLO	3 1/2" На ч зно wн <i>(там</i>)	and Auger ~ MSL)
See	Plan G AGENCY		12, MAN	UFACTUR	ER'S DESI	GNATION OF D	RILL
Sava	annah Distri		12		A ger	DISTURBED	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
4. HOLE NO and file :	D. (As shown on pr rumber)	A-2	13. TOT	TAL NO. OF	OVER-	EN 1	UNDISTUR 0
	F DRILLER s LaRoche	<u> </u>		AL NUMBI		BOXES -	lelow.
6. DIRECT	ON OF HOLE					ATED	COMPLETED
Z VERT	TICAL INCLIN	ED DEG. FROM VER	r•	E HOLE		May 91	6 May 91
	ESS OF OVERBUR					LE 19.62'	
	PRILLED INTO RO	· · · · · · · · · · · · · · · · · · ·	19. SIGN	ATURE O	FINSPECT	Y FOR BORING	
9. TOTAL	PEPTH OF HOLE	5.0'	D			, Geologis	st
ELEVATIO	N DEPTH LEGE	CLASSIFICATION OF MATER (Description)	IALS	Well Const- ruction	BOX OR SAMPLE NO.	(Drilling tim	REMARKS e, water loss, depth , etc., il etgnificant g
						Depth to	
19.62'	0 -			 		during	drilling: 3
] =	(SM)SILTY SAND, brown fine to very fine gr				Water 1	evel reading
	- ∃∳ ! ∳	w/10% silt, moist.	,			24 hour	s after hole
	∃ †፤ †	Tan.				complet	ion: 3.31'
	2 -	, , , , , , , , , , , , , , , , , , ,	•				log for mor
		Very moist. Some black lenses.	-			informa	tion.
	=	Dome Black lenses.	_		A-2-1		
]]	Brown & tan. Saturat	ed. —				
	4	Brown,w/some roots.2	5% silt		.		
	∃ ! ∮ !	Saturated.					
14.62'	- [•]					<u>-</u>	
		Bottom of Hole = 5.0	•			- -	
	6			ĺ			
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] =						
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		NOTE: Soils visually f	ield				
		classified in accorda					
		Classification System					
	=						
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	•	<u> </u>		<u> </u>	<u> </u>		

								Hole No. A-3	
		DRIL	LING LOG	South Atlantic	HUN	LATION ter AAF	Ceor	SHEETI	
	1	I. PROJECT						gia of l sheet 3 1/2" Hand Auger	<u>3</u>
	<i>}</i>		ng 710 - Sit N <i>(Coordinates or S</i>	e Investigation	11. DAT	UM FOR E	LEVATION	N SHOWN (TBM or MSL)	7
	,	See 1	Plan		12. MAN	MSL		GNATION OF DRILL	4
22.2		3. DRILLING Savai	AGENCY nnah Distri	ct		Hand A	uger		
			(As shown on gra		13. TOT	AL NO. OF DEN SAMP	OVER-	EN 1 0	
		S. NAME OF				AL NUMBE			7
	•	Douglas	LaRoche		15. ELE	VATION G		ATER See Below	
				DEG. FROM VERT	16. DAT	E HOLE		May 91 6 May 91	
		7. THICKNES	S OF OVERBURD	EN 5.01	———	VATION TO			_
		8. DEPTH DE	RILLED INTO ROC	× 0.0¹		AL CORE		Y FOR BORING	긔
		9. TOTAL DI	EPTH OF HOLE	5.01	Da	avid C.	Leeth	, Geologist	
		ELEVATION d	DEPTH LEGEN	CLASSIFICATION OF MATERI (Description)	ALS	Well Const- ruction		REMARKS (Drilling time, water lose, depth of westhering, etc., if significant)	
									,
								Depth to water during drilling: 4.0'	
		18.97'	0 =	Gravel fill				during driffing. 4.0	4
		18.47	= 111	(SM) SILTY SAND, brown,	loose	†		Water level reading	ŧ
			l ∃I∤I.	fine-very fine grains		*		24 hours after hole completion: Caved	-
-	,		□ ∃ [†]{	silt.	-				þ
)		2 -	Brown & tan. Moist	<u> </u>	<u> </u>		See HTW log for more information.	E
	•		∃ ∳ I ∳ I	Brown, very moist.	_ :				F
		15.97'		Tan.	— r		A-3-1		F
				Brown & tan.				-	F
			4 -]	(SP) POORLY GRADED SAN	•	₽,			
			- 1111	loose, very fine grain	<u>ea.</u> _				E
		13.97'		Saturated.					_
			3	(SM)SILTY SAND, tan, lo very fine grained, w/l					F
	•		6	silt.					E
		}		Bottom of Hole = 5.0					þ
									-
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			3				-	ı	-
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									E
			彐						-
		•	⇉			:			F
		,	7]		
			\exists	NOTE:Soils visually find classified in accordant					F
)			with the Unified Soil		ł			
			=	Classification System					E
		<u> </u>							E
									F
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Building 710 - Site Investigation 2. Location (Coordinates or Station) See Plan 3. DRILLING AGENCY Savannah District Hunter AAF, Georgia 10. SIZE AND TYPE OF BIT 3 1/2"Hand Auger 11. DATUM FOR ELEVATION SHOWN (TBM or MSL) MSL 12. MANUFACTURER'S DESIGNATION OF DRILL Hand Auger	e							Hole No.	A4	
Building 710 - Site Investigation 10. SIZE AND TWO OF BUT 3 1/2" Hand Auger 11. GATUM FORTICEATION SHOWN THE AUGUST 12. CACATION (Coordinates of Station) 12. CACATION (Coordinates of Station) 13	DRILL	.ING LC	og □				Cent	ന്ദ	SHEET	
LOCATION Coordinates as Serious LOCATION FOR Coordinates as Serious LOCATION Coordinates as Serious LOCATION Coordinates as Serious LOCATION Coordinates as Serious LOCATION Coordinates as Serious LOCATION Coordinates as Serious LOCATION Coordinates as Serious LOCATION Coordinates as Serious LOCATION Coordinates as Serious LOCATION Coordinates as Serious LOCATION Coordinates as Serious LOCATION Coordinates as Serious LOCATION COORDINATES LOCATIO					<u> </u>		*			HEETS
See Plan 10. ORILLING AGENCY Savannah District A-4 11. MORAN PROPERTY SESSIONATION OF GRILL 12. AND OF ORILLE A STANDARD OF GRAND (11.5) 13. AND OF ORILLE BOUNDARY AND OF COMPANY AND O	Building	g 710	- Site	Investigation	11. DAT	UM FOR E	EVATION	SHOWN (TON OF HELL))	
1. DATE LING ABENCY 1. MANUFACTURET'S DESIGNATION OF DRILL	See P	(Coordin lan	ales or St	etion)						
A-4 1. TOTAL NO. OF OVER- BURGER SAMPLES TAKE. 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL HUMBER CORE BOXES 1. TOTAL CORE RECOVERY FOR BORING 1. TOTAL CORE RECOVERY	3. DRILLING	AGENCY			12. MAN			GNATION OF DRILL		
14.29' 1. TOTAL NUMBER CORE BOKES DEC. FROM VERT. 1. SELEVATION GROUND WATER See Below DEC. FROM VERT. 1. DATE HOLE TYMENTES OF OVERBURDEN 8.0' 1. DEC. FROM VERT. 1. DATE HOLE TYMENT OF PHOLE 1. DATE HOLE TYMENT OF PHOLE 1. DATE HOLE TYMENT OF PHOLE 1. DATE HOLE TYMENT OF PHOLE 1. DATE HOLE TYMENT OF PHOLE 1. DATE HOLE TYMENT OF PHOLE 1. DATE HOLE TYMENT OF PHOLE TYMENT OF					13. TOT				UNDISTU	RBED
Douglas LaRoche A DIRECTION OF NOLE CYCRITICAL INCLINED DEC. FROM VERT. THICKNESS OF OVERBURDEN 8.0' II. DATE HOLE 18.79' THICKNESS OF OVERBURDEN 8.0' III. TOTAL CORE RECOVERY FOR BORING B. TOTAL DEPTH OF HOLE 8.0' III. TOTAL CORE RECOVERY FOR BORING BELEVATION DEPTH LEGEND CLASSIFICATION OF MATERIALS Continue time, water seasons CHASSIFICATION OF MATERIALS Continue time, water seasons CHASSIFICATION OF MATERIALS Continue time, water seasons CHASSIFICATION OF MATERIALS Continue time, water seasons CHASSIFICATION OF MATERIALS Continue time, water seasons CHASSIFICATION OF MATERIALS Continue time, water seasons CHASSIFICATION OF MATERIALS Continue time, water seasons CHASSIFICATION OF MATERIALS Continue time, water seasons CHASSIFICATION OF MATERIALS Continue time, water seasons CONTINUE SAND, brown, orange Loose, very fine grained, w/ lox sit. Brown & tan, moist. Brown & tan, moist. Brown & tan, with a tan, water seasons CA-4-1 Water level readir 24 hours after hole completion: Caved Caved fill. Water level readir 24 hours after hole completion: Caved Caved fill. Continue time, water seasons CA-4-1 Water level readir CA-4-1 Water level readir CA-4-1 Water level readir CA-4-1 Water level readir CA-4-2 CA-4-1 Water level readir CA-4-1 CA-4-1 Water level readir CA-4-2 CA-4-1 Water level readir CA-4-1 CA-4-1 CA-4-2 CA-4-	and file mus	nbee)	··· cas paralle		BUR	DEN SAMP	LES TAKE	EN 2	<u> </u>	0
A. DIRECTION OF HOLE STARTED DEG. FROM VERT. 18. DATE HOLE T May 9 TO MAY 9 TO MICHAESS OF OVERBURDEN 8.0' 19. TOTAL CORE RECOVERY FOR BORING 19. TOTAL CORE RECOVERY FOR BORING 19. TOTAL CORE RECOVERY FOR BORING 19. TOTAL CORE RECOVERY FOR BORING 19. TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. TOTAL CORE RECOVERY FOR BORING 19. TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING 19. SIGNATURE OF INSECTOR TOTAL CORE RECOVERY FOR BORING TOTAL CORE RECOVERY FOR BORING TOTAL CORE RECOVERY FOR BORING TOTAL CORE									- '	
THICKINESS OF OVERBURDEN 8.0' 1. THICKINESS OF OVERBURDEN 8.0' 2. THICKINESS OF OVERBURDEN 8.0' 3. TOTAL DEPTH ORILLED INTO ROCK 0.0' 3. TOTAL DEPTH OF HOLE 8.0' 10. TOTAL CORE RECOVERY FOR BORING DAVID CONTROL 10. SOLD OF CONTROL 10. SOLD O					13. ELE	VATION GI				
Depth to water during drilling: 6 (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. 18.29' 18.29' 18.29' 18.30' 18.40	VERTIC	AL []	NCLINE	DEG. FROM VERT.	16. DAT	EHOLE		1		
8. OFPH DRILLED INTO ROCK 0.0' 8. TOTAL DEPTH OF HOLE 8.0' CLASSIFICATION OF MATERIALS DEVINE CONTROL OF MATERIALS (Constitution of Materials) 18.79' 18.29' Cravel fill. (SM) SILTY SAND, brown, orange loose, every fine grained, w/ 10% silt. Brown & tan w/trace of clay Very moist. No clay. 4	7. THICKNESS	OF OVE	RBURDE	N 9 01	17. ELE	VATION TO	P OF HO	LE 18.79'		
ELEVATION DEPTH LEGEND CLASSIFICATION OF MATERIALS David C. Leeth, Geologist CLASSIFICATION OF MATERIALS Well SAMPLE Control SAMPLE Control SAMPLE Control SAMPLE Control SAMPLE Control SAMPLE CONTROL SAMPLE CONTR										*
ELEVATION DEPTH LEGEND CLASSIFICATION OF MATERIALS COAST- (Description) (STATE INC. MICH	. TOTAL DE	PTH OF I	HOLE							
18.79' 18.29' Cravel fill. Depth to water during drilling: 6	FLEVATION	DEBTH	LECTUS						ıks.	
18.79' 0 Cravel fill. (SM)SILTY SAND, brown, orange loose, very fine grained, w/ 10% silt. Brown & tan, moist. Brown & tan w/trace of clay. Very moist. No clay. Brown & tan. (ML) INORGANIC SILT, black, meil, organic rich, lean. Trace of sand. Saturated. (SM)SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil.	į					Const-	SAMPLE NO.	(Drilling time, wate	r loss, dem	th of
18.79' 18.29' Gravel fill.				d		•		9		
18.79' 18.29' Cravel fill.		\exists						Depth to was	ter	
Cravel fill. (SM)SILTY SAND, brown, orange loose, very fine grained, w/ 10% silt.	18.79	ه ــــا				<u> </u>		during dril	ling: 6	.41'
CSM/SILTY SAND, brown, orange loose, very fine grained, w/ 10% silt. Brown & tan, moist.	1	=		Gravel fill.						_
10.79 Into graine, with the grainet, with the unified Soil. 2		\exists	+ [+]							
Brown & tan, moist. Brown. Brown & tan w/trace of clay Very moist. No clay. Brown & tan. (ML) INORGANIC SILT, black, med, organic rich, lean. Trace of sand. Saturated. (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil.			† [†]		ed,w/					е.
Brown. Brown & tan w/trace of clay Very moist. No clay. Brown & tan. (ML) INORGANIC SILT, black, med, organic rich, lean. Trace of sand. Saturated. (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil.		ヨ	·┿┇┿┇┆		i			comprecion.	ouvee	
Brown & tan w/trace of clay Very moist. No clay. Brown & tan. (ML) INORGANIC SILT, black, mell, organic rich, lean. Trace of sand. Saturated. (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. NOTE: Soils visually field classified in accordance with the Unified Soil.		2 —	+] +] }		_			See HTW log	for mo	re
Very moist. No clay. Brown & tan. (ML) INORGANIC SILT, black, med, organic rich, lean. Trace of sand. Saturated. (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. 10.79' Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil.		耳	†[†]		- _{clav}		Ī	information	•	
No clay. Brown & tan. (ML) INORGANIC SILT, black, meil, organic rich, lean. Trace of sand. Saturated. (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil.		7	†]†]				İ			
Brown & tan. (ML) INORGANIC SILT, black, med, organic rich, lean. Trace of sand. Saturated. (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil.			†	→ very moist.	_					
Brown & tan. (ML) INORGANIC SILT, black, med, organic rich, lean. Trace of sand. Saturated. (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil.		=	┊┪┇┪	No clay.			A-4-1			
organic rich, lean. Trace of sand. Saturated. (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil.		4 —	† ↓†↓}	Brown & tan.	-		A-4-1			
organic rich, leam. Trace of sand. Saturated. (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil.	14 29'		<u> </u>	(MI) INODCANIC SILT blo	ok mar	,				
Trace of sand. Saturated. (SM)SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE:Soils visually field classified in accordance with the Unified Soil.	14.27	\exists			ck, met	*,	A-4-2	<i>(</i>		
Saturated. 12.29'		\exists	1111		-	Ţ				
12.29' (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil		∄		iface of Sand.	İ		İ			
12.29' (SM) SILTY SAND, brown & tan, loose, very fine grained, w/40% silt. Bottom of Hole = 8.0' NOTE: Soils visually field classified in accordance with the Unified Soil	1	6	╎╎╎┼	Saturated.	ļ	ļ				
NOTE:Soils visually field classified in accordance with the Unified Soil.	12.291	+	╁╅╁╅╫			ļ	į			
NOTE:Soils visually field classified in accordance with the Unified Soil		그	I+I+I	· · · · · · · · · · · · · · · · · · ·			Ī			
Bottom of Hole = 8.0' NOTE:Soils visually field classified in accordance with the Unified Soil		コ	<u></u> ∮Ĭ∳Ĭ		-,	-	- 1			
Bottom of Hole = 8.0' NOTE:Soils visually field classified in accordance with the Unified Soil	10 70	。井	┇┿┇┿╽	•		1				;
NOTE:Soils visually field classified in accordance with the Unified Soil	10./9/	°		Bottom of Hole = 8.0						·
classified in accordance with the Unified Soil	-	7				ŀ				
classified in accordance with the Unified Soil.		\exists								
classified in accordance with the Unified Soil.		\exists								,
classified in accordance with the Unified Soil		\Box	1			.				- 1
classified in accordance with the Unified Soil		=		MOMB C	- 1	1				Ī
with the Unified Soil.		7		NOTE: Soils visually fie	eld			-		
		-7		with the Unified Soil	e	1	1			Ī
		\exists								Ī
		7]	ĺ	•		[
		\exists					}		-	<u> </u>
		\exists				1				
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	1	7	1		1	ļ	I			L

							Hole No	A-5			
DRILLING L	.og		South Atlantic	Hunt	ATION er AAF	, Geor		of 1 sheets			
PROJECT				10. S17£	AND TYPE	OF BIT	3 1/2" Hand	Auger			
Building 710			Investigation	II. DATI	IN FOR EL	EVATION	SHOWN (TBM or ME	(L)			
See Plan	mates or	r o tad	ion.	MSL 12. MANUFACTURER'S DESIGNATION OF DRILL							
DRILLING AGENC					Hand A						
HOLE NO. (A. ale			a title!	13. TOTAL NO. OF OVER- DISTURBED UNDISTUR BURDEN SAMPLES TAKEN 1 0							
and His mumber			A-5		AL NUMBE			<u> </u>			
							TER See Bel	ow			
Douglas LaRed DIRECTION OF H		NED.	DEG. FROM VERT.	16. DAT		7	May 91	7 May 91			
THICKNESS OF O				17. ELE	VATION TO	P OF HO	LE 19.10'				
DEPTH DRILLED			<u> </u>				Y FOR BORING	_			
TOTAL DEPTH O			6.0'	19. SIGN Da	ATURE OF	Leeth	, Geologist				
LEVATION DEPT	H LEGE	END	CLASSIFICATION OF MATERIA (Description)	LS		BOX OR SAMPLE	(Dellling time, w	ARKS			
a b	c		d		ruetion	NO.	weathering, et	c. if eignificant)			
	#					1	Donth to	nater.			
,,,,,	7		٠.				Depth to w	ater [] [] [] [] [] [] [] [] [] [] [] [] [] [
19.10' 0 -	- 11	I	(SM)SILTY SAND, brown,	Loose,							
	∃∳I∳	It	Tine-very fine graine				Water leve				
	╛┩┇┥	Įŀ	10% silt, moist.	-		1	1	fter hole			
	∃ ∳┇┿	ĬĹ	Brown & tan.	-			completion	1: 4.40			
17.10' 2-	<u>-</u> +]+		Brown.				See HTW lo	og for more			
17.10' 2 -	- 11	T	Brown & orange.			ŀ	informatio	-			
	∃ 	$\ \cdot\ '$	(MH) INORGANIC SILT, bl:								
	□ 		soft, organic rich, fat	•							
	7		10% sand.	_							
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	7 11			 _		A-5-1					
15.10' 4 -	- 11	M	(SM) SILTY SAND, black,	loose, 5%]					
	╕╅┇┥	∤Ĭŀ	very fine grained, w/4.	% د		1					
	∃ ∤1 ∮	ŀĪŀ		_			•				
	⋺┝Ӏ┥	I	Saturated.	-							
13.10' 6-	<u> </u>		Tan,25% silt.								
12.10. 0 -		T	Bottom of Hole = 6.0'				•				
	⇉				!						
-	#										
	=										
	7										
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	7										
-	7										
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			NOTE:Soils visually fi	ادام							
	∃		classified in accordan	931							
			with the Unified Soil.					•			
ļ			Classification System.								
	7										
	7										
	7					[
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	ING LOG	IVISION South Atlantic	instal. Hun	ter AAF	, Geor	Hole No	SHEET I		
1. PROJECT Buildin	g 710 - Site	Investigation		AND TYP		I SHOWH (TBM or MS	<i>T</i>		
2. LOCATION See F	(Coordinates or St	ation)	MSL						
3. DRILLING	AGENCY		12. MANUFACTURER'S DESIGNATION OF DRILL 3½-inch Hand Auger						
	mah Distric		13. TOT	AL NO. OF DEN SAMP			UNDISTU		
<u> </u>		A-7	ļ <u></u>	•			. 0		
Douglas			14. TOTAL NUMBER CORE BOXES 15. ELEVATION GROUND WATER See Below						
Douglas			16. DAT	EHOLE	i		OMPLETED		
 		DEG. FROM VER		VATION TO		· · · · · · · · · · · · · · · · · · ·	3 May 91		
	S OF OVERBURDE	0.0	ļ	—		Y FOR BORING	_		
 	PTH OF HOLE	6.0'	19. SIGN	ATURE OF	INSPECT	OR , Geologist			
		<u> </u>		Well	BOY OR	, pen	ARKS		
ELEVATION	DEPTH LEGENO	(Description)	IIALS	Const- ruction	SAMPLE	(Drilling time, we weathering, etc.	ter loss, dept		
19.06'	0					Depth to w			
		(SM)SILTY SAND, brown very fine grained, w/silt, moist.				Water leve 24 hours a	fter hole		
	2	Dark brown.				completion See HTW lo			
•		25% silt,very moist.	<u> </u>			informatio	n.		
	4	Saturated.			A-7-1	·			
		Light brown, roots.							
13.06'									
	1	Bottom of Hole = 6.0	•						
		·							
				_		••			
		NOTE:Soils visually	ield						
		classified in accordance with the Unified Soi Classification System	ince L.						
	=	January Cystel	•						

DRIL	LING LO	G DI	vision South Atlantic	Hole No. A-9 INSTALLATION Hunter AAF, Georgia OF 1 SM						
1. PROJECT										
Buildín 2. LOCATIO	g 710 -	- Site	Investigation	11. DAT	UM FOR E		3 1/2" Hand Au shown (TBM or MSL)	ger		
See	Plan			12. MAN			GNATION OF DRILL	·-·		
i DRILLING Sava	nnah Di	strici				Auger				
4. HOLE NO.	(As shown			13. TOT	AL NO. OF DEN SAMP	OVER-	N DISTURBED	ONDIX.		
S. HAME OF	DRILLER					R CORE E				
Dougla	s LaRoc	che		15. ELE	VATION G		TER See Below			
			DEG. FROM VE	VERT. 18. DATE HOLE 7 May 91 7 May 91						
7. THICKNES	S OF OVE	RBURDE	N 6.0'	17. ELEVATION TOP OF HOLE 18.08						
8. DEPTH DE	HLLED INT	TO ROCK				RECOVER	Y FOR BORING			
9. TOTAL DE	PTH OF H	OLE	6.0'	Da	avid C.	Leeth	, Geologist			
ELEVATION	DEPTH		CLASSIFICATION OF MATE (Description)	RIALS	ruction	BOX OR SAMPLE NO.	REMAR (Drilling time, water weathering, etc., i	loss. d		
		С .		·	 •	<u>'</u>	9	·		
							Depth to wat			
18.08'	0 -	1414	(SM)SILTY SAND,ligh	t brown	 		during drill	.ing:		
	· =	†	loose, fine grained				Water level	read:		
٠ ,	\exists	†	silt. Moist.		1		24 hours aft	er h		
	\exists	I+I+l	Some orange.	,	}		completion:	2.15		
	2]	I+I+l	Tan w/trace or oran	ge,	1		See HTW log	for		
	- ∃;	IțIțl	very moist.			أحجا	information.			
	· = ;	Ĭ ∳ <u>Ĭ</u> ∳┆	Tan & grey,w/trace	or orang	P.	A-9-1				
	<u> </u>	Į┿┇┿┟	Grey, w/some wood. S	aturated						
	= 1,	┧ ϯ┇┿╏	Grey & tan.							
14.08'	4 —	┊ ╇╏╋╏	(MH) INORGANIC SILT,	black. L						
13.58'	∃.	┍┼╁┞┤	soft,fat,w/roots,or							
		 † 	rich.							
10 501	∃.		(SM)SILTY SAND, blac							
12.58'	_ = = = = = = = = = = = = = = = = = = =	7.3.3	very fine grained, w silt, organic rich, w							
12.08'	6									
	ヸ		(SP)POORLY GRADED S white,loose,very fi	, ,	<u>'</u>					
	\dashv		ed.							
	\exists		Bottom of Hole = 6.	0'						
	_=									
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-	⇉									
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	コ		NOTE:Soils visually	field						
			classified in accord	ance						
	二	1	with the Unified Soi	.1.	•	1				
	크		Classification Syste	m. ,						
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	LING LO	SC		ı Atlar	ntic			ter AAI	F, Geor	gi	.a		T 1 SHEET	73	
PROJECT Buildin	g 710	- Site	Inve	stigat	ion			E AND TYP	E OF BIT	<u> </u>	1/2" Hand Au		J., L.	<u> </u>	
See F	Plan		mion)				1.	MSI	-		4.710U ca -			_	
DRILLING		istric					'*. MA'	Hand A	uger	IUN	ATION OF DRILL				
HOLE NO.							13. TO1	TAL NO. OF	FOVER-	EN	DISTURBED	;	STURBED	,	
NAME OF					A-10)	14. TOTAL NUMBER CORE BOXES								
Dougla							15. ELE	VATION G	ROUND W	ATE	R See Below	'			
DIRECTION			·		DEG. F	OM VERT.									
THICKNES	S OF OVE	RBURDE					17. ELEVATION TOP OF HOLE 18.661								
DEPTH DR							19. SIG	ATURE O	F INSPECT	TOR	<u> </u>				
TOTAL DE	PTH OF	HOLE	6.0				-			<u> </u>	Geologist			_	
LEVATION	DEPTH 6	LEGEND	C		ATION O Descript	F MATERI.	ALS	Well Const- ruction	BOX OR SAMPLE NO.		REMAR (Drilling time, water weathering, etc.,)	r loes.	depth of		
	=						-			Ī				_ ¬	
18.66'	0 —	1111									Depth to wat during drill	er Ling:	4.78	,	
	\exists	1 + 1 +				,brown		,			Water level	T 00-	line		
	\exists	IţIţ		se,ver		ne grain	ned,w/				24 hours aft				
i	コ	I † I †	·	wn,moi						completion:	4.27	7 '			
	٦_ إ	++++		ck.							See HTW log	for	поте		
	2 =	1111	35% silt, very moist.								information.		TOTE		
[] † [†]	Roo	te	,										
	\exists	 		urated						-					
	4	† [†]	Jal	31 a L E U	•				A-10-1						
	コ	† [† [40%	silt.			•	-							
	_=	1 1 1													
ľ	\exists	1111													
	_ =	ItItl	20%	silt.			_								
12.66'	6 -	<u> </u>	R	tom of	Hala	= 6.0			 	-				-	
	\exists		304	rom oi	поте	- 0.0	•			•					
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	크		with	the U	nifie	d Soil.				!					
	=		Clas	sifica	tion	System.				:					
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	\exists									ı					
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DRILL	ING LO	G DIV	vision South Atlantic	INSTALL		Coor	Hole No.	SHEET
I. PROJECT			South Atlantic		er AAF		4"ID Hollow St	or l SHEET
Building	g 710	- Site	Investigation	TI. DAT	UM FOR EL	EVATION	3 1/2" Hand	
2. LOCATION See P		stee or Ste	tion)	12 MAN	MSL		GNATION OF DRILL	1 Auget
3. DRILLING				1'	CME		ONATION OF DRIEE	
4. HOLE NO.	(As shows	strict		13. TOT BUR	AL NO. OF DEN SAMP	OVER-	IN 2	UNDISTURBED
S. NAME OF C				-	AL NUMBE			
Dougla				15. ELE	VATION GE			MPLETED
			DEG. FROM VERT.		E HOLE	7	May 91 7	May 91
7. THICKNESS	OF OVE	RBURDEN	6.0'				LE 18.081	
8. DEPTH DR	ILLED IN	TO ROCK	0.0'	19. SIGN	ATURE OF	INSPECT	Y FOR BORING	 _
9. TOTAL DE	PTH OF I	10LE	6.0'	Da	vid C.	Leeth	, Geologist	
	DEPTH	LEGEND	CLASSIFICATION OF MATERIA (Description)	ALS	Well Const- ruction	BOX OR SAMPLE NO.	REMAR (Drilling time, water weathering, etc.,	r loss, depth of
c		· ·	d		•		8	
10.001							Depth to wat	er Ling:4.15'
18.08'	\equiv	4141	(SM)SILTY SAND, dark b	rown,			Γ	
	\exists	+1+11	loose, fine-very fine		·		Water level	
,		+	ed,w/10% silt.				24 hours aft completion:	
	\exists	+	Moist.				Completion:	2.02
	2	+I+IL	Light brown, very moi	ST.]		See HTW log	for more
	_ =	$\phi [\phi]$	Brown & tan.		<u> </u>	ļ	information	•
	⇉	+ [+ []	Brown,40% silt.		1	MW-9-1		
15.08'	<u></u>	-' 	(MH) INORGANIC SILT, bl	ack.	1			
	⇉		soft, organic rich, fat		at-	MW-9-2	-	
14.08'	4 —	,,,, ,	ed.					
	7	ItItl	Roots.			1		
	⇉	I † I †	(SM)SILTY SAND, black					
	\exists	I † I †	very fine grained,w/4	U%		}		
	\exists] †] † İ	Black.					
12.08	6	I	Grey	— _Г				
	\exists				1] ;		
			Bottom of Hole = 6.0'					
	ᆿ							
	\exists		-		:			
	ᆿ							•
	コ							
1 . 1				;				
	コ							
	\exists							
	\exists		NOTE: Soils visually for					
			classified in accordant with the Unified Soil					
	コ		Classification System					
	コ		,					
1								
1 t		- 1						
	コ	1			i			

D-2 - HTW BORING LOGS

•

ON HTW BORING LOGS

ODOR

}

N = NONE

T = TRACE

SL = SLIGHT

M = MEDIUM

ST = STRONG

VS = VERY STRONG

MOISTURE CONTENT

V.D. = VERY DAMP

MST. = MOIST

V.MST. = VERY MOIST

SAT. = SATURATED

COLOR

BK = BLACK

BRN = BROWN

GRA = GRAY

ORG = ORANGE

YLW = YELLOW

WHT = WHITE

DK = DARK

LT = LIGHT

MATERIAL

GVL = GRAVEL

ASP = ASPHALT

CON = CONCRETE

SP = POORLY GRADED SAND

SM = SILTY SAND

SC = CLAYEY SAND

MH = INORGANIC SILT (FAT)

ML = INORGANIC SILT (LEAN)

CH = FAT CLAY

CL = LEAN CLAY

PROJE	CT:	BUILDIN	G 710								BORING	NΟ	1.41	W - 710 · 1
7 171000			VESTIGAT	ION										N-710-1
LOCAT	ION:	HUNTER	ARMY /	NRFIELI	D, SAV	ANNAH,	, GEOR	GIA			ELEVAT	ION:		(TOH) (TOR)
WATER	LEV	/EL DUR	ING DRI	LLING	4.8	0	2.	4 <i>-</i> HOU	IR WATER LE	VEL	READING	G:	3.57	
WEATH	IER:	PARTLY	CLOUDY	& HO	T, 81°				DRILLER:	JAMES	ROUNTR	EE		
REMAR	KS:	CGI NOT	WORKIN	G					GEOLOGIST	CH	RIS LEETH	ł		
					<u>_</u>	5				PLES	3			
		DE	PTH		FOOT	CONTENT	z		OVA (ppm)		HNU opm)	ΑT	TOP	OF HOLE
ž		i	T.)			δ	15 15		(рр	``	opiii)	С	:GI	2244
SAMPLE NO.	ODOR	•		(1991)	PER	끭	<u>ပ</u> ို		FIELD	FI	ELD	· · · · ·		OVA /
) AM	ᅵ딩				WS	l Ti	SSIF	OR	HEADSPACE	1		LEL	02	(ppm)
"		FROM	то	DATE	BLOWS	MOISTURE	CLASSIFICATION	COLOR	ANALYSIS	ANA	LYSIS	%	%	(ррии)
	SL	0.0	0.4	5/01		-	CON	LT. GRA						
	ST	0.4	1,0	5/01	-	MST.	SM	BRN/ TAN	>1000					>1000
	ST	1.0	1.5	5/01	•	MST.	SM	BRN/ TAN						
	vs	1.5	2.0	5/01	-	MST.	SM	BRN/ TAN	>1000					>1000
	vs	2.0	2.5	5/01	-	MST	МН	BLK						
	vs	2.5	3.0	5/01	-	MST.	SM	BRN/ TAN	>1000					>1000
	vs	3.0	3.5	5/01	-	V.MST	SM	BRN/ TAN			:			
MW-710-1-	ı vs	3.5	4.0	5/01	-	V.MST	SM	BRN/ TAN	>1000					>1000
	vs	4.0	4.5	5/01	-	SAT.	SM	BRN						
ļ <u>.</u>	VS	4.5	5.0	5/01	-	SAT.	SM	BRN	>1000					>1000
	vs	5.0	5.5	5/01	-	SAT.	SM	BRN						
	vs	5 .5	6.0	5/01	-	SAT.	SM	BRN						>1000
	VS	6.0	6.5	5/01	-	SAT.	SM	BRN						
ļ	VS	6 <i>.</i> 5	7.0	5/01	-	SAT.	SM	BRN						>1000
	VS	7.0	7.5	5/01	-	SAT.	SM	BRN						
	vs	7.5	8.0	5/01	-	SAT.	SM	BRN						>1000
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PROJE	CT:	BUILDIN SITE IN	G 710 VESTIGAT	FION							BORING	NO.	M\	w-710-3
LOCATI	ON:	HUNTER	RARMY	AIRFIEL), SAV	ANNAH	, GEOR	GIA			ELEVAT	ION:		5 (TOH) 5 (TOR)
WATER	LEV	/EL DUR	ING DR	ILLING:	3.8	5	2	4-HOL	JR WATER LE	VEL	READING	3:	3.15	
WEATH	ER:	CLEAR 8	COOL,	83*			102		DRILLER:	JAMES	ROUNTR	EE		
REMAR	<s:< td=""><td>CGI NOT</td><td>WORKING</td><td>;</td><td></td><td></td><td>, . </td><td></td><td>GEOLOGIST</td><td>: CHF</td><td>RIS LEETH</td><td>1</td><td></td><td></td></s:<>	CGI NOT	WORKING	;			, . 		GEOLOGIST	: CHF	RIS LEETH	1		
					L	=			SAM	PLES				
NO.		DEF	PTH		FOOT	CONTENT	NO		OVA (ppm)		HNU opm)	AT	TOP	OF HOLE
<u>-</u>	~	(F	T.)	=	PER	1	¥					С	:GI	OVA /
SAMPLE	ODOR			(1991)		MOISTURE	CLASSIFICATION	껉	FIELD HEADSPACE	ŀ	ELD	LEL	02	HNU
Ŝ		 		DATE	BLOWS	Si	S	COLOR		1		0/	.	(ppm)
		FROM	TO	1				-	ANALYSIS	ANA	LYSIS	%	%	<u> </u>
	N	0.0	0.5	5/02	-	DRY	SP	TAN						
	N	0.5	1.0	5/02	-	MST	SP	TAN	0.0	ļ				0.0
	N	1.0	1.5	5/02	-	MST.	SM	TAN						
	N	1.5	2.0	5/02	-	MST.	SM	TAN	0.0		· · · · · · · · · · · · · · · · · · ·			0.0
	N	2.0	2.5	5/02	-	SAT	SM	TAN						
MW-710-3-1		2.5	3.0	5/02	-	SAT.	SM	TAN	0.0					3.0
	SL	3.0	3.5	5/02	-	SAT.	SM	GRA						·
	SL	3.5	4.0	5/02	-	SAT.	SM	TAN/ GRA	0.0					0.0
	SL	4.0	4.5	5/02	-	SAT.	SM	TAN/ GRA						
	SL	4.5	5.0	5/02		SAT.	SM	BRN	0.0					0.0
	SL	5.0	5.5	5/02	-	SAT.	SM	BRN						
	SL	5.5	6.0	5/02	-	SAT.	SM	BRN	5.0					5.0
	SL	6.0	6.5	5/02	-	SAT.	SM	BRN						
	SL	6.5	7.0	5/02	-	SAT.	SM	OK. BRN						38.0
	SL	7.0	7.5	5/02	-	SAT.	SM	DK. BRN						30.0
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	PROJE	CT:	BUILDIN SITE IN	IG 710 IVESTIGAT	TION							BORING		M'	W-710-4
	LOCATI	ON:	HUNTER	R ARMY	AIRFIELI	D, SAV	ANNAH	, GEOR	RGIA			ELEVAT	TION:		TOH) (TOR)
	WATER	LEV	/EL DUR	RING DR	ILLING	3.1	5	2	4-HOL	JR WATER LE	EVEL	READIN	G:	3.30	
	WEATH	ER:	HOT &	CLEAR, 8	5*					DRILLER:	JAMES	ROUNTE	REE		
	REMARI	(S :	CGI NOT	WORKING	;		•			GEOLOGIST	: CHF	RIS LEETS			
							5			SAM	IPLES				
	9		DEI	PTH		FOOT	CONTENT	N O		OVA (ppm)		HNU pm)	AT	TOP	OF HOLE
	SAMPLE NO.	ODOR		T.)	DATE (1991)	BLOWS PER	MOISTURE C	CLASSIFICATION	COLOR	FIELD HEADSPACE	HEAL		LEL	_	OVA / HNU (ppm)
ŀ		<u>.</u>	FROM	TO					LT.	ANALYSIS	ANA	_YSIS	%	%	
ŀ		N	0.0	0.6	5/02	-	-	CON	GRA		<u> </u>				
ŀ		SL	0.6	1.0	5/02	-	MST.	SP	TAN BRN/	600					>1000
ŀ		ST	1.0	1.5	5/02	-	MST.	SM	TAN BRN/						
ŀ		ST	1.5	2.0	5/02	-	V.MST		TAN BRN/	>1000	-				>1000
ŀ		ST	2.0	2.5	5/02	-	V.MST		TAN BRN/						
ř	IW-710-4-1		2.5	3.0	5/02	-	V.MST		TAN	>1000			<u></u>		>1000
ŀ		ST	3.0	3.5	5/02	-	V.MST	<u> </u>	BRN/ TAN						
-		VS	3.5	4.0	5/02	-	SAT.	SM	BRN/ TAN	880		-			>1000
Ļ		VS	4.0	4.5	5/02	-	SAT.	SM	BRN/ TAN	-					
ŀ		vs	4.5	5.0	5/02	-	SAT.	SM	BRN	980					>1000
L		vs	5.0	5.5	5/02	-	SAT.	SM	BRN						
-		VS	5. 5	6.0	5/02	-	SAT.	SM	BRN						>1000
-		VS	6.0	6.5	5/02	-	SAT.	SM	BRN						
ŀ		VS	6.5	7.0	5/02	-	SAT.	SM	BRN						>1000
\mid		vs	7.0	8.0	5/02	-	SAT.	SM	BRN						>1000
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PROJE	CT:	BUILDIN SITE IN	IG 710 IVESTIGA	TION							BORING		***	W-710-5
LOCAT	ION:	HUNTE	RARMY	AIRFIEL	D, SAV	/ANNAH	i, GEOF	RGIA			ELEVA'	TION:		(TOH) (TOR)
WATER	LEV	/EL DUF	RING DR	ILLING	: 3.1	0	2	4-HOU	JR WATER L	EVEL	READIN	G:	3.87	
WEATH	ER:	CLEAR	k HOT, 9	2*					DRILLER:	JAMES	ROUNT	REE		
REMAR	KS:				-				GEOLOGIST	: CHR	IS LEET	H		
NO.			PTH		FOOT	CONTENT	NOI		OVA (ppm)		HNU pm)			OF HOLE
SAMPLE NO.	ODOR		T.)	DATE (1991)	BLOWS PER	MOISTURE C	CLASSIFICATION	COLOR	FIELD HEADSPACE	HEAD		LEL	-	OVA / HNU (ppm)
		FROM	TO	à	<u>a</u>	 	ਹ	 	ANALYSIS	ANAL	YSIS	%	%	
ļ	N	0.0	0.5	5/03	-	DRY	SM	BRN			,			
	N	0.5	1.0	5/03	-	MST.	SM	DK. BRN	0.2			0.0	21.1	0.0
	N	1.0	1.5	5/03	-	MST.	SM	BLK	·····					
<u> </u>	N	1.5	2.0	5/03	-	MST.	SM	BLK	0.0			0.0	20.7	0.0
ļ	N	2.0	2.5	5/03	-	MST	sc	GRA/ BLK						
MW-710-5-1	SL	2.5	3.0	5/03	-	MST.	sc	BLK	0.0			0.0	20.8	1.0
	SL	3.0	3.5	5/03	-	MST.	SC	BLK						
	N	3.5	4.0	5/03	-	MST.	sc	BLK	0.0			0.0	20.9	1.0
	N	4.0	4.5	5/03	_	MST.	SM	BLK						
	N	4.5	5.0	5/03	-	MST	SM	BLK	0.2			0.0	20.7	0.4
	N	5.0	5.5	5/03	-	MST.	SM	TAN/ BLK						
	N	5.5	6.0	5/03	-	MST.	SM	TAN				0.0	20.9	0.4
							-							
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	_						· -							
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	-								<u> </u>	<u></u>				
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Γ	PROJE	CT:	BUILDIN	G 710 VESTIGAT	TIÓN				<u> </u>			BORING	NO.	MV	N-6
-	LOCATI	ON:	HUNTER			D, SAV	ANNAH,	GEOR	GIA	<u> </u>		ELEVAT	ION:		(TOH) 9 (TOR)
	WATER	LEV	ÆL DUR	ING DR	ILLING	: 5.6	1	2	4-HOL	IR WATER LE	EVEL	READING	3:	4.29	
	WEATH	ER:	OVERCA	ST & WA	RM, 80	•				DRILLER:	DOUG	LAS LARO	CHE		
	REMARK		CGI NOT ODOR IS			ERLY				GEOLOGIST	: CHI	RIS LEETH	(
ŀ	ō.		DEI	PTH		FOOT	CONTENT	NO		SAM OVA (ppm)	•	HNU opm)	AT	TOP	OF HOLE
	SAMPLE NO.	ODOR	(F	т.)	TE (1991)	BLOWS PER	MOISTURE CO	CLASSIFICATION	COLOR	FIELD HEADSPACE	Į .	ELD DSPACE	LEL	0 ₂	OVA / HNU (ppm)
			FROM	ТО	DATE	E E	Q _M	겁	8	ANALYSIS	ANA	LYSIS	%	%	
		N	0.0	0.5	5/14	-	MST.	SM	BLK						
		N	0.5	1.0	5/14	-	MST.	SM	BRN	0.2			-7	20.6	0.0
Γ		N	1.0	1.5	5/14	-	MST.	SM	BRN						
		N	1,5	2.0	5/14	-	MST	SM	BLK	6.0			-8	20.5	4.0
	,	N	2.0	2.5	5/14	-	MST.	ML	BLK						
	/W-6-1	N	2.5	3.0	5/14	-	MST.	ML	BLK	22.0			-7	20.6	60.0
		N	3.0	3.5	5/14	•	MST.	SM	BRN						
		N	3.5	4.0	5/14	-	v.MST	SM	BRN	6.2			-7	20.6	50.0
Г		N	4.0	4.5	5/14	•	SAT.	SM	BRN						
Г		SL	4.5	5.0	5/14	-	SAT.	SM	BRN	10.0			-7	20.7	30.0
		SL	5.0	5.5	5/14	•	SAT.	SM	BRN						
		SL	5.5	6.0	5/14	1	SAT.	SM	BRN				-6	20.6	50.0
												!			

BUILDING 710 PROJECT: BORING NO. MW-7 SITE INVESTIGATION ELEVATION: 18.88 (TOH) LOCATION: HUNTER ARMY AIRFIELD, SAVANNAH, GEORGIA 18.68 (TOR) WATER LEVEL DURING DRILLING: 4.54 24-HOUR WATER LEVEL READING: 3.75 WEATHER: OVERCAST & WARM, 78°, GUSTS DRILLER: DOUGLAS LAROCHE REMARKS: ODOR WAS ORGANIC GEOLOGIST: CHRIS LEETH CGI NOT WORKING PROPERLY SAMPLES MOISTURE CONTENT FOOT OVA HNU AT TOP OF HOLE DEPTH Š CLASSIFICATION (ppm) (ppm) BLOWS PER (FT.) (1991) CGI SAMPLE ODOR OVA / FIELD **FIELD** 02 HNU LEL COLOR HEADSPACE HEADSPACE (ppm) % **ANALYSIS** % **ANALYSIS FROM** TO N 0.0 DRY 0.4 5/13 **ASP** BLK/ 0.4 1.0 N 5/13 DRY SM 1.0 0.0 20.7 2.0 TAN BLK/ TAN 1.0 1.5 MST. SL 5/13 SM 1.5 SL 2.0 5/13 MST. SM BRN 0.0 20.7 >1000.0 300.0 SL 2.0 2.5 5/13 V.MST SM BRN SL 2.5 3.0 BRN 5/13 V.MST SM >1000.0 0.0 20.9 >1000.0 MW-7-1 MW-7-1A SL 3.0 V.MST 3.5 5/13 SM BRN MW-7-10 SL 4.0 3.5 SAT. 5/13 SM **BRN** 250.0 -13 20.8 >1000.0 BRN/ SL 4.0 4.5 5/13 SAT. SM SL 4.5 5.0 5/13 SAT. SM 20.0 -8 20.8 200.0 TAN 5.0 Ν 5.5 5/13 SAT. TAN 5.5 Ν 5.0 SAT. SP TAN 5/13 -8 20.9 400.0

												· ·			
)	PROJE	CT:	BUILDIN SITE IN	IG 710 IVESTIGA	TION							BORING			w-8
	LOCAT	ION:	HUNTER	RARMY	AIRFIEL	D, SAV	'ANNAH	, GEOF	RGIA			ELEVAT	ION:		(TOH) (TOR)
	WATER	LEV	/EL DUF	RING DR	ILLING	: 3,6	51	2	4 -HOL	JR WATER LE	EVEL	READIN	G:	3.47	
	WEATH	ER:	PARTLY	CLOUDY	& HO	T, 90°		•		DRILLER:	DOUGI	AS LARC	CHE	·	
	REMAR	KS:	CGI NOT	WORKING	PROP	PERLY		•••		GEOLOGIST	CHF	RIS LEETI	4	•	
Į							L_			SAM	IPLES				,
	ð.		DE	PTH		FOOT	CONTENT	CLASSIFICATION		OVA (ppm)	(DVM opm)	AT	TOP	OF HOLE
١	Г	1~	(F	T.)	€	PER					(CGI	OVA /		
	4	ODOR			(1991)		뀚		FIELD	FI	ELD	LEL	02	1	
-	SAMPLE NO.	0				₩S	S.	HEADSPACE	HEAD	SPACE		1 2	(ppm)		
	•		FROM	ТО	DATE	BLOWS	MOISTURE	COLOR	ANALYSIS	ANA	YSIS	%	%	(ррии)	
		N	0.0	0.5	5/14	-	-	ASP	-					 	
		SL	0.5	1.0	5/14	-	MST.	SM	BLK	200.0		8.0	-5	10.0	50.0
		N	1.0	1.5	5/14	-	MST.	SM	BRN						
		N	1.5	2.0	5/14	-	MST.	sc	GRA	>1000.0	().0	-6	20.5	400.0
		ORG	2.0	2.5	5/14	-	MST.	МН	BLK						
		N	2.5	3.0	5/14	•	V.MST	МН	BLK	200.0	(0.0	0	20.7	>1000.0
	MW-8-1	ORG	3.0	3.5	5/14	-	V.MST	МН	BLK						
		SL	3.5	4.0	5/14	-	SAT.	мн	BLK	>1000.0	1	2.0	-3	20.8	>1000.0
		SL	4.0	4.5	5/14	-	SAT.	мн	BLK						
		SL	4.5	5.0	5/14	•	SAT.	мн	BLK	200.0	C	0.0	-2	20.8	>1000.0
		N	5.0	5.5	5/14	-	SAT.	SM	BLK						
		N	5.5	6.0	5/14	-	SAT.	sc	TAN						
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PROJE	CT:	BUILDIN SITE IN	IG 710 VESTIGAT	rion							BORING	NO.	M'	w-10
LOCAT	ION:	HUNTER	RARMY	AIRFIELI	D, SAV	HANNA'	, GEOF	RGIA			ELEVAT	ION:		(TOH)) (TOR)
WATER	LEV	/EL DUF	RING DR	ILLING	: 4.3	54	2	4-HOL	JR WATER LI	EVEL	READIN	G:	4.88	
WEATH	ER:	OVERCA	ST & WA	RM, 74	•				DRILLER:	DOUGL	AS LARC	CHE		
REMAR	KS:	CGI NOT	WORKING	; 					GEOLOGIST	: CHR	IS LEET	1		
						 				IPLES				
SAMPLE NO.		ŀ	PTH		F001	CONTENT	CLASSIFICATION		OVA (ppm)	t .	INU pm)	AT	TOP	OF HOLE
щ	22	(F	T.)	<u>e</u>	PER		¥					C	GI	OVA /
ΔPL	ODOR			(1991)		본			FIELD	FIE	ELD	LEL	02	ł
SA	0				BLOWS	STL	SS	g	HEADSPACE	HEAD	SPACE			(ppm)
-		FROM	ТО	DATE	BLC	MOISTURE	CLA	COLOR	ANALYSIS	ANAL	YSIS	%	%	1111040111
	N	0.0	0.5	5/07	-	DRY	SP	BRN	<u> </u>					
	N	0.5	1.0	5/07	-	MST.	SP	BRN	0.0					0.0
_	Z	1.0	1.5	5/07	-	MST.	SM	BRN						
	N	1,5	2.0	5/07	_	MST.	SM	BRN/ BLK	0.0					0.0
	2	2.0	2.5	5/07	_	MST.	SM	BLK						
	N	2.5	3.0	5/07	-	MST.	SM	BLK	0.0					0.0
	N	3.0	3,5	5/07	-	MST.	мн	BLK						
· · · · · · · · · · · · · · · · · · ·	N	3.5	4.0	5/07	-	MST.	мн	BLK	0.0					0.0
	N	4.0	4.5	5/07	-	V.MST	мн	BLK						
MW-10-1	N	4,5	5.0	5/07	-	SAT.	МН	BLK	0.0					0.0
	N	5.0	6.0	5/07	-	SAT.	SM	TAN	<u> </u>					
	N	6.0	7.0	5/07	-	SAT.	SM	TAN						0.0
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)	PROJE	CT:	BUILDIA SITE IA	IG 710 IVESTIGA	TION							BORING			IW-11
	LOCAT	ION:	HUNTE	R ARMY	AIRFIEL	D, SAV	'ANNAH	, GEOF	RGIA			ELEVAT	ΓΙΟN:		5 (TOH) 5 (TOR)
	WATER	LE'	VEL DUF	RING DR	ILLING	3.9	88	2	4-HOU	JR WATER LI	EVEL	READIN	G:	3.40)
	WEATH	IER:	PARTLY	CLOUDY	& HO	T, 82°	_			DRILLER:	JAMES	ROUNTE	REE		
	REMAR	KS:	CGI NOT	WORKING	PROF	ERLY				GEOLOGIST	: CHF	RIS LEETI	Н		
	Š.		DE	PTH		PER FOOT	CONTENT	NO		OVA (ppm)		HNU ppm)	AT	TOP	OF HOLE
	SAMPLE NO.	ODOR	(F	T.)	E (1991)	FIELD HEADSPACE		ELD SPACE	LEL	O ₂	OVA / HNU (ppm)				
			FROM	то	DATE	BLOWS	MOISTURE	CLASSIFICATION	COLOR	ANALYSIS	ANA	LYSIS	%	%	фрин
		N	0.0	0.5	5/15	-		GVL	LT. BRN						
	-	N	0.5	1.0	5/15	-	MST.	SM	LT. BRN LT.	0.0			-2	20.6	0.0
		N	1.0	1.5	5/15		MST.	SM	BRN						
1	·	N	1.5	2.0	5/15		MST.	SM	LT. BRN	0.0			-2	20.6	0.0
		N	2.0	2.5	5/15	-	MST.	SM	TAN						
		N	2.5	3.0	5/15	-	V.MST	SM	TAN	0.0			-3	20.7	0.0
		N	3.0	3.5	5/15	-	V.MST	SM	TAN						
	MW-11-1	SL	3.5	4.0	5/15	-	SAT.	SM	TAN	0.0			-2	20.7	20.0
		SL	4.0	4.5	5/15	-	SAT.	мн	BLK						
	· · · · · · · · · · · · · · · · · · ·	SL	4.5	5.0	5/15	-	SAT.	МН	BLK	740.0			-2	20.8	60.0
ſ	MW-11-2	SL	5.0	5.5	5/15	-	SAT.	мн	BLK						
ſ		SL	5.5	6.0	5/15	-	SAT.	мн	BLK/ TAN				-1	20.8	>1000.0
Ī	<u> </u>								17.53		•				
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PROJE	CT:	BUILDIN SITE IN	IG 710 IVESTIGAT	TION					· · · · · · · · · · · · · · · · · · ·		BORING	NO.	. A	- 1
LOCAT	ION:	HUNTER	RARMY	AIRFIELI	D, SAV	'ANNAH	, GEOF	RGIA			ELEVAT	ION:	19	.35
WATER	LE.	VEL DUF	RING DRI	LLING	: 5	.0	2	4-HOL	JR WATER LE	EVEL	READIN	G:	3.63	
WEATH	IER:	MOSTLY	CLOUDY	& HO	T, 88°				DRILLER:	DOUGL	AS LARC	CHE		
REMAR	KS:	 .	<u>.</u>						GEOLOGIST	: CHR	IS LEETI	1		
	1					 			SAM	IPLES				
NO.			РТН		FOOT	CONTENT	CLASSIFICATION		OVA (ppm)		INU pm)	AT	TOP	OF HOLE
Ш	2	(F	T.)	91	PER	1	AT						CGI	OVA /
SAMPLE	ODOR			(1991)		본	FIC		FIELD	FI	ELD	LEL	02	HNU
X	0			1	BLOWS	ST	SS	P.	HEADSPACE	HEAD	SPACE		4	(ppm)
		FROM	TO	DATE	BL (MOISTURE	CL/	COLOR	ANALYSIS	ANAL	YSIS	%	%	(ppills
	N	0.0	0.5	5/06	-	DRY	GVL	-						
	N	0.5	1.0	5/06	-	DRY	GVL	-						
	SL	1.0	1.5	5/06	-	MST.	SM	BRN/ TAN	150.0			0	20.7	1.0
	SL	1.5	2.0	5/06	-	MST.	SC	GRA						
	SL	2.0	2.5	5/06	-	MST.	SM	GRA	40.0			0	20.7	24.0
	SL	2.5	3.0	5/06	-	MST.	ML	BLK						
A-1-1	SL	3.0	3.5	5/06	-	V.MST	ML	BLK	10.0			0	20.7	15.0
	SL	3.5	4.0	5/06	-	V.MST	ML	BLK						
<u> </u>	SL	4.0	4.5	5/06	_	SAT.	ML	BLK	2.0			0	20.8	15.0
	SL	4.5	5.0	5/06	-	SAT.	ML	BLK						
	N	5.0	5.5	5/06	-	SAT.	ML	BLK	0.0			0	20.7	5.0
	N	5.5	6.0	5/06		SAT.	SM	BLK				0	20.6	3.0
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PROJE	CT:	BUILDIN SITE IN	IG 710 IVESTIGA	TION							BORING	NO.	A	-2
LOCAT	ION:	HUNTE	R ARMY	AIRFIELI	D, SAV	/ANNAH	, GEOF	RGIA		1	ELEVAT	ION:	19	9.62
WATER	LEV	/EL DUF	RING DR	ILLING	: 3.	55	2	4-HOL	JR WATER LI	EVEL I	READIN	G:	3.31	
WEATH	iER:	PARTLY	CLOUDY	& HO	T, 86°				DRILLER:	DOUGL	AS LARC	CHE		
REMAR	KS:			· · · · · · · · · · · · · · · · · · ·					GEOLOGIST	: CHR	S LEETI	Η		
NO.		1	РТН		FOOT	CONTENT	NO		OVA (ppm)		NU om)	АТ	TOP	OF HOLE
SAMPLE NO.	ODOR	(F	T.)	DATE (1991)	BLOWS PER	MOISTURE C	CLASSIFICATION	COLOR	FIELD HEADSPACE	FIE HEAD:		LEL	~	OVA / HNU (ppm)
	ļ	FROM	ТО	ΔO	BE	∑ V	ರ	S	ANALYSIS	ANAL	YSIS	%	%	
	N	0.0	0.5	5/06	-	MST.	SM	BRN						
	N	0.5	1.0	5/06	-	MST.	SM	TAN	0.0			0.0	20.9	0.0
<u> </u>	N	1.0	1.5	5/06	-	MST.	SM	TAN						
	N	1.5	2.0	5/06	-	V.MST	SM	TAN	0.0			0.0	20.8	0.0
	N	2.0	2.5	5/06	<u>-</u>	V.MST	SM	TAN						
	N	2.5	3.0	5/06	-	V.MST	SM	TAN BRN/	0.0			0.0	20.9	0.0
A-2-1	N	3.0	3.5	5/06	-	SAT.	SM	TAN				<u> </u>		
	N	3.5	4.0	5/06		SAT.	SM	BRN	0.0			0.0	20.8	0.0
<u> </u>	N	4.0	4.5	5/06	-	SAT.	SM	BRN	0.0			0.0	20.9	0.0
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PROJECT: BUILDING 710 BORING NO. A-3 SITE INVESTIGATION **ELEVATION:** LOCATION: HUNTER ARMY AIRFIELD, SAVANNAH, GEORGIA 18.97 WATER LEVEL DURING DRILLING: 4.0 24-HOUR WATER LEVEL READING: CAVED WEATHER: PARTLY CLOUDY & HOT, 96° DRILLER: DOUGLAS LAROCHE REMARKS: GEOLOGIST: CHRIS LEETH SAMPLES MOISTURE CONTENT BLOWS PER FOOT OVA AT TOP OF HOLE HNU DEPTH **CLASSIFICATION** (ppm) (ppm) (FT.) (1991) CGI SAMPLE ODOR OVA / FIELD **FIELD** LEL 02 HNU COLOR HEADSPACE HEADSPACE (ppm) % % **ANALYSIS** FROM **ANALYSIS** TO Ν 0.0 DRY 0.5 5/06 **GVL** 0.5 1.0 MST. 5/06 SM TAN 0.0 0.0 20.9 0.0 BRN/ 1.0 1.5 5/06 MST. SM N 1.5 2.0 5/06 V.MST SM BRN 0.0 0.0 20.9 0.0 2.0 2.5 5/06 V.MST SM TAN BRN/ TAN 2.5 3.0 V.MST N 5/06 SM 0.0 0.0 20.9 0.0 A-3-1 N 3.0 3.5 5/06 V.MST SW WHT Ν 3.5 4.0 WHT 5/06 SAT. SW 0.0 0.0 20.8 0.0 4.0 Ν 4.5 SAT. 5/06 SW WHT Ν 4.5 5.0 SAT. 5/06 TAN SM 0.0 0.0 20.9 0.0

	PROJE	CT:	BUILDIN	G 710 VESTIGAT	ION				-		BORII	NG NO	· A-	- 4
	LOCATI	ION:	HUNTER), SAV	ANNAH,	GEOR	GIA		ELEV	ATION:	18.	79
	WATER	LE	/EL DUR	ING DRI	LLING:	6.4	-1	2	4-HOL	R WATER LE	VEL READ	ING:	CAVE	.D
Γ	WEATH	ER:	CLEAR 8	WARM,	72°					DRILLER:	DOUGLAS LA	ROCHE		· · · · · · · · · · · · · · · · · · ·
	REMARK	(S:	CGI NOT ODOR IS	WORKING						GEOLOGIST	CHRIS LEE	ETH		
						Ţ	N				PLES		T00	
	o.		DEI	PTH		F00T	CONTENT	<u>×</u>		OVA (ppm)	HNU (ppm)	AI	TOP	OF HOLE
	SAMPLE NO.	_~	(F	T.)	2	PER		CLASSIFICATION			, ,		CGI	OVA /
	APL.	ODOR			(1991)		MOISTURE	FIC		FIELD	FIELD	LEL	02	
	S₽	^				BLOWS	STL	SSI	COLOR	HEADSPACE	HEADSPAC	E	-	(ppm)
			FROM	ТО	DATE	BL (Θ.	ر ا	00	ANALYSIS	ANALYSIS	1%	%	
		N	0.0	0.5	5/07	-	DRY	NA						
		N	0.5	1.0	5/07	-	DRY	SM	BRN/ ORG	0.0				0.0
		N	1.0	1.5	5/07	-	MST.	SM	BRN/ ORG					
		N	1.5	2.0	5/07	•	MST.	SM	BRN/ TAN	0.0				0.0
		N	2.0	2.5	5/07	-	MST.	SM	BRN					
		N	2.5	3.0	5/07	-	MST.	SM	BRN/ TAN	0.0				0.0
L		N	3.0	3.5	5/07	-	V.MST	SM	BRN/ TAN					
	A-4-1	N	3.5	4.0	5/07		V.MST	SM	BRN/ TAN	0.0				0.0
		N	4.0	4.5	5/07	-	V.MST	SM	BRN/ TAN					
	A-4-2	ST	4.5	5.0	5/07	-	V.MST	ML	BLK	220.0				12.0
		\$T	5.0	5.5	5/07	-	V.MST	ML	BLK					
L		ST	5.5	6.0	5/07	-	V.MST	ML	BLK	80.0				20.0
L		ST	6.0	6.5	5/07	-	SAT.	ML	BLK					
L		ST	6.5	7.0	5/07		SAT.	SM	BRN/ TAN	· - · · · · · · · · · · · · · · · · · · ·				19.0
_		SL	7.0	8.0	5/07	-	SAT.	SM	BRN/ TAN				<u> </u>	
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)	PROJE	CT:	BUILDIN	G 710 VESTIGAT	ION							BORING	NO.	A-	
	LOCATI	ION:	HUNTER), SAV	ANNAH,	GEOR	GIA			ELEVAT	ION:	19	.10
	WATER	LEV	ÆL DUR	ING DR	LLING	4.3	JR WATER LEVEL READING: 4.40								
	WEATH	ER:	OVERCAS	ST & WA	RM, 78'	•	DRILLER: DOUGLAS LAROCHE								
	REMARK	<s:< td=""><td>CGI NOT</td><td>WORKING</td><td></td><td></td><td>GEOLOGIST</td><td>CHF</td><td>RIS LEETH</td><td>†</td><td></td><td></td></s:<>	CGI NOT	WORKING			GEOLOGIST	CHF	RIS LEETH	†					
İ						_	Ϋ́Τ			SAM	IPLES				
	O			PTH		FOOT	CONTENT	NO.		OVA (ppm)		HNU opm)			OF HOLE
	PLE	SAMPLE NO.		(FT.)		PER	1 1	CLASSIFICATION		FIELD	FI	ELD	LEL	GI 0 ₂	OVA / HNU
	SA	0			E (1991)	M.S	ĭ	SSI	OR	HEADSPACE	HEAD	SPACE		Z	(ppm)
			FROM	. TO	DATE	BLOWS	MOISTURE	CLA	COLOR	ANALYSIS	ANA	LYSIS	%	%	(рріп)
		N	0.0	0.5	5/07	-	MST.	SM	BRN						
		N	0.5	1.0	5/07	-	MST.	SM	BRN/ TAN	0.0					0.0
		N	1.0	1.5	5/07	-	MST.	SM	BRN						
		N	1.5	2.0	5/07	-	MST.	SM	BRN/ ORG	0.0					0.0
		SŁ	2.0	2.5	5/07	-	V.MST	MH	BLK						
		SL	2.5	3.0	5/07	-	v.mst	мн	BLK	>10000.0					100.0
		SL	3.0	3.5	5/07	-	V.MST	мн	BLK						
	A-5-1	SL	3.5	4.0	5/07	_	v.MST	мн	BLK	800.0					700.0
		ST	4.0	4.5	5/07	-	V.MST	SM	BLK						
		ST	4.5	5.0	5/07	-	SAT.	SM	BLK	30.0					90.0
		SL	5.0	6.0	5/07	-	SAT.	SM	TAN	30.0					60.0
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ELEVATION:														A-6 -710-2)		
	LOCATI	ON:	HUNTER	R ARMY	ARFIELI	D, SAV	HANNAH	, GEOR	GIA		:	ELEVAT	18.58			
	WATER	LEV	/EL DUR	ING DR	ILLING:	: CA	/ED	24	4-HOL	JR WATER LEVEL READING: CAVED						
	WEATH	ER:	CLEAR, V	VINDY &	нот, 8	7*	DRILLER: JAMES ROUNTREE / DOUGLAS LAROCHE									
	REMAR	<s:< td=""><td></td><td></td><td></td><td></td><td colspan="7">GEOLOGIST: CHRIS LEETH</td></s:<>					GEOLOGIST: CHRIS LEETH									
							17	<u>-</u>		SAM	IPLES					
	9		DEI	PTH		FOOT	CONTENT	8		OVA (ppm)		HNU pm)	AT .	TOP	OF HOLE	
	<u>~</u> Ш.	ODOR	(FT.)		=	1 1 1	¥					С	GI	OVA /		
	SAMPLE				(1991)	BLOWS PE MOISTURE	5		FIELD	FI	ELD	LEL	02	HNU		
						BLOWS	STL	MOISTURE CONT	COLOR	HEADSPACE	HEAD	SPACE		2	(ppm)	
			FROM	ТО	DATE	ЭН	ΘW	CLA	100	ANALYSIS	ANA	LYSIS	%	%	(PP111)	
L		-	0.0	0.4	5/02	•	-	CON	-							
		SL	0.4	1.0	5/02	-	MST.	SM	BRN/ TAN	>1000.0					52.0	
		ST	1.0	1.5	5/02	-	MST.	SM	BRN/ TAN							
		ST	1.5	2.0	5/02	-	MST.	SM	BRN/ TAN	>1000.0		<u></u>			>1000.0	
		ST	2.0	2.5	5/02	-	SAT.	SM	BRN/ TAN							
	IW-710-2-1	٧S	2.5	3.0	5/02	-	SAT.	SM	BRN/ TAN	>1000.0					>1000.0	
		vs	3.0	3.5	5/02	-	SAT.	SM	BRN							
		vs	3.5	4.0	5/02	-	SAT.	SM'	BRN	>1000.0					>1000.0	
		٧s	4.0	4.5	5/02	-	SAT.	SM	BRN/ TAN							
		٧s	4.5	5.0	5/02	-	SAT.	SM	BRN/ TAN	740.0					>1000.0	
		v\$	5.0	5.5	5/02	-	SAT.	SM	BRN/ TAN							
		vs	5.5	6.0	5/02	_	SAT.	SM	BRN/ TAN						>1000.0	
		vs	6.0	6.5	5/02	-	SAT.	SM	BRN/ TAN							
		vs	6.5	7.0	5/02	-	SAT.	SM	BRN						>1000.0	
		vs	7.0	8.0	5/02	-	SAT.	SM	BRN/ TAN						>1000.0	
								_								

	PROJE	CT:	BUILDIN SITE IN	G 710 VESTIGAT	ION							BORING	NO.	A·	-7
	LOCAT	ION:	HUNTER	R ARMY /	NRFIELI), SAV	ELEVATION: 19.06								
	WATER	LEV	/EL DUR	RING DRI	LLING:	3.5	4-HOL	JR WATER LEVEL READING: 3.75							
	WEATH	ER:	HAZY &	WARM, 7	5•			DRILLER:	DOUGL	AS LARC	CHE				
	REMARI	<s:< td=""><td></td><td></td><td></td><td></td><td></td><td>GEOLOGIST</td><td>: CHR</td><td>IS LEETI</td><td>1</td><td></td><td></td></s:<>						GEOLOGIST	: CHR	IS LEETI	1				
							5			SAM	IPLES				
	SAMPLE NO.			PTH	-	F001	CONTENT	NO		OVA (ppm)		INU pm)	AT	TOP	OF HOLE
	Ш Ш	~	(F	(FT.)		PER		ΑŢΙ					CGI	GI	OVA /
	J	ODOR			(1991)		띪	FIC		FIELD	FIE	ELD	LEL	0-	HNU
	₹	ō			1 1	WS	jč	SSII	OR	HEADSPACE	HEAD	SPACE		02	
			FROM	ТО	DATE	BLOWS	MOISTURE	CLASSIFICATION	COLOR	ANALYSIS		_YSIS	%	%	(ppm)
L		N	0.0	0.5	5/08	-	MST.	SM	BRN						
		N	0.5	1.0	5/08	-	MST.	SM	BRN	0.0			0.0	20.8	0.0
Γ		N	1.0	1.5	5/08	-	MST.	SM	BRN						
		N	1.5	2.0	5/08	-	MST,	SM	BRN	0.0			0.0	20.9	0.0
Γ		N	2.0	2.5	5/08		V.MST	SM	BRN						
Γ		N	2.5	3.0	5/08	-	V.MST	SM	BRN	0.0		• • • • • • • • • • • • • • • • • • • •	0.0	20.7	0.0
		N	3.0	3.5	5/08	-	SAT.	SM	BRN	· · · · · · · · · · · · · · · · · · ·					
	A-7-1	N	3.5	4.0	5/08	-	SAT.	SM	BRN	0.0			0.0	20.8	0.0
		N	4.0	4.5	5/08	•	SAT.	SM	BRN						
		N	4.5	5.0	5/08		SAT.	SM	LT. BRN	0.2			0.0	20.8	0.0
		N	5.0	5.5	5/08	-	SAT.	SM	LT. BRN		-				
		N	5.5	6.0	5/08	<u>-</u>	SAT.	SM	LT. BRN				-		-
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PROJE	CT:	BUILDIN SITE IN	G 710 VESTIGAT	FION							BORING NO. A-9				
LOCATI	ON:	HUNTER	R ARMY A	AIRFIEL	D, SAV	ELEVATION: 18.08									
WATER	LEV	/EL DUR	RING DRI	ILLING	4. 1	5	2	4-HOL	JR WATER LE	EVEL	. READING: 2.15				
WEATH	ER:	OVERCA	ST & WA	RM, 84	•	DRILLER:	DOUGL	AS LARC	CHE						
REMARK	(S:	CGI NOT	WORKING	;					GEOLOGIST: CHRIS LEETH						
					<u> </u>	늘			SAMPLES						
SAMPLE NO.		DE	PTH		F001	CONTENT	NOI		OVA (ppm)		łNU pm)	AT	TOP	OF HOLE	
ш	2	(FT.)		91	(1991) S PER		ATI					C	GI	OVA /	
MP	ODOR			(19		JRE	FIC		FIELD	FIE	ELD	LEL	02	HNU	
SA	O	Ì			1 97	MOISTURE	CLASSIFICATION	COLOR	HEADSPACE	HEAD	SPACE		2	(ppm)	
		FROM	ТО	DATE	BL (MOM	כר /		ANALYSIS	ANAL	.YSIS	%	%	_	
	N	0.0	0.5	5/07	•	MST	SM	LT. BRN							
	N	0.5	1.0	5/07		MST.	SM	LT. BRN	0.0					0.0	
	N	1.0	1.5	5/07	•	V.MST	SM	SOME ORG.							
	SL	1.5	2.0	5/07	1	V.MST	SM	TAN	0.2					0.0	
	N	2.0	2.5	5/07	-	V.MST	SM	TAN							
A-9-1	N	2.5	3.0	5/07	-	V.MST	SM	GRA/ TAN	8.0	_				0.0	
	Z	3.0	3.5	5/07	-	SAT.	SM	GRA							
	N	3.5	4.0	5/07	-	SAT.	SM	GRA/ TAN	1.0					6.0	
	SL	4.0	4.5	5/07	-	SAT.	МН	BLK							
	SL	4.5	5.0	5/07	-	SAT.	SM	BLK	25.0					90.0	
	SL	5.0	5.5	5/07	-	SAT.	SM	BLK]	
	SL	5.5	6.0	5/07	-	SAT.	SP	WHT						60.0	
		<u> </u>													
		:						;							

) [PROJE	CT:	BUILDIN SITE IN	G 710 VESTIGAT	TION							BORING NO. A-10				
	LOCAT	ION:	HUNTER	R ARMY	AIRFIELI	D, SAV		ELEVATION: 18.66								
	WATER	LEV	ÆL DUR	ING DR	ILLING:	4.	4-HOL	UR WATER LEVEL READING: 4.27								
	WEATH	ER:	CLEAR, V	VINDY &	WARM,	78*	DRILLER: DOUGLAS LAROCHE									
	REMAR	<s:< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td colspan="7">GEOLOGIST: CHRIS LEETH</td></s:<>								GEOLOGIST: CHRIS LEETH						
						<u></u>	<u> </u>			SAM	PLES					
	ġ		DE	PTH		FOOT	CONTENT	NO		OVA (ppm)	1	HNU pm)	AT	TOP	OF HOLE	
	SAMPLE NO.	2	(F	T.)	(16)	PER		:AT						GI	OVA /	
		ODOR		(1991)		JRE	FF		FIELD	FII	ELD	LEL	02	HNU		
		0				BLOWS	MOISTURE	CL ASSIFICATION	o.	HEADSPACE	HEAD	SPACE		-	(ppm)	
ı			FROM	TO	DATE	BL (ΘW	ਹੋ	COLOR	ANALYSIS	ANA	YSIS	%	%		
Ì		N	0.0	0.5	5/08	-	DRY	SM	BRN/ TAN							
ļ		N	0.5	1.0	5/08	-	MST.	SM	BRN	0.0			0.0	20.8	0.0	
Ī		N	1.0	1.5	5/08	-	MST	SM	BRN							
		N	1.5	2.0	5/08	-	MST.	SM	BLK	0.0			0.0	20.5	0.0	
		N	2.0	2.5	5/08	-	V.MST	SM	BLK							
Ī	71117	N	2.5	3.0	5/08	-	V.MST	SM	BLK	0.0			0.0	20.7	0.0	
		N	3.0	3.5	5/08	-	v.mst	SM	BLK	·		- "				
	A-10-1	N	3.5	4.0	5/08	-	SAT.	SM	BLK	0.0		-	0.0	20.7	0.0	
		N	4.0	4.5	5/08	_	SAT.	SM	BLK							
		N	4.5	5.0	5/08		SAT.	SM	BLK	0.0			0.0	20.9	0.0	
		N	5.0	5.5	5/08	-	SAT.	SM	BLK							
		N	5.5	6.0	5/08	-	SAT.	SM	TAN	0.0			0.0	20.8	0.0	
						:					_					
L																
Ĺ				<u></u>												
				-												

	PROJEC	CT:	BUILDING SITE IN	G 710 VESTIGAT	ION							BORING	NO.	A- (MW		
	LOCATI	ON:	HUNTER	ARMY /	NRFIELD), SAV	ANNAH,	GEOR	GIA		ELEVATION: 18.08					
	WATER	LEV	ÆL DUR	ING DRI	LLING:	4.	15	2.	4-HOU	UR WATER LEVEL READING: 2.61						
	WEATH	ER:	OVERCAS	ST & WA	RM, 79'	•	DRILLER: DOUGLAS LAROCHE									
	REMARK	<s:< td=""><td>CGI NOT</td><td>WORKING</td><td>3</td><td></td><td></td><td></td><td></td><td>GEOLOGIST</td><td>CHF</td><td>NS LEETH</td><td>1</td><td></td><td></td></s:<>	CGI NOT	WORKING	3					GEOLOGIST	CHF	NS LEETH	1			
ĺ						,	Ļ			SAM	PLES					
	NO.			PTH		FOOT	CONTENT	NO O		OVA (ppm)	HNU (ppm)		AT TOP OF HOLI			
ĺ	ш	n2	(F	T.)	5	PER	i i	ATI					C	GI	OVA /	
	쥩	ODOR			190	S PER URE C		E		FIELD	FI	ELD	LEL	02	HNU	
	SAMPLE	5			1 3	XS	STC	SS	8	HEADSPACE	HEAL	SPACE		2	(ppm)	
	•	•	FROM	то	DATE	BLOWS	MOISTURE	CLASSIFICATION	COLOR	ANALYSIS	ANA	LYSIS	%	%	ТРРПП	
Ì		N	0.0	0.5	5/07		DRY	SM	BRN					,		
ľ		N	0.5	1.0	5/07	-	MST.	SM	BRN	0.0					0.0	
Ì		N	1.0	1.5	5/07		V.MST	SM	LT. BRN							
Ì		N	1.5	2.0	5/07	-	V.MST	SM	BRN/ TAN	0.0					0.0	
ľ		N	2.0	2.5	5/07	_	V.MST	SM	BRN						-	
	MW-9-1	N	2.5	3.0	5/07		V.MST	SM	BRN	3.0					0.0	
		SL	3.0	3.5	5/07	_	SAT.	мн	BLK			7.77				
ľ	M₩-9-2	ST	3.5	4.0	5/07	-	SAT.	мн	BLK	500.0					680.0	
		SL	4.0	4.5	5/07	-	SAT.	SM	BLK/ TAN							
		SL	4.5	5.0	5/07	-	SAT.	SM	BLK	85.0					350.0	
		SL	5.0	5.5	5/07	-	SAT.	SM	BLK	_					·	
		SŁ	5.5	6.0	5/07	_	SAT.	SM	GRA						420.0	
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HYDRAULIC CONDUCTIVITY DATA REPORT

HYDRAULIC CONDUCTIVITY TESTS
FOR
CAP INVESTIGATION AT BUILDING NO. 710
HUNTER ARMY AIRFIELD, SAVANNAH, GA

7

INTRODUCTION:

Slug tests were conducted September 5, 1991 in seven (7) ground-water monitoring wells adjacent to Buildings 710 and 725, at Hunter Army Airfield, Georgia. These monitoring wells were 2 diameter PVC with screens intercepting the ground-water surface. Slug-in tests were performed, which consisted of lowering a weighted cylinder to the bottom of the well, and measuring time and water level until the water level reached the static level. These data were then used to calculate the hydraulic conductivity of the aquifer.

METHODOLOGY:

The equipment used to perform the slug tests consisted of a slug with nylon cord, water level indicator, ruler and stop watch. The slug was a 1-1/2 diameter PVC pipe with a length of about 2.7. This pipe was filled with silica sand and capped. The water level indicator was a model No. 51453 made by Slope Indicator Company. Before each slug test, the slug and water level indicator were decontaminated using a three phase wash consisting of an Alconox soap wash, tap water rinse and an alcohol rinse. A new nylon cord was used on the slug for each slug test. A static water level reading was made before the start of the slug test. The slug was then lowered to the bottom of the well. Immediately (less than 5 seconds) after inserting the slug, an initial water level reading was made. Water level readings were then made at one minute intervals until the water level has reached the static level. The field data is listed in Appendix 1.

CALCULATIONS:

The computer program SLUGTST was used to calculate the actual K values. SLUGTST is a program, written by Wylie and Wood (1990) in TURBOBASIC, which employs the method developed by Hvorslev (1951) to calculate the hydraulic conductivity. The formula shown in Figure 1 was used by the program for the case of an unconfined aquifer with a well point in uniform soil. The values in the formula are:

kh = horizontal permeability
kv = vertical permeability

d = casing diameter

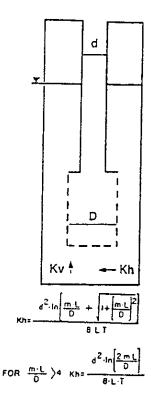
 $m = transformation ratio = \sqrt{Kh/Kv}$

L = intake length

D = intake diameter

T = basic time lag

FIGURE 1



Well point-filter in uniform soil

RESULTS:

The values of hydraulic conductivity (K) varied from 0.0011 ft/min to 0.0031 ft/min (see Table 1). This range is normal for the silty fine sand found at the site.

TABLE 1

WELL #	K (ft/min)	Soil Type
MW-710-1 MW-710-4 MW-710-5 MW-710-6 MW-710-7 MW-710-8 MW-710-11	0.0025 0.0017 0.0031 0.0022 0.0018 0.0014 0.0009	silty sand silty sand silty sand silty sand poorly graded sand clayey sand
MW-/10-11	0.0009	inorganic sılt

REFERENCES:

- Hvorslov, M. J., 1951, Time lag and soil permeability in ground water observations, U.S. Army Corps of Engineers, Waterways Station, Vicksburg, MS, Bul. 36.
- Wylie, A. and Wood, T. R., 1990, A program to calculate hydraulic conductivity using slug test data, Ground Water, Vol. 28, No. 5, pp. 783-786.

APPENDIX 1 FIELD DATA

4

HUNTER AAF, BUILDING 710 HYDRAULIC CONDUCTIVITY TESTS ON MONITORING WELL MW-1 THURSDAY, 5 SEPTEMBER 1991 David C. Leeth

TYPE OF TEST:	Slug-in	ł	TIME	W/L	1
AQUIFER TYPE:	Unconfined	- }	0.0	3.23	į
STATIC W/L (ft):	3.40	t i	1.0	3.33	į
INITIAL W/ (ft):	3.23	;	2.0	3.37	1
SCREEN LENGTH (ft):	3.27	Í	3.0	3.40	i
CASING DIAM. (ft):	0.16699	ł	4.0	3.40	1
SAND PACK DIAM. (ft):	0.64600	ſ	5.0	3.40	į
RATIO OF Kh:Kv:	1:1	1	6.0	3.40	}
DATA SETS:	13	i	7.0	3.40	i
		1	8.0	3.40	;
		1	9.0	3.40	į
		i	10.0	3.40	1
		ł	11.0	3.40	
		1	12.0	3.40	÷

HUNTER AAF, BUILDING 710 HYDRAULIC CONDUCTIVITY TESTS ON MONITORING WELL MW-4 THURSDAY, 5 SEPTEMBER 1991 David C. Leeth

TYPE OF TEST:	Slug-in	1	TIME	W/L	? 3
AQUIFER TYPE:	Unconfined	;	0.0	2.98	1
STATIC W/L (ft):	3.07	ì	1.0	3.05	í
INITIAL W/ (ft):	2.98	1	2.0	3.06	;
SCREEN LENGTH (ft):	8.10	í	3.0	3.07	ť
CASING DIAM. (ft):	0.16699	į	4.0	3.07	ŀ
SAND PACK DIAM. (ft):	0.64600	į	5.0	3.07	i
RATIO OF Kh:Kv:	1:1	ļ	6.0	3.07	ì
DATA SETS:	13	ŧ	7.0	3.07	-
		1	8.0	3.07	i
		1	9.0	3.07	1
		i	10.0	3.07	ŀ
		ļ	11.0	3.07	;
		:	12.0	3.07	į

HUNTER AAF, BUILDING 710 HYDRAULIC CONDUCTIVITY TESTS ON MONITORING WELL MW-5 THURSDAY, 5 SEPTEMBER 1991 David C. Leeth

TYPE OF TEST:	Slug-in	;	TIME	W/L	,
AQUIFER TYPE:	Unconfined	i	0.0	2.58	į
STATIC W/L (ft):	2.86	;	1.0	2.84	í
INITIAL W/ (ft):	2.58	3 3	2.0	2.85	;
SCREEN LENGTH (ft):	6.39	į	3.0	2.85	ì
CASING DIAM. (ft):	0.16699	i	4.0	2.86	i
SAND PACK DIAM. (ft):	0.64600	1	5.0	2.86	1
RATIO OF Kh:Kv:	1:1	;	6.0	2.86	i i
DATA SETS:	16	ł	7.0	2.86	;
		ŀ	8.0	2.86	}
		1	9.0	2.86	i
		i	10.0	2.86	;
		ŀ	11.0	2.86	;
		1	12.0	2.86	1
		1	13.0	2.86	1
		i	14.0	2.86	-
		1	15.0	2.86	į

HUNTER AAF, BUILDING 710 'HYDRAULIC CONDUCTIVITY TESTS ON MONITORING WELL MW-6 THURSDAY. 5 SEPTEMBER 1991
David C. Leeth

TYPE OF TEST:	Slug-in	1	TIME	W/L	1
AQUIFER TYPE:	Unconfined	;	0.0	2.16	;
STATIC W/L (ft):	2.89	į	1.0	2.77	1
INITIAL W/ (ft):	2.16	1	2.0	2.85	1
SCREEN LENGTH (ft):	7.09	į	3.0	2.88	į
CASING DIAM. (ft):	0.16699	i	4.O	2.89	; !
SAND PACK DIAM. (ft):	0.64600	i	5.0	2.89	i
RATIO OF Kh:Kv:	1:1	;	5.0	2.89	ţ
DATA SETS:	16	1	7.0	2.89	i
		1	8.0	2.89	ł
		{	9.0	2.89	i
		;	10.0	2.89	į
		1	11.0	2.89	i
		i	12.0	2.89	ľ
		;	13.0	2.89	į
		1	14.0	2.89	1
		1	15.0	2.89	į

HUNTER AAF, BUILDING 710 HYDRAULIC CONDUCTIVITY TESTS ON MONITORING WELL MW-7 THURSDAY, 5 SEPTEMBER 1991 David C. Leeth

TYPE OF TEST:	Slug-in	i	TIME	W/L	1
AQUIFER TYPE:	Unconfined	i	0.0	2.16	į
STATIC W/L (ft):	2.68	ł	1.O	2.63	-
INITIAL W/ (ft):	2.16	í	2.0	2.64	-
SCREEN LENGTH (ft):	6.57	1	3.0	2.66	i
CASING DIAM. (ft):	0.16699	1	4.0	2.66	1
SAND PACK DIAM. (ft):	0.64600	ł	5.0	2.67	i
RATIO DF Kh:K∨:	1:1	;	6.0	2.67	į
DATA SETS:	21	1	7.0	2.67	1
		ł	8.0	2.67	ļ
		1	9.0	2.67	- }
		ļ	10.0	2.67	i
		i i	11.0	2.67	-
		1	12.0	2.67	1 .
		ŀ	13.0	2.67	ŧ
		1	14.0	2.67	;
		ţ	15.0	2.67	ł
		ŀ	16.0	2.67	;
		ŧ	17.0	2.67	ŧ
		į.	18.0	2.67	1
		i	19.0	2.67	i
		1	20.0	2.67	1

HUNTER AAF, BUILDING 710 HYDRAULIC CONDUCTIVITY TESTS ON MONITORING WELL MW-8 THURSDAY, 5 SEPTEMBER 1991 David C. Leeth

TYPE OF TEST:	Slug-in	i	TIME	W/L	į
AQUIFER TYPE:	Unconfined	į	0.0	1.99	i
STATIC W/L (ft):	2.65	1	1.0	2.54	1
INITIAL W/ (ft):	1.99	ì	2.0	2.61	- {
SCREEN LENGTH (ft):	6.60	;	3.0	2.63	í
CASING DIAM. (ft):	0.16699	i	4.O	2.64	1
SAND PACK DIAM. (ft):	0.64600	ŧ	5.0	2.64	ì
RATIO OF Kh:Kv:	1:1	1	6.0	2.65	;
DATA SETS:	18	1	7.0	2.65	ł
		1	8.0	2.65	1
		í	9.0	2.65	í
		1	10.0	2.65	i
		5	11.0	2.65	;
		ł	12.0	2.65	į
		ŧ	13.0	2.65	į
		1	14.0	2.65	i
		1	15.0	2.65	š
		ł	16.0	2.65	1
		4	17 O	O. 45	:

HUNTER AAF, BUILDING 710 HYDRAULIC CONDUCTIVITY TESTS ON MONITORING WELL MW-11 THURSDAY, 5 SEPTEMBER 1991 David C. Leeth

```
TYPE OF TEST:
                      Slug-in
                                  : TIME
                                           W/L
AQUIFER TYPE:
                      Unconfined !
                                      0.0
                                           1.57
STATIC W/L (ft):
                            2.27
                                      1.0
                                           2.02
INITIAL W/ (ft):
                           1.57
                                      2.0
                                           2.13
SCREEN LENGTH (ft):
                           6.98
                                      J.O
                                           2.17
CASING DIAM. (ft):
                        0.16699
                                           2.20
                                      4.0
SAND PACK DIAM. (ft):
                        0.64600
                                      5.0
                                           2.20
RATIO OF Kh:Kv:
                         1:1
                                           2.21
                                      6.0
DATA SETS:
                           40
                                      7.0
                                           2.21
                                      8.0
                                           2.22
                                      9.0
                                           2.22
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LABORATORY ANALYTICAL REPORTS AND CHAIN OF CUSTODY DOCUMENTATION

5102 LaRoche Avenue (31404) • P.O. Box 13548 • Savannah, GA 31416-0548 • (912) 354-7858 • Fax (912) 352-0165

LOG NO: S1-33097

Received: 01 MAY 91

Ms. Toni Nicholson

U.S. Army Engineer District, Savh

Contract: DACA21-91-MO378

P. O. Box 889

Savannah, Georgia 31402-0889

Project: HAAF BLD 710

REPORT OF RESULTS

LOG NO SAMPLE DESCRIPTION , SOLID OR SEMI	SOLID SAMPLES SAMPLED BY
33097-1 MW-710-1-1 (5/1/91)	Client
PARAMETER	33097-1
Aromatic Volatiles (8020) Benzene, ug/kg dw Ethylbenzene, ug/kg dw Toluene, ug/kg dw Xylenes, ug/kg dw Petroleum Hydrocarbons (418.1), mg/kg dw Lead, mg/kg dw Percent Solids, %	150000 1200000 2200000 4500000 25000 7.9 92

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Contract: DACA21-91-MO378

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Savannah, Georgia 31402-0889

Project: HAAF BLD 710

REPORT OF RESULTS

Page 2

LOG NO	SAMPLE DESCRIPTION , QC REPORT	FOR SOLID	SEMISOLID		SAMPLED BY
33097-2 33097-3 33097-4 33097-5	Method Blank-Soil Accuracy (Mean % Recovery)-Soil Precision (% RPD)-Soil Date Analyzed-Soil	1			Client
PARAMETER		33097-2	33097-3	33097-4	33097-5
Benzene, u Ethylbenze Toluene, u Xylenes, u	ne, ug/kg dw g/kg dw g/kg dw ydrocarbons (418.1), mg/kg dw	<5.0 <5.0 <5.0 <5.0 <10 <0.50	92 % 103 % 98 % 102 %	6.5 % 4.9 % 5.1 % 2.9 %	05.13.91 05.14.91

Methods: EPA SW-846.

Steven J. White

WDS

Steven J. White

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j 5102 LaRoche Avenue (31404) • P.O. Box 13548 • Savannah, GA 31416-0548 • (912) 354-7858 • Fax (912) 352-0165

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Savannah, Georgia 31402-0889

Project: HAAF BLD 710

Purchase Order: DACA21-91-M0378

REPORT OF RESULTS

LOG NO	SAMPLE DESCRIPTION , SOLID OR	SEMISOLID	SAMPLES		SAMPLED BY
33152-1	MW-710-2-1 (5/2/91)				Client
33152-2	MW-710-3-1 (5/2/91)				
33152-3	MW-710-4-1 (5/2/91)				
33152-4	MW-5-1 (5/3/91)				
PARAMETER		33152-1	33152-2	33152-3	33152-4
	Hydrocarbons (418.1), mg/kg dw Volatiles (8020)	1400	14	34	46
Benzene,	• •	<1100	<6.1	200	<6.8
-	zene, ug/kg dw	4900	<6.1	<6.1	<6.8
Toluene,		1600	<6.1	73	<6.8
Xylenes,	ug/kg dw	3000	<6.1	830	<6.8
Percent Sc	olids, %	89	82	82	74

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Purchase Order: DACA21-91-M0378

P. O. Box 889

Savannah, Georgia 31402-0889

Project: HAAF BLD 710

REPORT OF RESULTS

LOG NO SAMPLE DESCRIPTION , QC REPORT	FOR SOLID	SEMISOLID		SAMPLED BY
33152-5 Method Blank-Soil 33152-6 Accuracy (Mean % Recovery)-Soi 33152-7 Precision (% RPD)-Soil 33152-8 Date Analyzed-Soil	1			Client
PARAMETER	33152-5	33152-6	33152-7	33152-8
Petroleum Hydrocarbons (418.1), mg/kg dw Aromatic Volatiles (8020)	<10	96 %	10.4 %	05.21.91
Benzene, ug/kg	<5.0	85 %	2.4 %	05.15.91
Ethylbenzene, ug/kg	<5.0			05.15.91
Toluene, ug/kg	<5.0	100 %	2.0 %	05.15.91
Xylenes, ug/kg	<5.0			05.15.91
Lead, mg/kg dw	<0.50	102 %	2.9 %	06.06.91

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LOG NO: S1-33152

Received: 03 MAY 91

Ms. Toni Nicholson

U.S. Army Engineer District, Savh

Purchase Order: DACA21-91-M0378

P. O. Box 889

Savannah, Georgia 31402-0889

Project: HAAF BLD 710

REPORT OF RESULTS

Page 3

LOG NO	SAMPLE DESCRIPTION , SOLI	D OR SEMISOLID SAMPLES	SAMPLED BY
33152-9 33152-10	MW-710-3-1 (5/2/91) MW-710-4-1 (5/2/91)		Client
PARAMETER		33152-9	33152-10
Lead, mg/kg	dw	3.4	6.7

Methods: EPA SW-846

Steven J. White

DATE/TIME DATE/TIME P REMARKS DATE REPORT REQUESTED Savarnah Division 5102 Lafodhe Averue Savernah (A. 31404 Phone: (912) 354-7850 STANDAND PAGE RUSH RELINOUISHED BY: (SIGNATURE) RELINOUISHED DY: (SIGNATURE) LABONATONY NEMANKS: REQUIRED ANALYSES SAVANNAH LABORATORIES AND ENVIRONMENTAL SERVICES, INC. DATE/TIME DATE/TIME ANALYSIS REQUEST AND CHAIN OF CUSTODY RECORD CUSTODY CUSTODY SEAL NO. SL. LOGNO.
HATACT

YESYNO LABORATORY USE ONLY H dl X318 RECEIVED BY: (SIGNATURE) RECEIVED BY: (SIGNATURE) MONACUEOUS MATRIX XIRTAM SUOBUDA 5675-616 TELEPI IONE 3:401 Sh. 1 12 Uy HAAF ج کر 5/3 Bidd DATE/TIME DATE/TIME SAMPLE ID 1- h - 016 - 01W Mus - 710 . 3-1-2-015-MM PROJECT NAME 8c0 16 CONTY 889 CAJANAAU 1- 7-WM RECEIVED FOR LABOUATIONY BY: (SIGNATURE) TON F. DICHOLSON COE CAJAJAH) TELINOGIISHED BY: (SIGNATURE) P.O. NO. IIME SAMPLING CLIENT NAME DATE (c) JOB NO. ι√ J.

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LOG NO: \$1-33215

Received: 08 MAY 91

Ms. Toni Nicholson

U.S. Army Engineer District, Savh

P. O. Box 889

Savannah, Georgia 31402-0889

Project: BLD 710 PHASE 1

Contract: DACA21-91-M0378

REPORT OF RESULTS

LOG NO	SAMPLE DESCRIPTION	, SOLID OR	SEMISOLID	SAMPLES		SAMPLED BY
33215-1	A-3-1 (5/6/91)					Client
33215-2	A-1-1 (5/6/91)					
33215-3	A-2-1 (5/6/91)					
33215-4	A-4-1 (5/7/91)					
33215-5	A-4-2 (5/7/91)					
ARAMETER				33215-3	33215-4	33215-5
etroleum Hye	drocarbons	24		<12	12	18
Aromatic Vol	atiles (8020)					
Benzene, ug	/kg dw	<6.3	<6.7	<6.0	<5.8	<6.8
Ethylbenzen	e, ug/kg dw	<6.3	<6.7	<6.0	<5.8	<6.8
Toluene, ug	/kg dw	<6.3	<6.7	<6.0	<5.8	<6.8
Xylenes, ug	/kg dw	<6.3	<6.7	<6.0	<5.8	<6.8
Percent Solid	is, %	80	75	83	86	74

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LOG NO: S1-33215

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Project: BLD 710 PHASE 1

Contract: DACA21-91-M0378

REPORT OF RESULTS

LOG NO	SAMPLE DESCRIPTION	, solid or	SEMISOLID	SAMPLES		SAMPLED BY
33215-6 33215-7 33215-8 33215-9 33215-10	A-5-1 (5/7/91) A-9-1 (5/7/91) MW-10-1 (5/7/91) MW-9-1 (5/7/91) MW-9-2 (5/7/91)					Client
ARAMETER		33215-6	33215-7	33215-8	33215-9	33215-10
(418.1), r	ARAMETER atroleum Hydrocarbons (418.1), mg/kg dw cromatic Volatiles (8020)		46	64	26	18
	• •					
Benzene, u		1100	<5.5			<6.8
-	ne, ug/kg dw	<65	<5.5	<7.4	<6.6	
Toluene, u	g/kg dw	410	<5.5	<7.4	<6.6	<6.8
Xylenes, ug	g/kg dw	<65	<5.5	<7.4	<6.6	<6.8
Percent Solids, %		77	81	68	76	74

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Contract: DACA21-91-M0378

Project: BLD 710 PHASE 1

REPORT OF RESULTS

LOG NO	SAMPLE DESCRIPTION , SOLID	OR	SEMISOLID	SAMPLES		SAMPLED BY
	A-10-1 (5/8/91) A-7-1 (5/8/91)					Client
PARAMETER				33215-11	33215-12	
	ydrocarbons (418.1), mg/kg (dw		19	13	
denzene, u	•			<6.0	<6.1	
	ne, ug/kg dw			<6.0	<6.1	
Toluene, u	g/kg dw			<6.0	<6.1	
Xylenes, u	g/kg dw			<6.0	<6.1	
Percent Sol	ids, Z			83	82	

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Savannah, Georgia 31402-0889

Project: BLD 710 PHASE 1

Contract: DACA21-91-MO378

REPORT OF RESULTS

Page 4

LOG NO	SAMPLE DESCRIPTION , QC REPORT	r FOR SOLID	/SEMISOLID		SAMPLED BY
33215-13 33215-14 33215-15 33215-16	Method Blank-Soil Accuracy (Mean % Recovery)-So: Precision (% RPD)-Soil Date Analyzed-Soil	il			Client
PARAMETER		33215-13	33215-14	33215-15	33215-16
troleum H	ydrocarbons (418.1), mg/kg dw latiles (8020)	<10	94 %	7.4 %	05.21.91
Benzene, u		<5.0	90 %	4.4 Z	05.15.91
	ne, ug/kg dw	<5.0			05.15.91
Toluene, u		<5.0	108 %	3.7 %	05.15.91
Xylenes, u		<5.0			05.15.91

Methods: EPA SW-846.

Steven J. White

Sovered Olikkon 5102 Lalloche Averse Sovered CA, 21401 Plere: (913) 254.2050	PAGE OF	STAMOAND	UNSH HSOU	DATE NEPONT		NEHANKS										DATE/TWE	DA1E/IME			
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ORATO	SLO 7 to PLAKE 1	SAJAMNAH	SAVANIAM CA 314/62]		SAMPLE 10	A-10-1 ·	4-7-1	A-4.1	A-4-2	1.6-(1)	MW)-9-7	A-9-1	A-5-1	1-01-	0ΑΙΕ/ΙΜΕ 3/8 (1:37		' Ի	Ship 12:03 (3) 110	
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ERVICES, INC. RECORD	NEOUINED ANALYSES	,									DA1F/Tue RELINOUS		DATE(TIME DELINOUS		
DRIES AND ENVIRONMENTAL SERVICES, INC. EST AND CHAIN OF CUSTODY RECORD		XIZIAM :		AT STS)	/	1				GAV TUNE)		GKATURE)	. <u>.</u> r	357(5)
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	JOB 710. P.O. NO.	CUENTIAME COE (CAS) E CUENTADONESS	CLIENT PROJECT MANAGER	SAMPLING DATE THAE) />			-			BECANGLIST OF SKENNINE	プロの	,		G: Johnson

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5102 LaRoche Avenue (31404) • P.O. Box 13548 • Savannah, GA 31416-0548 • (912) 354-7858 • Fax (912) 352-0165

LOG NO: S1-33340

Received: 16 MAY 91

Ms. Toni Nicholson

U.S. Army Engineer District, Savh

P. O. Box 889

Savannah, Georgia 31402-0889

Contract: DACA21-91-MO424

Requisition: 910111

Project: HAAF-Building 710

REPORT OF RESULTS

LOG NO	SAMPLE DESCRIPTION	, SOLID OR	SEMISOLID	SAMPLES		SAMPLED BY
33340-1 33340-2 33340-3 33340-4	MW-7-1 (5/13/91) MW-7-1-C (5/13/91) MW-8-1 (5/14/91) MW-11-1 (5/15/91)					Client
33340-5	MW-11-2 (5/15/91)					
PARAMETER				33340-3		_
Aromatic Vo	platiles (8020)					
Benzene, u	ıg/kg dw	<6.3	<6.4	41	<6.1	48
Ethylbenze	ne, ug/kg dw	<6.3	<6.4	9.1	<6.1	<6.3
Toluene, u	ıg/kg dw	18	<6.4	160	<6.1	19
Xylenes, u	ıg/kg dw	6.8	<6.4	78	<6.1	660
Petroleum H (418.1),	ydrocarbons mg/kg dw	990	42	310	20	36
Percent Sol	ids, %	80	78	68	82	80

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LOG NO: S1-33340

Received: 16 MAY 91

Ms. Toni Nicholson

U.S. Army Engineer District, Savh

P. O. Box 889

Savannah, Georgia 31402-0889

Contract: DACA21-91-MO424

Requisition: 910111

Project: HAAF-Building 710

REPORT OF RESULTS

LOG NO	SAMPLE DESCRIPTION , SOLID (SAMPLED BY
33340-6 33340-7	MW-6-1 (5/14/91) A-5-1 (5/14/91)				Client
PARAMETER			33340-6	33340-7	
Aromatic Vo	latiles (8020)				
Benzene, u	g/kg dw		<6.0	<6.4	
Ethylbenze	ne, ug/kg dw		<6.0	<6.4	
Toluene, u	g/kg dw		15	<6.4	
Xylenes, u	g/kg dw		11	<6.4	
Petroleum H	ydrocarbons (418.1), mg/kg dw	Į.	21	15	
Lead, mg/kg	dw		4.9	18	
Percent Sol	ids, %		84	78	

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LOG NO: S1-33340

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U.S. Army Engineer District, Savh

P. O. Box 889

Savannah, Georgia 31402-0889

Contract: DACA21-91-MO424

Requisition: 910111

Project: HAAF-Building 710

REPORT OF RESULTS

Page 3

LOG NO SAMPLE DESCRIPTION , QC REPORT	FOR SOLID/	SEMISOLID		SAMPLED BY
33340-8 Method Blank-Soil 33340-9 Accuracy (Mean % Recovery)-Soil 33340-10 Precision (% RPD)-Soil 33340-11 Date Analyzed-Soil	1	-		Client
PARAMETER	33340-8	33340-9	33340-10	33340-11
Aromatic Volatiles (8020) Benzene, ug/kg dw Ethylbenzene, ug/kg dw Toluene, ug/kg dw Xylenes, ug/kg dw Petroleum Hydrocarbons (418.1), mg/kg dw Lead, mg/kg dw	<5.0 <5.0 <5.0 <5.0 <10 <0.50	104 % 110 % 89 % 104 %	6.7 % 15.4 % 3.4 % 6.7 %	05.27.91 05.27.91 05.27.91 05.27.91 05.29.91 05.31.91

Methods: EPA SW-846.

Steven T. Whi

WDS

4-4 - 29 ALW-6-70

SAVANNAH LABORATORIES AND ENVIRONMENTAL SERVICES, INC. SANTAL SERVICES AND ENVIRONMENTAL SERVICES, INC. SANTAL SERVICES AND CHAIN OF CUSTODY RECORD PROPERTY SERVICES (913) 354-7050	uilding 710 neouneo MMLYSES	COE Savannah District 944-5675 E ECLENIADDRESS CLENIADDRESS P.O. Box 889 EN-GGH, 31402 \$ 31402	SONTE MONACUES ACUEOUS ACUEOUS ACUEOUS ACUEOUS ACUEOUS	MW-4-1	Mw-7-1C	MW-6-1	AW-8-1	4-5-1	MW-11-1	MW-11-2		DATE/TIME RECEIVED BY: (SIGNATURE) DATE/TIME RELINQUISHED BY: (SIGNATURE) DATE/TIME	DATE/TIME RECEIVED BY: (SIGNATUTE) DATE/TIME RELINOUTSHED BY: (SIGNATUTE) DATE/TIME	LABOTATONY BY: (SICHATURE) S. DATE/TIME CUSTODY CUSTODY SEAL NO. SL. LOG NO. LABOTATONY REMAIRS:
SAV.	a war	COE Savannah cuent Aboness P.O. Box 889	SAMPLING SAMPLING SAMPLING DATE TIME	MM 16/0/2	11 11	S/H/OI	NW 5	1 4.5-	4 15/pz	יי	de lucheren de constant	Lection of the Comments)	necement pri LADRIMIONY BY: (SIGNATURE)

, 5102 LaRoche Avenue (31404) • P.O. Box 13548 • Savannah, GA 31416-0548 • (912) 354-7858 • Fax (912) 352-0165

LOG NO: S1-33561

Received: 29 MAY 91

Ms. Toni Nicholson

U.S. Army Engineer District, Savh

Contract: DACA21-91-MO378

P. O. Box 889

Savannah, Georgia 31402-0889

Project: HAAF-BLD 710

REPORT OF RESULTS

LOG NO	SAMPLE DESCRIPTION	, LIQUID SA	AMPLES			SAMPLED BY
33561-1 33561-2 33561-3 33561-4 33561-5	MW-3-1 (05.28.91) MW-5-1 (05.28.91) MW-7-1 (05.29.91) MW-7-1C (05.29.91) MW-8-1 (05.29.91)				,	Client
PARAMETER	*	33561-1	33561-2	33561-3	33561-4	33561-5
Purgeable A	Aromatics (EPA 602)					
Benzene, u	ug/l	22	<1.0	<1.0	<1.0	36
Ethylbenze	ene, ug/l	<1.0	<1.0	<1.0	<1.0	<1.0
Toluene, ı	ug/l	<1.0	<1.0	<1.0	<1.0	2.4
Xylenes, u	ug/l	<1.0	<1.0	<1.0	<1.0	<1.0
Petroleum F (418.1),	Hydrocarbons mg/l	<1.0	<1.0	1.9	<1.0	2.9

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LOG NO: S1-33561

Received: 29 MAY 91

Ms. Toni Nicholson

U.S. Army Engineer District, Savh

Box 889

P. O. Box 889

Savannah, Georgia 31402-0889

Project: HAAF-BLD 710

Contract: DACA21-91-MO378

REPORT OF RESULTS

LOG NO	SAMPLE DESCRIPTION ,	LIQUID SAMPLES			SAMPLED BY
33561-6 33561-7	MW-10-1 (05.28.91) MW-11-1 (05.29.91)				Client
PARAMETER			33561-6	33561-7	
	ng/l ne, ug/l ng/l	-	<1.0 <1.0 <1.0 <1.0 <1.0	9.2 17 16 27 <1.0	

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LOG NO: S1-33561

Received: 29 MAY 91

Ms. Toni Nicholson

U.S. Army Engineer District, Savh

P. O. Box 889

Savannah, Georgia 31402-0889

Project: HAAF-BLD 710

Contract: DACA21-91-M0378

REPORT OF RESULTS

			-
LOG NO SAMPLE DESCRIPTION	, LIQUID SAMPLES		SAMPLED BY
33561-8 MW-1-1 (05.29.91) 33561-9 MW-4-1 (05.29.91) 33561-10 MW-6-1 (05.28.91)			Client
PARAMETER	33561-	33561-9	33561-10
Purgeable Aromatics (EPA 602) Benzene, ug/l	5200	600	<1.0
Ethylbenzene, ug/l	3800	26	<1.0
Toluene, ug/l	22000	5.8	<1.0
Xylenes, ug/l	17000	170	1.5
Petroleum Hydrocarbons (418.1),	mg/l 55	<1.0	<1.0
Lead, mg/l	0.038	<0.0050	<0.0050

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LOG NO: S1-33561

Received: 29 MAY 91

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Savannah, Georgia 31402-0889

Contract: DACA21-91-MO378

Project: HAAF-BLD 710

	· RE	PORT OF RESULTS	Page 4
LOG NO	SAMPLE DESCRIPTION , LIQ	QUID SAMPLES	SAMPLED BY
33561-11	Rinsate (05.29.91)		Client
PARAMETER		33561-11	
Petroleum H	ydrocarbons (418.1), mg/l	<1.0	

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LOG NO: S1-33561

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Savannah, Georgia 31402-0889

Contract: DACA21-91-MO378

Project: HAAF-BLD 710

REPORT OF RESULTS

			J -
LOG NO	SAMPLE DESCRIPTION , LIQUID SA	MPLES	SAMPLED BY
33561-12	Trip		Client
PARAMETER		33561-12	
Purgeable A	romatics (EPA 602)		
Benzene, u	g/l	<1.0	
) Ethylbenze		<1.0	•
) Toluene, u		<1.0	
Xylenes, u	g/l	<1.0	



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LOG NO: S1-33561

Received: 29 MAY 91

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P. O. Box 889

Savannah, Georgia 31402-0889

Project: HAAF-BLD 710

Contract: DACA21-91-MO378

REPORT OF RESULTS

Page 6

LOG NO SAMPLE DESCRIPTION , QC REP	PORT FOR LIQUI	D SAMPLES		SAMPLED BY
33561-13 Method Blank-Water 33561-14 Accuracy (Mean % Recovery) - 33561-15 Precision (% RPD) -Water 33561-16 Date Analyzed-Water	Water			Client
PARAMETER	33561-13	33561-14	33561-15	33561-16
Petroleum Hydrocarbons (418.1), mg/l Purgeable Aromatics (EPA 602)	<1.0	110 %	5.5 %	06.07.91
Benzene, ug/l	<1.0	94 %	2.2 %	06.10.91
Ethylbenzene, ug/l	<1.0			06.10.91
Toluene, ug/l	<1.0	92 %	3.7 %	06.10.91
Xylenes, ug/l	<1.0			06.10.91
Lead, mg/l	<0.0050	113 %	7.1 %	06.07.91

Methods: EPA 40 CFR Part 136

Steven J. White

Sword Differ Sigt Liles Avere Sword Or, 21401 Plece: (917) 354-1850	PAGE 06	STAMDAND	Пзи	DATE REPORT REOUESTED	NELLANKS									•	DATE/TIME	SMI/31VO	
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ICES, INC.	NEOUINEO ANALYSES		-	-											DATE/TIME REUNOUSFE	DATE/TIME NEUNOUSIFE	LABONATORY PELLAPIKS;
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SAVANNAH LAB ANALYSIS			P.O 302 889 SAV. GA 31402	en 1040060		MW-1-1	MW-3-	1- h- MW	MW-5-(MW - 6-1	MW-7-	AW-4-	MW-8-	MW-10-(
1 00 00 00 00 00 00 00 00 00 00 00 00 00		COE (XS)	2.0 TO BB3	TONI F. NICHOUSEN	SAMPLETG DATE TIME	1,62/5	1492/5	रिक्षा	5/18/1	1492/5	1911	16/12/3	5/19/71	16/92/5	UNOUSHED BY: (SKOW)		RECEIMED FOR LUBORATIONY BY: (SYCHATUME)

ರ DATE/TIME DATE/TIME NELLANTES DATE NEPONT DEOUES160 Severationships 5107 Lelloche Averae Samay CA. 31101 Place: (917) 354-71150 STANDAND PACE NUSH NELLYNOUSHED BY: (SICHATURE) RELINGUISHED BY: (SIGNATURE) LADONATIONY NEWARKS; REQUINED ANALYSES SAVANNAH LABORATORIES AND ENVIRONMENTAL SERVICES, INC. DATE/TRIE DATE/TIME ANALYSIS REQUEST AND CHAIN OF CUSTODY RECORD 33561 AUSTOOY CUSTOOY SEAL NO. SI LOGINO. LABORATORY USE ONLY H 62 以りての RECEMED BY: (SKGNA TURE) NECEMED BY; (SKICHATURE) NOW YOU WATRIX AGUEOUS MATAX (E) PS 5t75-hh6 TELEPTIONE P.D. BOX 889 SAN. GA 31402 EN-4614 44F- 300, 710 135/4/10:42 RECENÇO FON LABORATORY BY: FSICALATURE) S DATE/TIME DATE/TXE SWAPLEID TRIP BLANK Phoject NAME MW - 14 - 1 RINSA 16 JICHOLSON MAR P.O. NO (SAS) Ŋ IME TONI F. Co E (S CLIENTINAE OATE JOB 210. 62/3 62/5

WATER SYSTEM SURVEY DATA

- G-1 HUNTER ARMY AIRFIELD DATA
 - G-2 USGS WATER WELL SURVEY
 - G-3 CITY OF SAVANNAH DATA

TABLE 1 Information on Water Supply Wells at Hunter Army Airfield, Savannah, Georgia

No.	1	Well: Buildin	g 71	1								
			_									
		Tank capacity										
		Elect. Mtr										1300 GPM Type - Layne Turbine 100 hp
		Drilled										1941
		Depth										550 ft
		Diameter										12 in.
		Cased to										250 ft
		Pump setting										140 ft
		Static level										92 ft
		Dynamic level										
		DAMPHIC LEAGI	• •	•	•	•	•	•	•	•	•	100 10
		•										
No.	2	Well: Building	g 12	05								
		Tank capacity										200,000 gal
												1300 GPM Type - Layne Turbine
		Elect. Mtr										100 hp
		Drilled										1941
		Depth										600 ft
		Diameter										12 in.
		Cased to										250 ft
		Pump setting										140 ft
		Static level										108 ft
		Dynamic level										
		•										
No.	3	Well: Building	g 84	55								
		Tank capacity	. ,									1.000 gal
												30 GPM Type - 'Sta-rite 4'
		• • •					•					Submersible Pump
		Drilled		-								1951
		Depth										360 ft ·
		Diameter										4 in.
		Cased to										40 ft-Casing mdl 20P4E02E 1X76
		Pump										121 ft

Notes:

1. Information was obtained from the HAAF Environmental Office during March of 1991.

TABLE 1 (con't) Information on Water Supply Wells at Hunter Army Airfield, Savannah, Georgia

No. 4 Well: Not in use, information unavailable.

No. 4A Well: Building 8581

Tank capacity		,				1,000 gal '
Pump capacity						80 GPM
Elect. Mtr						5 hp
Depth						
Diameter						4 in.
Cased to				,		92 ft
Mtr Mfr						Holloshaft Mtr

No. 5 Well: Building 8641

Tank capacity	•	٠.	٠		٠		80 gal
Pump capacity							30 GPM TypeKenco Mdl 59A
Drilled							1955
Depth							380 ft
Diameter							4 in.
Cased to							85 ft
Water Level							30 ft

No. 6 Well: Not in use, information unavailable.

No. 7 Well: Building 8703

Tank capacity						5,000 gal
Pump capacity						70 GPM Type - Gould
Drilled						
Depth						450 ft
Cased to					٠	330 ft
Water Level						₹7 f+

Notes:

1. Information was obtained from the HAAF Environmental Office during March of 1991.

The second secon

TABLE 1 (Con't) Information on Water Supply Wells at Hunter Army Airfield, Savannah, Georgia

No. 8 Well: Building 8632

Tank capacity						15,000 gal
Pump capacity						80 GPM Type - Layne Turbine
Elect. Mtr					٠	7.5 hp
Drilled						
Depth						
Diameter		٠				8 in.
						107 ft
Cased to						
						126 ft (Well could be deeper)
Static level						
Pump will prod						

No. 9 Well: Building 8661

Pump	•			., .		Sabre Hall
Storage	capacity					0 gals
Pumping	capacity					1.000 GPM
Depth						Deep well. exact depth unknown
Drilled						'Old', exact age unknown
Emergend	y standby	y				
equipmen	nt instal:	led				100 hp gas driven engine
						stable water source for emergency
fire cor	itrol.					•

Notes:

1. Information was obtained from the HAAF Environmental Office during March of 1991.

G-1 - HUNTER ARMY AIRFIELD DATA

G-2 - USGS WATER WELL SURVEY

GWSI CODES

USE OF WATER :

A, aircond.; B, bottling; C, commercial; D, dewater; E, power; F, fire; H, domestic; I, irrigation; J, industrial (cooling); K, mining; M, medical; N, industrial; P, public supply; Q, aquaculture; H, recreation; S, stock; T, institutional; U, unused; Y, desalination; Z, other.

TOPOGRAPHIC SETTING:

A, aliuvial fan; B, playa; C, stream channel; D, depression; E, dunes; F, flat; G, flood plain; H, hilltop; K, sinkhole; L, lake or swamp; M, mangrove swamp; O, offshore; P, pediment; S, hillside; T, terrace; U, undulating; V, valley flat; W, upland draw.

SOURCE OF DATA:

A, other gov't; D, driller; G, geologist; L, logs; M, memory; O, owner; R, other reported; S, reporting agency; Z, other.

METHOD OF CONSTRUCTION;

A, air-rotary; B, bored or augered; C, cable tooled; D, dug; H, hydraulic rotary; J, jetted; P, air percussion; R, reverse rotary; T, trenching; V, driven; W, drive wash; Z, other.

CASING MATERIAL :

B, brick; C, concrete; D, copper; G galv. Iron; I, wrought Iron; M, other metal; P, pvc or plastic; R, rock or stone; S, steel; T, tile; U, coated steel, W, wood; Z, other material.

TYPE OF FINISH:

C, perous concrete; F, gravel with perf.; G, gravel screen; H, horiz. gallery; O, open hole; P, perf. or slotted; S, screen; T, sand point; W, walled; X, open hole; Z, other.

TYPE OF MATERIAL FOR OPEN SECTIONS:

B, brass; C, concrete; G, galv. iron; I, wrought iron; M, other metal; P, pvc or plastic; R, stainless steel; S, steel; T, tile; Z, other.

TYPE OF LIFT (PUMP TYPE):

A. air; B, bucket; C, centrifugal; J, jet; P, piston; R, rotary: S, submersible; T, turbine; U, unknown; Z, other.

TYPE OF LOGS:

A, time; B, coller; C, calliper; D, driller's; E, electric; F, fluid conduct.; G, geologist; H, magnetic; I, induction; J, gamma ray; K, dip meter; L, lateral log; M, microlog; N, neutron; O, microlateral log; P, photo video; Q, radioactive; S, sonic; T, temperature; U, gamma-gamma; V, fluid velocity; X, core; Z, other.

METHOD OF DISCHARGE MEASUREMENT:

A, accoustic meter; B, baller; C, current meter; D, Doppler meter; E, estimated; F, flume; M, totaling meter; O, orlfice; P, poltot-tube meter; R, reported; T, trajectory; U, venturi meter; V, volumetric measurement; W, weir; Z, other.

METHOD OF WATER LEVEL MEASUREMENT:

A, airline; B, analog; C, calibrated airline; E, estimated; G, pressure gage; H, calibrated pressure gage; L, geophysical logs; M, manometer; N, non-rec. gage; R, reported; S, steel tape; T, electric tape; V, calibrated electric tape; Z, other.

DATE: 08/30/91

320142/0810804 -- Half Hile Radius 10675

PAGE

k	STATION NAME	LATITUDE (DEGREES)	LONGITUDE (DEGREES)	TOP OF CASING (FEET)	DEPTH OF WELL (FEET)	BOTTOM OF CASING (FEET)	DIAMETER OF CASING (IN)	DATE OF CONSTRUCTION	DISCHARGE (GPM)	PRIMARY USE OF WATER
\$	US ARMY, MUNTER OT	320145	0810806	-00	504	259.00	12.00	11-01-40	1300.00	A

DATE: 0	98/30/91		320142/08	10804	3 Hile R	adīus 106	75			PAGE 1
GRID	STATION	LATITUDE	LONGITUDE	TOP OF CASING	DEPTH OF WELL	BOTTOM OF CASING	DIAMETER OF CASING			PRIMARY USE
NUMBER	NAME	(DEGREES)	(DEGREES)	(FEET)	(FEET)	(FEET)	(IN)	DATE OF CONSTRUCTION	DISCHARGE (GPM)	OF WATER
36P036	SAVANNAH, GA 36	315922	0810845	.00	414	252.00	10.00	11-18-60	703.00	Þ
360017	HOWARD JOHNSONS HTL	320314	0810850	.00	448	294.00	4.00	08-05-53		Ċ
360112	SCL RR, SAV SHOPS	320149	0810853	.00	508	275.00	8.00	- 25	450.00	Č
36 912 5	MCCALLAN, MRS.	320309	0810858	-88	341	146.00	4.00	0938	454,00	P
				146-00		249.00	3.00			r
360164	RAHN DAIRY	320150	0811038	.00	375	310,00	4.00	10-14-58	20,00	Ħ
369181	BILTHORE GARDENS HHP	320239	0811048	-00	380	290.00	3.00	01-01-4989	150.00	P
369284	US ARMY, HUNTER D9	320019	0811008	.00	623	270.00	12.00	0459	.50100	F
360285	US ARMY, HUNTER 01	320145	0810806	_00	504	259.00	12.00	11-01-40	1300.00	Ä
360286	US ARHY, HUNTER 02	320115	0810745	.00	555	260,00	16.00	42	1440.00	Ť
34-287	US ARMY, HUNTER 03	320003	0810912	.00	. 370	324.00	4.00	51	30.00	Р
}	US ARMY, HUNTER D4A	320103	0810958	0	360	267	4	06-01-58		H
)	US ARMY, HUNTER 04	320058	0810955	.00	300	90.00	3.00	26		"
. 1	US ARMY, HUNTER 06	320017	0811034		180			**		P
$\lambda = E$	US ARMY, HUNTER OB	320003	0811023		375					p.
360302	SAVANNAH, GA 25	320225	0810854	.00	540	287_00	10_00	73	930.00	_
379006	SAVANNAH, GA 13	315948	0810705	-00	1000	270.00	12.00	04-01-54	730,00	· p
37P078	RIVERS END SUBDIV 01	315929	0810646	.00	440	200.00	4.00	45	55.00	ប្
3 7 P079	RIVERS END SUBDIV 02	315924	0810646	-80	400	227.00	4.00	54	80.00	P
370023	US GEOL SURVEY TW 05 PT 1	320404	0810659	.00	930	870.00	3.00	17		P U
370029	E & U LAUNDRY	320352	0810622	.00	516	199.00	8,00	31	134_00	
370031	SAVANNAH, GA 09	320219	0810614	.00	710	267.00	16.00	05-01-41	3500.00	Ŋ
370033	DERST BAKING CO	320258	0810728	-00	568	258.00	10.00	11-03-47	632,00	P
370034	BENEDICTINE SCHOOL	3200 29	0810522	.00	327	100.00	4.00	09-01-55	034,UQ	N 1-
379035	SAVANNAH, GA 06	320040	0810547	-00	750	240.00	12.00	1050		ប្
370095	PULTURE OF THE TO AN ARE			,			12100	10 20		Þ
379096	CHATHAM CO BD DF ED (9/19	320352	0810729	.00	325	270.00	4.00	09-10-51		U
214030	REYNOLDS-HANLEY L1	320243	0810659	.00	346	68.00	6.00	36	800.00	ŭ
379097	BEVUOLDO ALLEN DE LO	77444		68.00		128.00	4.00		• •	_
370101	REYNOLDS-MANLEY L2 DUNN, T T	320248	0810706	.00	514	258.00	6.00	11-17-53		N
	DUNK, I I	320102	0810521	-00	542	250,00	6.00	04-19-55		H
370175 370180	SAV ELEC & PUR CO OP 2	320317	0810716	8	561	276	6	0657		H
370180 370181	MEMORIAL HEDICAL CTR	320148 330607	0810524	-00	1000	283.00	10-00	0663	500.00	7
21.01.01	US GEOL SURVEY TH 05 PT 2	320404	0810659	-00	830	515.00	10.00	17		Ù
370184	CANDLER HOSPITAL	320146	0010557	-00		180.00	12.00		••	-
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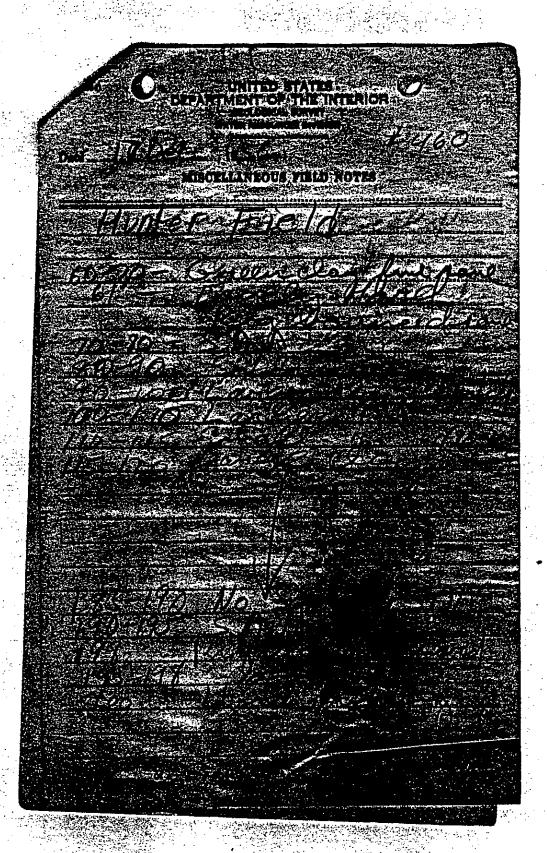
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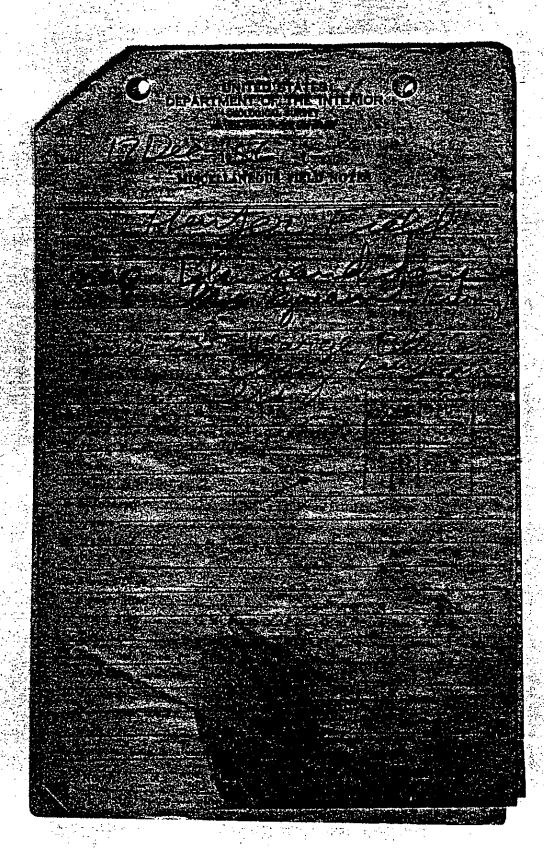
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RECORD BY S. M. Herrick

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UNITED STATES DEPARTMENT OF THE INTERIOR GEOLOGICAL SURVEY WATER RESOURCES DIVISION WELL LOG

No.	GGS 80 (
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		i

OTHER NOS.

State <u>Georg</u>	County Chatham Subarea		· .
Owner City	of Savannah		
Owner Testa			
Location _Abe	ercorn and 59th Street, Savannah, Georgia		
Orilled by L	ayne-Atlantic Co. Address		···
Date <u>May</u>	L9h1 Casing diam. Land-surf. a	it. <u>18 fe</u> r	et
louwon of Anto	Well Cuttings		
ource of asia	(Enter type of well, perforations, yield, and drawdown at end of		 -
	(Enter type of weat, perforations, yield, and arawaown at end of	oy)	
Correlation	MATERIAL	THICKNESS (feet)	DEPTH (feet)
	No samples	30	30
*	Sand, fine- to medium-grained, argillaceous, micaceous	10	40
	Sand, medium-grained, with occasional fragments of macro-shells	?	60
	Sand, coarse-grained, with occasional fragments of macro-shells (80-84)	L	811
	No samples	31	115
	Clay, dark green, silty	30	3 4.5
	No samples	20	165
1.**	Rock, light brown, sandy, dolomitic, impregnated with brown to black, phosphatic pubbles & brown chert	18	1833
	Limestone, light gray, crystalline (re-crystallized) san Clay, dark green, sandy, with brown, phosphatic pebbles	d y <u>17</u> 20	200 220
	Limestone, gray, crystalline (re-crystallized), sandy, with occasional macro-shells & fish teeth	10	230
	limestone, some gray, crystalline (re-crystallized), dan sandy, nodular, with occasional what resched had fish tee	17	250
	shells & fish teeth Limestone, nodular, re-crystallized, fossiliferous	20	270
	No samples	40	310
		٠.	
7	Limestone, cream, re-crystallized, fossiliferous Limestone, dense, gray, re-crystallized, fossiliferous	<u>?</u> 15	310 325
	Limestone, cream, toolight brown, re-crystallized,		330

8. S. SOVERHMENT PRINTING OFFICE . 16-61887-1

UNITED STATES DEPARTMENT OF THE INTERIOR GEOLOGICAL SURVEY WATER RESOURCES DIVISION

OLOGICAL SURVEY 14 1 1 1 1	NoGGS 80
R RESOURCES DIVISION	• .

OTHER NOS. 37Q31

Land-surf. alt. 18 feet

WELL LOG

	-			•	-		
State _	Georgia	. County .	Chatham	Subarea			
	City of Savanna						
Locatio	n Abercorn and 5	9th Stre	et, Savannah,	Georgia			
						:	
Drilled	by Layne-Atlanti	c Co.		Address			

Source of data Well Cutting

(Enter type of well, perforations, yield, and drawdown at end of log)

Casing diam. _

MATERIAL	THICKNESS (feet)	DEPTH (feet)
Limestone, considerable dense, light gray, re-crystal- light, saccharoidal, much calcitized	17	347
Limestone, dense, gray, re-crystallized	. 39	386
No samples	80	п ее
Linestone, light gray, sandy, saccharoidal	20	486
Limestone, light gray, sandy, saccharoidal, with	20	506
The state of the s	·	605
No samples	15	620
sacchatoidal	20	6h0
	20	660
Limestone, light gray to white, re-crystallized, saccharoidal, with appreciable amount of gray	ьо	700
The same of the sa		
Formation: Pliocene - Recent? (155') from 0 to 155 feet		*************
Miocene(107') from 155 to 260(_) feet		
Ocala(375'+) from 325 to 700(+) feet		
Possible Water-Bearing Horizons:		
Somewhat porous limestone from 310 to 700 feet	***************************************	
	Limestone, dense, gray, re-crystallized No samples Limestone, light gray, sandy, saccharoidal Limestone, light gray, sandy, saccharoidal, with abundant Echinoid spines Limestone, somewhat softer, saccharoidal, re-crystalliz No samples Limestone, light gray to white, re-crystallized, saccharoidal Limestone, light gray to white, re-crystallized, saccharoidal Limestone, light gray to white, re-crystallized, saccharoidal, sparsely glauconitic Limestone, light gray to white, re-crystallized, saccharoidal, with appreciable amount of gray Summary: Formation: Pliocene - Recent? (155') from 0 to 155 feet Oligocene(Suwannee;65') from 260 to 325 feet Ocala(375'+) from 325 to 700(+) feet Possible Water-Bearing Horizons:	limestone, dense, gray, re-crystallized No samples Limestone, light gray, sandy, saccharoidal Limestone, light gray, sandy, saccharoidal, with abundant Echinoid spines Limestone, somewhat softer, saccharoidal, re-crystallized No samples Limestone, light gray to white, re-crystallized, saccharoidal Limestone, light gray to white, re-crystallized, saccharoidal, sparsely glauconitic Limestone, light gray to white, re-crystallized, saccharoidal, with appreciable amount of gray Summary: Formation: Pliocene - Recent? (155') from 0 to 155 feet Miccene(107') from 155 to 260(") feet Oligocene(Suwannee;65') from 260 to 325 feet Possible Water-Bearing Horizons:

RECORD BY S. M. Herrick

DATE .

SHEET ...2... of2...

230

SHEET _____ OF __

9=068 (December 1949)

UNITED STATES DEPARTMENT OF THE INTERIOR GEOLOGICAL SURVEY WATER RESOURCES DIVISION

No	GGS	воу	
-		1	
OTHER 1	Nos	89	

WELL LOG

State <u>Geor</u>	gia County Chatham Subarea		
OwnerCity	of Savannah		
Location Aber	rcorn and 59th Streat, Savannah, Georgia		
Drilled by	Layne-Atlantic Co. Address		·
Date <u>May 1</u>	941 Casing diam. 20" 10267 Land-surf. al	. <u>18 fe</u>	et
Source of data	Well Cuttings		
	(Enter type of well, perforations, yield, and drawdown at end of le	og)	,
CORRELATION	MATERIAL	THICKNESS (feet)	DEPTH (feet)
	Sand, fine to medium-grained, with some gray, micaceou silty clay	·, ··	30
	Sand, fine-grained, micaceous, lignitic, finely-phosp-	-	40
	Sand, medium- to coarse-grained, sparsely-phosphatic, with eccasional shell fragments	-	60
A TO STATE OF THE	Sand, midium to coarse-grained, sparsely-phosphatic, with frequent fragments of pale green, sandy, phosphat-	-	80
, mark	io clay		XX
	Sand, coarse-grained, sparsely-phosphatic, with frequent fragments of pale green, sandy, phosphatic clay		82
	Sand, coarse-grained, sparsely-phosphatic, with frequent trapments of light brown, sandy, saccharoidal,	· 	8L
	dělěmitic rock		
	Clay, pale green, sandy, with scattered fragments of white, sandy, phosphatic limestone		115
The state of the s	Clay, pale green, blocky, phosphatic	<u>-</u> .	125
Visit Control	Clay, pale green, blocky, phosphatic, with occasional fragments of white, sandy, phosphatic linestone	-	145
	Rock; light brown; sandy, cherty, phosphatic; dolomitic phosphatic pebbles abundant	18	183
	Rock, light brown, sandy, cherty, phosphatic, dolomitic with frequent fragments of white, re-crystallized, sac-		
m minimum Mini	charoidal, fossiliferous limestone, with macro-shells, bryozoan re-mains and foraminifera (sample probably out-	_	200_
	ef-place)		
	Clay, pale green, sandy, with scattered fragments of white, sandy, phosphatic limestone Limestone, dense, sandy, re-crystallized, saccharoidal,		220

U. S. SOVERREENT PRINTING OFFICE 15-61567-1

phosphatic

11 11 11 11 11

RECORD BY South Herrick

RECORD BY S. M. Herrick

UNITED STATES DEPARTMENT OF THE INTERIOR GEOLOGICAL SURVEY WATER RESOURCES DIVISION

No	GGS	80
•		
	37	

SHEET2... of3...

WELL LOG

State <u>Geo</u>	rgia County Chatham Subarea		
Owner Cit	y_of_Savannah		
			·
Location Abe	rcorn and 59th Street, Savannah, Georgia		
			
Drilled by L	ayne-Atlantic Ce. Address		
Date <u>May</u>	1941 Casing diam. Land-surf. a	lt. <u>18 fe</u> j	
		lv. — <u>1016</u> !	3 L
Source of data	Well Cuttings	·	
	(Enter type of well, perforations, yield, and drawdown at end of	log)	
Correlation	MATERIAL	THICKNESS (feet)	DEPTH (feet)
	Limestone, light gray, sandy, somewhat weathered, with occasional macro-shells and foraginifera	20	270
Section and an artist of the section and an artist of the section and artist of the section artist of the section and artist of the section artist of the section and artist o	highly calcitized, fossiliferous, with foreminifera of	1, 40	310
i et i	Oligocene & Middle Eccene Age, latter re-worked		
	Limestone, dense, light gray, calcitized, fessiliferous	15	
	with frequent Echinoid spines, bryskoss kalmiss; and large foraminifers	42	325
72.	Limestone, rather dense, white to cream, re-crystallized highly calcitized, fessiliferous, with foreminifera of		
	Oligocene & Middle Eocene Age, latter re-worked	3	330
	Limestone, dense, cream, with some light gray, rather		
	unfossiliferous limestons	17	347
·	Limestone, dense, gray, re-crystallized	39	386
	Ne samples	80	166
	Limestone, light gray, sandy, saccharoidal	20	<u>1</u> 86
	Limestone, light gray, sandy, saccharoidal, with abund- ant Echinoid spines	20	506
.e. *	limestone, semewhat softer, saccharoidal, re-crystallize		605
e grande de la companya de la compan	No samples	15	
	Limestone, light gray to white, re-crystallized; saccher	cidal	620
	arolda1	20	640
	dimestone, light gray to white, re-crystallised, saco- haroidal, sparsely glauconitic	20	660
	Limestone, light gray to white, re-crystallized, saccharoidal, with appreciable amount of gray		
	uran shhractants smonut of LLSA	40	700

E. S. SOTERREST PRINTISS OFFICE 10-61567-1

UNITED STATES DEPARTMENT OF THE INTERIOR GEOLOGICAL SURVEY WATER RESOURCES DIVISION

о.	GGS_	.8Q	************

OTHER Nos.

WI	ELL	L()G	· .:

StateGeo:	rgia County Chatham Subarea		
Owner <u>Cit</u> ;	y of Savannah		
•	rcorn and 59th Street, Savannah, Georgia	-	
LAUCAS LIUM	COUL AND 77 M MM SELS DETAINING MEDICAL		
Drilled by L	ayne-Atlantic Co. Address		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
Date		:18 fe	et
	Well Cuttings (Enter type of well, perforations, yield, and drawdown at end of lo	 og)	**
Correlation	MATERIAL	THICKNESS (feet)	DEPTH (feet)
and the second	Summary:		
	Forms Lour		
n emission	Pliscane - Recent? (155!) from O to 155 feet	-,-	***********
	Miocene (107!) from 155 te 260 feet(+)		
	Oligocane (Suwannee; 65!) from 260 to 325 feet		
	Desla (375!+) from 325 to 700 feet(+)		
	Possible Water-Bearing Horizons:		
19 (1984) 19 (1997) 19 (1997)	Semewhat porous limestome from 310 to 700 feet	· .	
V= 3.			.======================================
and the second s			

+ +			P***

RECORD BY S. M. Herrick

DATE ____

SHEET ___3__ or ___3_

OTHER NOS.

19-4908 (Planari bar 1000)

DEPARTMENT OF THE INTERIOR GEOLOGICAL SURVEY

ECLOSICAL SURVEY NO. COS33799

WELL LOG

er Chi	98 Showinh ## (3		
ي وسر درد د سرت درد د			
tion	- 4		F:55555565

ed byU	isome-Attlantate con. Address		
Apptl	11995 Coxing diam. Land-surf. at	t	
	E-19.23 To 19.44		
ce of Cata	Well Dufbillions		
	(Enter type of well, perforations, yield, and drawdown at end of t	0g)	
		*****************	E
MILATION .	MATERIA	THICKNESS (feet)	Deri (feet
<u> </u>			
The state of the s	blueatone, soft, cream, highly fossiliferous, with scat		
- 1941 - 1944 1941 - 1944	Conilie with abundant bryoners remains	BQ	72
	Sand, Cina to madium erained		
enizar (idmenture; soft, cream, highly fossiliferous, with scat-	36	3B
	Sandi Manantis colleges y similar after a granely glav-	1.2	BO
· · ·	wentite with abundant bryoneen remains; with scattered	THE PROPERTY OF	man oo.
-F-W	Chayespalas rolen . micaceous . milty	3/9	. 173
ستنهزيما	GEAPSTORES ENGINE MEDICALITY STATES OF THE S		
وه المنظمة الم	managed the property of the state of the sta		223°
A 100 A	brown, phosphatic pebbles, abundant		
n market see	Limitons, Francer and programmively finer-prairies		890
5	Ministers, mostly dense and to the grapped and graph and molds of shells with scattered fragments of	60	951
	weatheren, Hodesaryneren) iferateveroduler, Yobbistyero	Walter State Control	X21
	and Manapater preservitay (latter probably seathered line	50	250
الله محاول الله الله الله الله الله الله الله ا	81cma		general service.
	The state of the s	स्युक्तिकाः इत्रा व्य ासः विकासम्बद्धाः	********
કર્યું છે. જે કે જે જે જે જે જે જે જે જે જે જે જે જે જે		高度 高度	
	Parestana; cream, soft, fossiliferous	63	313.
* ************************************	Limetton federal, trie) ireservet Eddard franch deldfbise		
	fossit Academical is to homisal feet neden remains, echinoid spines; and foresimilar 273 to 221 foot	60	<u>3.73.</u>
		Survey of the second	
	Line aline podad department for the listed, foodby de loitise	***************	**********
	fossigifer quescui thus hundans between Consens, schinoid	61	434
	spiner detail Elementalistaries top not determined because		222 24.236 2
سري در در ميري در در در در در در در در در در در در در	of long maple interval. 615 - 700') from 700 to	0.0	
	Limestone Commendate than above; with abundant echinoid		
	spines (x-sections)	90	524
the gr		,	_
	Linestone that Foursement shift of destrict for our	91	615
	Limestenes coal program, this processiliferous, with sca-		
	ttered of research to configuration of the redense, sparsely glauco-	2.1.15	700

Georgia

CALBERT NOR

No	GGS 379	
States were	e Marie Committee Contraction of the Contraction of	
OTHER 1	√os	

WELL	ፒሰር
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Chatham

tate Georg	Collins of the Collin	-	
wner City	of Savannah of , 3		
cation	~··		
· F. R. 66 (II) analogo		CONTRACTOR PROPERTY OF THE PRO	

rilled by	Address Address		· · · · · · · · · · · · · · · · · · ·
ate April	1954 Cosing diam. Land-surf, al	·	
CONC. Designation of the second	and the state of the state of the state of the state of the state of the state of the state of the state of the		
out to of the	Well Cuttings (Enter type of well, perforations, yield, and drawdown at end of heart and grawdown at e	og).	
	Tenter time of west perforations, risid, and drawdown at end of		FED TO SE
CORRELATION	MATERIAL	THICKNESS TYPETY SES (1981)	DEPTH (feet)H
	imestone, soft, cream, highly fossiliferous, with scat-	!	**************************************
in the second	vered fragments of pray, rather dense, sparsely glau-	80	780
	confide with abundant bryoncas remains		
	amestons, soit, cream, highly fossiliferous, with scut	35	
and the second s	tared framents of gray, rather dense, sparsely glav- conicie, with abundant brystein remains; with scattered	42	:::: :::::::::::::::::::::::::::::
: To the the	【 自己的主义的 1997年,1997年,1997年,1997年,1997年,1997年,1997年,1997年,1997年,1997年,1997年 ,1997年,	10	790
To the second se	destroy destroy value of the first form of the first of t		820
****	rown, vicephatis rebbles, abundant Limestone, gramular and progressively finer-grained	30	- 44
anaman dan anaman dan dan dan dan dan dan dan dan dan d		70	890
	Linguigns, togicy symmetric or granular many with pact	- 60	950
1846 124	Limestone dense infesti feroug nodillar ffth bounde and light bross there are large probably mestimered limes	17 128, 50	1000(
arinns yr sy skameringydy	上海更多的基本 的问题是这种数据的文化。		بلان ه
	Swamary	************	
	Cormation: cream, acti, fossiliferous	6	313
	Indicterentiated Pitocene Recentation O to:171 fe		
	spines. Lamthorns, Iron, 171 to 221 feet	60	נונ
	Tampa from 221 to 235 feet(+)		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
	Limolingong (Spennes) from 215 to 113 feet (+) alcitime	6	tst.
t e ele	of long sample interval, 615 - 7001) from 700 t		
	Limeston Ofer the then above; with abundant echinoi		· • • • • • • • • • • • • • • • • • • •
	spines (x-ections)		521
	Limes Possible Water-Bearing Horizons: Ferons	21	615
	Limestone from 250 to 1000 feet; the second to 1000 feet;		
	nitic. With aburdant bryozoga remains		
CORD BY SH	No. Harrick: DATE	SHEET 2	. 0F2

G-3 CITY OF SAVANNAH DATA

WELL LOCATION WELL # WALZ DRIVE NEXT TO JULIETT LOWE SCHOOL X - USGS has listed as within 3-miles #1 of site. Checked in the field. STILES AVENUE BEHIND CITY LOT X Site is more than 3 miles away. #2 IN CITY LOT YARD X #3 BWINNETT STREET AT WEST BOUNDARY AND I-16 X #4 IN CORNER OF WHITAKER STREET AND FARK AVENUE X#5 FORSYTH PARK CORNELL AVENUE BETWEEN WATERS AVENUE AND #6 B. C. SCHOOL CORNER OF VICTORY DRIVE AND WATERS AVENUE X#7 DAFFIN PARK EDGEWOOD RD. AND PIERPONT AVENUE X #8 GIRL SCOUT PARK - GORDONSTON COLUMBUS DRIVE AND ABERCORN STREET #9 AUGUSTA AVENUE AT EAST LATHROF AVENUE X #1Q PENNSYLVANIA AVENUE AT HARRISON STREET X #11 BEHIND FIRE STATION 35TH STREET AND LINCOLN STREET L #12 MONTGOMERY CROSSROADS AT BARTLETT SCHOOL #13 WINDSOR FOREST ON BRIARCLIFF CIRCLE X #14 OFF WINDSOR ROAD WILSHIRE ESTATES ON LARGO DRIVE NEAR V USGS has listed of City of Savannah 415 TIBET AVENUE SOUTHEASTERN SHIPYARD X #16 TRAVIS FIELD ACROSS FROM AIRPORT TERMINAL X #17 TRAVIS FIELD NEXT TO QUALITY COURTS MOTELX #18 TRAVIS FIELD AT EDGE OF RUNWAY BEHIND HANGER X #19 BUILDING AT END OF SAPELO ROAD - ISLANDWOOD X #20 WILMINGTON ISLAND WELLINGTON CIRCLE OFF MILLWARD ROAD - X #21

WILMINGTON

				\sim
#22	WILMINGTON	IBLAND	RDAD	X

- #23 OFF LARGO DRIVE JUST BEFORE BERKSHIRE WEST X AT WATER STORAGE TANK
- #24 OFF LEANING DAKE DRIVE WOODRIDGE ESTATES X
- #25 BAMBLE ROAD BETWEEN ACL BLVD AND HIGHWAY 17
- #26 COFFEE BLUFF AT COFFEE BLUFF ESTATES X
- #27 BY ST. JOSEPH'S HOSPITAL ON MCAULEY DRIVE X
- #28 BRYAN WOODS ROAD WILMINGTON ISLAND X
- #29 GEORGETOWN BARKSDALE DRIVE & RED FOX DRIVE X
- #30 8-2 GEORGETOWN KING GEORGE BLVD X
- #31 CHATHAM PARKWAY BESIDE SAV GAS OFFICE X
- #32 JOHNNY MERCER BLVD & HIGHWAY 80 WHITEMARSH X
- #33 DUTCH ISLAND HERB RIVER DRIVE -X
 BETWEEN 401 AND 405
- #34 · DUTCH ISLAND KOLB DRIVE BET 840 AND 841 imes
- #35 I-95 & 204 BEHIND CHEVRON STATION X
- #36 I-95 & 204 ROAD BET. DAYS INN MOTEL AND χ
- #37 I-16 & DEAN FOREST ROAD ADJ. TO X
- #38 DUTCH ISLAND DUTCH ISLAND DRIVE BETWEEN X VERDELL DRIVE AND TERRAPIN

) WEIJ.	NO.	BORE DEPTH	PUMP SET	CASING LENGTH	CASING SET	DATE DRILLED	GPM	FREQUENCY OF USE
WELL		1000'	175'	3001	20"	1954	1200	24 HR/DAY
WELL	#6	750'	180'	2401	12"	1949	1400	24 HR/DAY
WELL	<i>#</i> 7	5251	2001	200 *	24"	1921	3000	18 HR/DAY
WELL	#9	7101	2201	2671	20"	1941	1600	24 HR/DAY
WELL	#12	550	2001	2651	14"	1920	1500	12 HR/DAY
WELL	#13	1000,	2101	270'	12"	1956	1300	24 HR/DAY
WELL	#14	800'	140'	3381	12"	1956	700	24 HR/DAY
WELL	#15	414'	130'	252'	10"	1960	1000	24 HR/DAY
WEJ.J.	#23	639'	100'	320'	16"	1970	1100	20 HR/DAY
WE].L	#25	540'	2001	2871	10"	1973	1100	24 HR/DAY
WELL	#27	550'	120	321 *	16 ^{tt}	1981	1470	24 HR/DAY
WELL	#36							