### CLOSURE PLAN FOR HUNTER ARMY AIRFIELD FIRE TRAINING AREA (AAFTA) FORT STEWART, GEORGIA

Prepared for:

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**DOCUMENT 2** 

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# LIST OF ACRONYMS

AAFTA	Army Airfield Fire Training Area
ASTM	American Society for Testing and Materials
CDAP	Chemical Data Acquisition Plan
cm/sec	centimeters per second
CME	Central Mine Equipment
COC	contaminant of concern
0	degree
°C	degrees Celsius
°F	degrees Fahrenheit
DI	deionized
DNR	Department of Natural Resources
DOT	U.S. Department of Transportation
EMC	EMC Engineering Services, Inc.
EPA	U.S. Environmental Protection Agency
ESE	Environmental Science & Engineering, Inc.
FCT	final cleanup target
FID	flame ionization detector
ft	feet
ft <sup>2</sup>	square foot
ft-bls	feet below land surface
ft/day	feet per day
ft/ft	feet per foot
ft/yr	feet per year
gal	gallon
GDNR	Georgia Department of Natural Resources
gpd	gallons per day
ID	inside diameter
MCL	maximum contaminant level

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# LIST OF ACRONYMS

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mgd	million gallons per day
mg/kg	milligrams per kilogram
Ml	milliliter
MRD	Missouri River District
NGVD	National Geodetic Vertical Datum
PAH	polynuclear aromatic hydrocarbon
PID	photoionization detector
ppm	parts per million
PVC	polyvinyl chloride
QA	quality assurance
QC	quality control
RCRA	Resource Conservation and Recovery Act
SC	clayey sand
SM	silty sand
SOC	scope of work
SOW	scope of work
SP	poorly graded sand
SSHP	site safety and health plan
TOV	total organic vapors
µg/kg	microgram per kilogram
$\mu$ g/L	micrograms per liter
U.S. 82	U.S. Highway 82
USACE	U.S. Army Corps of Engineers
USAEHA	U.S. Army Environmental Hygiene Agency
USAF	U.S. Air Force
USCS	Unified Soil Classification System

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# LIST OF ACRONYMS

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VOA	volatile organic analyte
VOC	volatile organic compound
WP	work plan
yd <sup>3</sup>	cubic yards

### **1.0 SITE DESCRIPTION**

### 1.1 SITE LOCATION AND LOCAL CONDITIONS

Hunter Army Airfield is located on 5,400 acres of land in Chatham County, Georgia, just southwest of Savannah (Figures 1-1 and 1-2). The airfield is bounded on the north by lightly populated areas, on the east and south by residential and light commercial areas, and on the west by the Little Ogeechee River. The Hunter Army Airfield Fire Training Area (AAFTA) is located on the northwest portion of the airfield, approximately 800 feet (ft) north-northwest of the control tower and 2200 feet north of the center of the airfield's east-west runway (Figure 1-3). A topographic survey of the site is also provided as Appendix A.

Fort Stewart and Hunter Army Airfield are located within the Southern Atlantic Coastal Plain Physiographic Province. Most of the land within Fort Stewart is flat, planted pine woods interfingered with freshwater swamps and tidal creeks with elevations ranging from approximately 10 to 100 feet above mean sea level (ft-msl). However, the northwestern portion of the reservation is characterized by rolling hills that rise to a maximum elevation of approximately 180 ft-msl.

The ground surface at the Hunter AAFTA, at an elevation of approximately 30 ft, slopes gently to the west and drains toward a small canal. The canal runs west approximately 400 ft then southeast approximately 1,500 ft, where it empties into the Little Ogeechee River tidal floodplain.

#### 1.2 SITE FEATURES AND USAGE

The Hunter AAFTA consists of a grassy cleared area measuring approximately 400 feet by 200 feet, bounded on the north and south by drainage ditches, by the airfield pavement on the east, and by trees on the west. The training area features a 6,400-ft<sup>2</sup> bermed, soil-covered concrete pad (hereafter referred to as "the pad" or "the fire training pad") with a simulated aircraft constructed from a used steel storage tank.

1-1

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The AAFTA was used from the time of its construction until burning was halted in approximately 1990 for training of the airfield's firefighters in extinguishing live fires. Fuel for training fires was provided by underground piping from an above-ground fuel storage tank located approximately 100 feet north of the training pad. Fuels were mostly watercontaminated jet fuel (JP-4) and diesel fuel; however, waste oils and solvents have reportedly also been used (USAEHA, 1987). During training exercises, jet fuel (JP-4) was pumped onto the surfaces of the simulated aircraft and ignited. Firefighting trainees then extinguished the fire with water or foam. The water was contained by the concrete berms around the fire training pad and sump. Some of the water (and fuel) occasionally ran over the concrete berms onto the adjacent soil, and some may have been splashed over the berms by the spray from the firefighting hoses.

### 1.3 SHALLOW SITE GEOLOGY

The coastal plain region of Georgia is underlain by a thick wedge of unconsolidated and semiconsolidated sediments that range in age from Recent to Cretaceous (Herrick and Vorhis, 1963). This sedimentary wedge thickens and slopes toward the east with a dip of less than 1 degree (°). Underlying these sediments in the Savannah area is a basement of crystalline igneous rocks of the Piedmont Formation, and various metamorphic and consolidated sedimentary rocks of Triassic to Precambrian age.

From youngest to oldest, the Recent and Pleistocene deposits consist of discontinuous units of sand, silt, and clay. These units are undifferentiated in the site region, with thicknesses of approximately 60 feet. Underlying the Pleistocene deposits is the Duplin Marl (Upper Miocene), consisting of green, stiff, phosphatic and calcareous sandy clay. The Duplin Marl is approximately 60 feet thick at the site region. The Hawthorn Formation (Middle Miocene) consists of green to buff phosphatic sandy clay and dolomitic limestone. The Hawthorn Formation is approximately 50 feet thick in the site region. The Tampa Limestone equivalent underlies the Hawthorn Formation and is of Lower Miocene age. The Tampa Limestone is approximately 10 feet thick and is dolomitic with seams of green sandy clay at its base. Underlying the Tampa Limestone is a thick sequence of limestone units (the Floridan Aquifer) which include an undifferentiated Oligocene unit, the Ocala Limestone, the gosport sand, and the lisbon formation. These units extend to approximately 850 feet below the ground surface in the vicinity of the site. Figure 1-4 is a composite geologic column for the Savannah area.

Deep borings performed during previous investigations [ESE, 1982; U.S. Army Environmental Hygiene Agency (USAEHA), 1987, Hunter/ESE 1990, ESE 1993a] at or in the vicinity of Hunter AAFTA indicate that the site is underlain predominantly by sand, siltysand, and some clayey sand deposits to a depth of at least 50 feet below land surface (ft-bls). Shallow borings performed during previous investigations (USAEHA, 1987; ESE, 1990; ESE 1993a) at the Hunter AAFTA indicate that the site is underlain predominantly by fine-grained sand deposits to a depth of at least 10 ft.

### 1.4 HYDROGEOLOGY

The two principal aquifer systems in the Georgia coastal plain are the artesian Floridan aquifer and the overlying (younger) surficial aquifer (water-table aquifer). The Floridan aquifer is comprised of Middle-Upper Eocene (Ocala Group) and Oligocene (undifferentiated) limestones. The overlying Lower-Miocene Tampa Limestone, which may include beds of sandy clay, may also form part of the Floridan aquifer. In the Savannah area, the top of the Floridan aquifer is approximately 150 to 20 ft-bls.

The Floridan aquifer is the major source of groundwater for the Coastal Plain of Georgia and adjoining states (Krause and Gregg, 1972). The Floridan aquifer in Georgia provides the majority of water for industrial and domestic use [500 million gallons per day (mgd) statewide in 1978].

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					co	MPOSITE GEOLOGIC COLUMN		
	+ 15 -	Elevat	Sys	em Series	Geologic Unit	Lithologic Description		
	+ 15 -			2	Spoil	Sand, silt, clay, mixed, brown	1	
	MSL –		QUATERNARY	Recent	Alluvium	Clay, soft, wet, highly organic, dark brown		
			σn	Pleistocene	Undifferen- tiated Sands	Sand, medium grained, fossiliferous		
	- 50 -			Upper Miocene	Duplin Marl	Clay, sandy, stiff, phosphatic, green, occasionally calcareous		
4 1				Middle Miocene	Hawthorn Formation	Clay and dolomitic limestone interbedded, phosphatic, sandy, green to buff		
				Lower Miocene	Tampa Lime- stone Equiv.	Limestone, dolomitic with seams of green sandy clay, conglomeritic at base		
SL)	-200 -		TERTIARY	Oligocene	Undifferen tiated Rocks	Limestone, soft, fossiliferous, gray to buff		
FEET (MSL	- 300 - - 400 -		TEI	Upper Eocene	Ocala Limestone	Limestone, soft to dense, granular fossiliferous, white to buff with lenses of bluish re-crystallized limestone glauconitic at base	5 	
i A	- 500 -		2	Middle Eocene	Gosport Sand	Limestone, sandy, fossiliferous, dense, white to gray		
	- 600 - - 700 - - 800 -				Lisbon Formation	Limestone, soft, glauconitic, dolomitic, marly, white to buff	-	
	- 900 -			ar Z	Pre-Lisbon Rocks			
		AY	日心	LIMES				
Figure 1-4 COMPOSITE	Figure 1-4 COMPOSITE GEOLOGIC COLUMN							
SOURCE: HERRICK		5, 1963				A DLCOOP Company		
		-		-				

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The Middle and Upper-Miocene Hawthorn Group and Duplin Marl, comprised of clay with occasional limestone beds, forms a confining unit that hydraulically separates the Floridan aquifer from the overlying surficial aquifer.

The Pleistocene to Recent deposits above the Miocene deposits consist of discontinuous units of sand, silt, and clay. The surficial aquifer is comprised of discontinuous beds and lenses of sand within these deposits. The depth to the water table in the Savannah area is approximately 3 to 10 ft-bls. The vertical extent of the surficial aquifer is not known, though Kundell (1978) reports that the aquifer may be up to 120-ft thick in the study area. Approximately 5-feet of soil fill was brought to the Hunter Army Airfield to raise the airfield and fire training pad above the level of the swamp which existed in the area prior to the construction of the Airfield.

There is no record of extended usage of the surficial aquifer in the study area; however, statewide usage amounted to 500,000 gallons per day (gpd) in 1978.

### 2.0 REGULATORY FRAMEWORK

The Hunter Army Airfield Fire Training Area (AAFTA) was identified as a potential contamination site during a 1982 ESE investigation related to the Resource Conservation and Recovery Act (RCRA) closure of three landfills at Fort Stewart. Follow-up investigations by USAEHA in 1987 and ESE in 1990 and 1992 found toxic metals contamination in the surface soils immediately adjacent to the fire training pad, carcinogenic semi-volatile organics in nearly all surface soil samples (0-1 foot bgs), and petroleum fuel related organics in deeper soils (3-6 feet bgs) on the north and south sides of the pad. These investigations found no evidence that site soils exhibited any hazardous characteristics, with the probable exception of toxic metal-contaminated soils on and immediately adjacent to the fire training pad. Although the fire training area was not a hazardous waste management facility, hazardous constituents (40CFR261, Appendix VIII) have been released to the environment (see Section 3.0), requiring corrective action for a "continuing release" under Section 3004(u) of RCRA. This closure plan is being developed in response to this requirement.

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#### **3.0 SITE CONTAMINATION**

The nature and extent of contamination in the site soils, groundwater, and surface sediments has been investigated in three separate sampling events in 1987, 1990, and 1992. The analytical results of these investigations are provided in Appendix E and a complete description of the efforts (USAEHA, 1987; ESE, 1990; and ESE 1992) can be found in the Significance of Contamination Report (SCR), Hunter Army Airfield Fire Training Area (ESE, June, 1993). Contamination, for the purposes of this closure plan, is defined as the presence of pollutants in concentrations greater than or equal to the preliminary cleanup target (PCT) concentrations developed in Section 4 of the SCR. Contamination was found to be present in three media, soils, ditch sediments, and groundwater.

### 3.1 SOIL CONTAMINATION

Available data on contamination in soils was collected in three efforts spanning 5 years. Soil sampling locations are shown in Figure 3-1 and results of analysis are shown in Table 3.1. The BH-series soil borings were completed by USAEHA in 1987, the HSB-series borings by ESE in 1990, and the PSB series by ESE in 1992. The BH-series samples were taken immediately adjacent to the fire training pad and did not indicate any significant organic contamination, but did detect elevated levels of lead. The 1990 HSB samples were concentrated mainly on the south side of the training pad because of visual evidence that water from the pad overflowed in that direction. Only one boring, HSB-2, was placed to the north of the fire training pad and samples from it were found to be highly contaminated with PAHs. The 1992 PSB series of borings were mainly grouped to the north of the pad to delineate the contamination previously detected in HSB-2. In addition to the soil sampling performed in these three investigations, an underground electrical line was being installed between the fire training pad and the access road during the 1992 field investigation. Cursory examination of the excavated soils revealed a black, oily appearance and a strong petroleum odor, resembling the JP-5 aviation fuel used in the training exercises.

3-1



### Table 3.1 Comparison of Soil Concentrations Detected at Hunter AAFTA to PCTs

	РСТ	-	Regional Background	0		л ца	1000 007 044				<b>.</b>				r	-	internet of another							59.1
Chemical	Systemic	Carc	SE Georgia	@PSB-1	· PSB-2	PSB-3	1992 SOIL SAN PSB-4	PSB-5	DED (	DPD 7	Don 1		DIMENT				1990 SOIL :	SAMPLES	r			1987 SOIL	SAMPLES	
INORGANICS	-			-100-1	130-2	135-3	F3B-4	F3B-3	PSB-6	PSB-7	PSS-1	PSS-2	PSS-3	PSS-4	HSB-1	HSB-2	HSB-3	HSB-4	HSB-5	HSB-6	BH-10	BH-11	BS-12	BS-13
Arsenic	80,000	400	<100-6,500	1,020.00	2,440.00	510.00	590.00	610.00	930.00	1,610.00	490,00	370.00	⊲310.00	1,050.00	<480.00			(60.00)				1,390.00	( 000 00	11 000 00
Baium	4,000,000	NA	10,000- 200,000	12,800.00	23,400.00	18,300.00	17,700.00	19, 100.00	23,700.00	47,600.00	15,600.00	9,950.00	7,970.00	12,000.00	3,830.00	<520.00 5,970.00	<\$40.00 6,210.00	650.00 4,440.00	850.00 15,400.00	<550.00 11,200.00	5,990.00 64,400.00	33,500.00	4,000.00	11,980.00 27.100.00
Cadmium	80,000	NΛ	NA	<570.00	<550.00	<510.00	<540.00	<550.00	<540.00	<540.00	≪520.00	<620.00	≪620.00	≪630.00	<370.00						1 050 00	1,990.00	-1 080 00	2 979 00
Chromium, total**	400,000	NA	1,000- 20,000	5,610.00	5,880.00	3,550.00	3,020.00	3,980.00	4,970.00	6,100.00	5,660.00	2,860.00	1,090.00	3,540.00	780.00	<400.00 3,490.00	<420.00 3,850.00	<410.00 5,870.00	<450.00 1,930.00	<420.00 2,390.00	<1,980.00 12,800.00	4,160.00	<1,980.00	3,870.00
Lead	500,000	NA	<10,000	28,000.00	17,300.00	7,390.00	<7,270.00	<7,310.00	23,900.00	107,000.00	29,400.00	22,900.00	<8,360.00	<8,460.00	<5,260.00	<5,710.00	ح,970.00	<5,810.00	7,400.00	⊲.970.00	645,000.00	1,163,700.00	102,000.00	1,185,000.00
Магалу	24,000	NA	3-10	<100.00	<100.00	<900.00	<100.00	<100.00	<100.00	<90.00	<110.00	<120.00	<110.00	<110.00	<100.00	<110.00	<110.00	<110.00	<120.00	<120.00	400.00	380.00	400.00	790.00
Selenium	400,000	NA	100-500	<290.00	<290.00	<280.00	<280.00	<280.00	<280.00	<280.00	<130,00	<330.00	<320.00	<340.00	<420.00	<450.00	<470.00	<460.00	670.00	<470.00	<200.00	<200.00	790.00	330.00
				·																				
PAHs and a second second																								
Acenzphthene	4,800,000	NA	NA	<850.00	<84.00	<380.00	<81.00	<82.00	<3,900.00	<80.00 -	<190.00	<960.00	<94.00	11 <mark>0.0</mark> 0	<130.00	300.00	<150,00	<150.00	<160.00	<150.00	-	-	-	
Acenaphthylene	2,400,000	NA	NA	<1,800.00	<180.00	<810.00	<170.00	<82.00	390.00	210.00	<190.00	<960.00	<94.00	< <mark>%.00</mark>	<96.00	400.00	<110.00	<110.00	<120.00	<110.00	-	-	_	-
Anthracene	24,000,000	NA	NA	<850.00	<84.00	670.00	<81.00	<\$2.00	440.00	210.00	210,00	2,400.00	<94.00	13 <mark>0.0</mark> 0	<25.00	1,300.00	<85.00	₹83.00	<91.00	<85.00		-	_	_
Benz(a)anthracene	ND	1,200	NA	370.00	170.00	5,300.00	160.00	<120.00	370.00	970.00	760.00	13,000.00	160.00	510.00	≪62.00	4,900.00	<70.00	<68.00	<75.00	<20.00	-	-	-	
Benzo(a)pyrene	ND	120	NA	320.00	220.00	4,800.00	180.00	<160.00	690.00	1,300.00	Į:50.00	12,000.00	<190.00	4 <mark>00.0</mark> 0	<180.00	3,400.00	<210.00	<200.00	<220.00	<210.00		·	-	_
Benzo(b)fluoranthene	ND	1,200	NA	560.00	370.00	6,900.00	· 260.00	<120.00	830,00	2,000.00	760.00	13,000.00	<130.00	4 <mark>50.0</mark> 0	<130.00	5,000.00	<150.00	<150.00	<160.00	<150.00	-	-		-
Benzo(ghi)perylene	2,400,000	NA	NA	<1,900.00	<190.00	<870.00	<190.00	<190.00	<9,000.00	<180.00	<440.00	5,100.00	<210.00	<2 <mark>20.0</mark> 0	<74.00	2,200.00	<84.00	<81.00	<89.00	<84.00	-	-	-	-
Benzo(k)fluoranthene	ND	1,200	NA	250.00	150.00	2,700.00	<120.00	<120.00	240.00	620.00	\$90.00	7,200.00	280.00	3 <mark>90.0</mark> 0	<170.00	2,500.00	<190.00	<180.00	<200.00	<190.00	-	-	-	_
Chrysene	ND	12,000	NA	560.00	200.00	5,300.00	170.00	<120.00	220.00	1,000.00	\$30.00	· 7,600.00	180.00	670.00	<97.00	5,100.00	<110.00	<110.00	<120.00	<110.00			• =	_
Dibenz(ah)anthracens	ND	120	NA	<1,900.00	<190.00	<870.00	<190.00	<190.00	<9,000.00	<180.00	<440.00	<2,200.00	⊲210.00	<22 <mark>0.0</mark> 0	<63.00	1,100.00	<72.00	<70.00	<77.00	<72.00	-	-	-	-
Fluoranthene	3,200,000	NA	NA	690.00	120.00	8,100.00	170.00	77.00	360.00	980.00	2,200.00	34,000.00	190.00	1,20 <mark>0.0</mark> 0	<110.00	13,000.00	140.00	<130.00	360.00	<130.00	-		-	
Fluorene	3,200,000	NA	NA	<850.00	<84,00	<380.00	<81.00	<82.00	<3,900.00	<80.00	<190.00	1,200.00	<94.00	130.00	<110.00	720.00	<120.00	<120.00	<130.00	<120.00	400.00	. <1.0	200.00	<3,0
Indeno(1,2,3-cd)pyrene	ND	1,200	NA	<1,900.00	<190.00	<870.00	<190.00	<190.00	570.00	<180.00	-440.00	7,600.00	<210.00	<22 <mark>0.0</mark> 0	<95.00	2,900.00	<110.00	<110.00	<120.00	<110.00		-		-
Naphthalene Phenanthrene	320,000	NA	NA	3,500.00	<84.00	<380.00	, <81.00 ,	<82.00	41,000.00	<80.00	<190.00	<960.00	<94.00	< <mark>96.0</mark> 0	<210.00	<230.00	5,700.00	<230.00	11,000.00	<240.00	10.00	. 7.00	5.80	<1.00
Pyrene -	2,400,000	NA NA	NA	<850.00	<84.00	670.00	<81.00	<82.00	170.00	100.00	810.00	19,000.00 .	<94.00	1,4 <mark>00.0</mark> 0	⊲67.00	8,100.00	150,00	<74.00	290.00	<76.00	0.90	· <1.00	0.20	<3.00
Тугеле	2,400,000	NA	NA	<850.00	190.00	5,200.00	140.00	<82.00	230.00	810.00	1,400.00	21,000.00	220.00	99 <mark>0.00</mark>	<72.00	9,400.00	140.00	<79.00	340.00	<81.00		-	1 <u>11</u>	-
voci																								
Benzene	1,600,000	24,000	NA	<30.00	~~~			£ 10				1				•								
Ethylbenzene	8,000,000	24,000 ND	NA	36.00	<.00	<del>ර</del> .70	<5.80	< <u>5.80</u>	39.00	⊲.70	-s6,80	<6.90	<6.70	<6.80	<1.20	<1,3	<170.00	<1.3	<1,800.00	<1.3	-	-	-	
Methylens chloride	4,800,000	93,000	NA	<60.00	< <u>&lt;6.00</u>	<5.70 -11.00	9.90	<.80	540.00	<5.70	56.80	≪5.90	<6.70	<6.80	1.1	1.1	1,500.00	1.2	10,000.00	1.2	-	· -		
Methyl ethyl ketons	4,000,000	ND	NA	<30.00	25.00 <6.00	<11.00	<12.00	<12.00	<78.00	<11.00	<14.00	<14.00	<13.00	<14.00	1.7	1.8	240.00	1.9	<2,600.00	6.7	-	-	- 1	
Toluens	16,000,000	ND	NA	<30.00		ත්.70 ත්.70	<5.80	<.80	<29.00	<5.70	·56.80	≪5.90	<6.70	<6.80			-			-		-	-	
Trichlorofluoromethane	24,000,000	ND	NA ·		≪6.00	< <u>5.70</u>	<del>ර</del> .80	<del>ح</del> .80	<29.00	ব.70		≪6.90	<6.70	<	2.8	2.9	<1,100.00	⊲0.82	<1,100.00	5.5	-	-	-	
Xylenes (total)	160,000,000	ND	NA	14.00	12.00	10.00	10.00	<u>්</u> .80	31.00	7.00	6.90	7.40	<6.70	<	, <b>-</b> ,				-	-		-	-	
e: all units in µg/L.	100,000,000		MA	200.00	<6,00	ব.70	60.00	ර.80	990.00	ජ.70	rf.80	≪5.90	<b>46.70</b>	<6.80	<1.1	<1.2	<150.00	<1.2	57,000.00	<1.2	-		-	-

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Note: all units in µg/L. Care. = carcinogenic effects. NA = not applicable. ND = not determined. ~ = information not available.

Source: ESE.

The areal extent and volume of soils requiring remediation are dependent upon the selection of a preliminary cleanup target or PCT. The PCTs for the organic contaminants of concern at this site were developed in the "Significance of Contamination Report for Hunter Army Airfield Fire Training Area" (ESE, 1993). The PCT analysis used conservative assumptions of a residential exposure duration of 70 years, per the RCRA closure guidance. A less conservative method uses a 20-year exposure for the risk assessment, per CERCLA guidance, and results in significantly higher PCTs. PCTs for metals in soils are taken from EPA guidelines for RCRA cleanups. The selected PCTs for each contaminant of concern are shown in Table 3.1 and are compared to the concentrations detected.

An estimated 2,500 to 11,000 cubic yards (yd<sup>3</sup>) of soils are contaminated with volatile and semi-volatile organics. The majority of this soil is at the ground surface [0-1 foot below ground surface (bgs)]. Approximately 200 to 300 yd<sup>3</sup> of soils on and around the fire training pad have total lead concentrations in excess of the 500 mg/kg PCT. The total extent of soils contamination and volume of contaminated soils will be determined by confirmatory sampling during closure, as described in Section 4.2.3.

### **3.1.1 ORGANIC CONSTITUENTS**

#### 3.1.1.1 Semi-volatiles

Organic soil contamination consists primarily of benzo(a)pyrene, a carcinogenic semi-volatile petroleum hydrocarbon which was detected at levels above its PCT of 120  $\mu$ g/kg in most ground-surface soil samples. Other carcinogenic semi-volatiles (benzo(a)anthracene, benzo(b)fluoranthene, and benzo(k)fluoranthene) were also detected, but not usually at concentration levels exceeding their PCTs. These carcinogenic semi-volatiles were most frequently detected in the surficial soils (0 to 1 foot below ground surface or "bgs") on the northern and western sides of the site (PSB-1, 2, 3, and 4). Some semi-volatile contamination was also found at depths of 3 to 6 feet in the area immediately to the north of the pad (PSB-6, PSB-7, and HSB-2). The pattern of contamination in soils and the lack of

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semi-volatile contamination in groundwater appears to indicate two modes of transport. The first mode is airborne soot and spray droplet dispersion and deposition onto the ground surface where the contamination is then washed by runoff over the ground surface, and eventually into the ditches, while attached to fine particulate matter (silt and soot). The second mode is flushing into the soil of semi-volatiles dissolved into other more mobile hydrocarbons, such as naphthalene and xylene.

Anticipating the results of the first-mentioned transport mechanism, the ground surface to the south of the pad (HSB-4, 5, and 6) is highly likely to be contaminated, since drainage conditions here are similar to those on the north. No surface samples have yet been taken from this area. Since the westernmost surface soil samples (PSB-1 and PSB-2) are contaminated with benzo(a)pyrene, it is possible that the remaining area west of the "woods line" and between the drainage ditches (up to 4,000 yd<sup>3</sup>) could also be contaminated with benzo(a)pyrene and could require remediation. This area is not likely to be extensively contaminated, since the heavy undergrowth would present an effective barrier to overland migration of contaminated silt and soot fines and the magnitude of soot deposition should decrease substantially with distance from the pad. Remediation of soils in the area west of the "woods line," if necessary, is complicated by the presence of medium-sized trees and construction debris.

**3.1.1.2** <u>Volatiles</u>. Volatile hydrocarbons (benzene, ethyl-benzene, and xylene), where detected, were far below their PCTs, except for one benzene detection in PSB-6 (39  $\mu$ g/kg detected vs. a 24  $\mu$ g/kg PCT). This contamination is intermingled with the deeper semi-volatile contamination in the same vicinity and requires no additional excavation. The presence of benzene contamination is also likely in the vicinity of HSB-5, since elevated levels of xylene, ethylbenzene, and naphthalene (which usually accompany benzene) resulted in a benzene detection limit of 1800  $\mu$ g/kg. Elevated benzene levels in groundwater samples

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from HMW-6 and HMW-7 would also tend to indicate a benzene source area to the south of the pad. This contaminated soil volume is estimated at 500 to 1,000 yd<sup>3</sup>.

### 3.1.2 METALS

In 1987, lead was detected at levels in excess of the 500 milligrams per kilogram (mg/kg) PCT at the ground surface in borings BH-10, BH-11, and BH-13, immediately adjacent to the pad. USAEHA tested these soils for extraction procedure toxicity in 1987, in accordance with the requirements of 40 CFR 262 at that time, and found no detectable lead in the leachate. For this reason, these soils are not believed to exhibit a characteristic hazard due to leachable lead, but this must be confirmed prior to disposal by TCLP analysis. The soils on the pad are assumed to also contain elevated levels of lead. No other soil samples indicated metal concentrations at levels of concern. It is estimated that 50 to 100 yd<sup>3</sup> of lead-contaminated surficial soils are present adjacent to the pad plus 150 to 200 yd<sup>3</sup> on the pad.

**3.1.3 SUMMARY**. Based on interpretation of soils analytical results, the total area and volume of soils requiring remediation is summarized in Table 3.2. A visual representation of these interpretations is provided in Figures 3-2 through 3-4. Figure 3-2 shows the site plan with areas of known, probable, and possible benzo(a)pyrene surface soils contamination. Figure 3-3 shows the areas of known and possible contamination of deeper soils (to 6 feet). Figure 3-4 shows the estimated areas of lead contamination of surface soils adjacent to the pad and the cover soils on the pad.

Table 3.2 Summary of Known and Potential	Soils Remedia	ation Volumes	
		KNOWN	TOTAL
	KNOWN	PLUS	POSSIBLE
AREA	VOLUME	PROBABLE	VOLUME
Surface Soils (0-1' bgs)		-	
North of the pad to ditch			
and west to "woods line"	1,500	2,000(1)	2,000
South of pad to ditch and		8 8 82	
west to "woods line"		1,000	1,000
West of "woods line" to		2 (S.17 S)	
ditch confluence		-	4,000
<i>y</i>			
Deeper Soils (1-6' bgs)			
North of pad around			
HSB-2, PSB-6, & PSB-7	1,000	1,000	3,000
South of pad around HSB-5	<u>-</u> ,	500	1,000
A COLOR DO LOUIS DO L			Vietna III - See second da anno 1
TOTAL ORGANIC-CONTAMINATED	2,500	4,500	11,000
		No. 10	
2			
Toxic Metals-Contaminated Surface Soils (0-1' b	egs)		
On pad	150	150	200
Adjacent to pad (BH-10, 11, & 13)	50	50	100
vennes © elementate inners ≥ statut in varie ≥ statute. S			
TOTAL METALS-CONTAMINATED	200	200	300

Table 3.2 Su	immary of	Known and	<b>Potential Soils</b>	Remediation	Volumes
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(1) Includes area of PSB-6, PSB-7, and HSB-2, where no contamination was detected at the ground surface, but soils would be difficult to segregate from deeper contaminated soils.

Source ESE, 1993



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### 3.2 SEDIMENT CONTAMINATION

Ditch sediments were sampled during both the 1990 and 1992 site investigations. Sample locations are shown in Figure 3-5 and analytical results are can be seen in Table 3.3. In 1990, sediment sample HSD-1 in the south ditch and HSD-3 in the north ditch were found to be contaminated with benzo(a)pyrene at concentrations of 9,200 and 18,000  $\mu$ g/kg, respectively, as well as other semi-volatiles. Samples HSD-1 and HSD-2 also had detectable levels of methylene chloride. In 1992, sediments were sampled in four locations (PSS-1 and -2 in the south ditch and PSS-3 and -4 in the north ditch) and were found to be contaminated in three of the four samples by semi-volatile hydrocarbons, primarily benzo(a)pyrene. Both sediment samples from the south ditch were found to be contaminated (850  $\mu$ g/kg benzo(a)pyrene in PSS-1 and 12,000  $\mu$ g/kg in PSS-2). In the north ditch only the western-most (downstream) sediment sample (400  $\mu$ g/kg benzo(a)pyrene in PSS-4) was found to be contaminated. possibly indicating a downstream migration of sediments due to stormwater flows since the last training exercise. The only volatile detected in 1992 was trichlorofluoromethane, which was detected at levels nearly equal to the detection limit (7.0  $\mu$ g/kg in PSS-1, 6.9 in PSS-2, and 7.4 in PSS-3, compared to detection limits of 5.7 to 6.8  $\mu$ g/kg). Because the ditch bottom elevations (approximately 15 ft msl) are significantly lower than both the ground surface and the local groundwater piezometric surface (30 ft msl, and 25 ft msl, respectively), the ditches act as interception trenches for both surface runoff and groundwater seepage. No sediment samples were taken further west than approximately 400 feet from the culvert outfalls into each ditch, but due to the levels of contaminants in these samples, it is presumed that contaminated sediments are present to at least the ditch confluence.

### 3.3 GROUNDWATER

### 3.3.1 METALS

The concentrations of arsenic, chromium, and selenium detected in a 1990

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### Table 3.3 Comparison of Maximum Sediment Concentrations Detected at Hunter AAFTA to PCTs

		PC (mg/	States Access		Background (mg/kg)	Southwe	age Ditch st of Fire Pit g/kg)	Northwes	ge Ditch at of Fire Pit g/kg)	Exceedance
Chemical	Systemic Effects		Carcinog Effect	110000000000	Southeastern Georgia (a)	HSD-1, HSD-2	PSS-1, PSS-2	HSD-3	PSS-3, PSS-4	of PCT
INORGANICS Arsenic Barium Chromium, total** Lead	80 4,000 400 500 *		0.4 NA NA NA		<0.1 · 6.5 10 · 200 1.0 · 20 <10 · 10	0.76 19.8 3.38 7.71	0.499 15.6 5.66 29.4	BDL 229 69.7 362	1.05 12 3.54 BDL	1,2 3 3 3
PAHs Acenaphthene Acenaphthylene Anthracene Benz(a)anthracene Benzo(a)pyrene Benzo(b)fluoranthene Benzo(k)fluoranthene Benzo(k)fluoranthene Chrysene Dibenz(ah)anthracene Fluoranthene Fluorene Indeno(1,2,3-cd)pyrene Naphthalene Phenanthrene Pyrene	24,000 ND ND ND	₽ ₽	ND ND 1.2 0.12 1.2 ND 1.2 12 0.12 ND ND 1.2 ND ND ND	++ ++ ++ ++ ++	24 24 24 24 24 24 24 24 24 24 24 24 24 2	1.1 BDL 3 13 9,2 76 6.2 7.2 22 4.2 36 1.5 7.9 BDL 20 27	BDL BDL 2.4 13 12 13 5.1 12 15 BDL 34 1.2 7.6 BDL 19 21	4.9 3.1 9.3 33 27 27 17 29 52 11 62 8.3 23 0.39 62 58	0.11 BDL 0.13 0.51 0.4 0.45 BDL 0.39 0.67 BDL 1.2 0.13 BDL 1.4 0.99	1 1 1 1 1 1
VOLATILE ORGANICS Acetone Benzene Carbon disulfide Methylene chloride Toluene Trichlorofluoromethane Xylenes, total	8,000 1,600 8,000 4,800 16,000 24,000 160,000		ND 24 ND 93 ND ND ND	Q R	NA NA NA NA NA	0.11 BDL 0.023 0.012 0.0032 BDL BDL	BDL BDL BDL BDL 7.4 BDL	0.12 0.031 BDL BDL BDL BDL 0.0024	BDL BDL BDL BDL BDL BDL BDL	

Note: ND = not determined.

NA = not applicable.

PAH = polycyclic aromatic hydrocarbon.

BDL = below detection limit.

NRQ = not required.

mg/kg = milligrams per kilogram.

(a) Average metal concentration in soils southwest of Savannah, Georgia (Shacklette and Boerngen, 1984).

(1) Site levels exceed carcinogenic PCT (highlighted in table).

(2) Regional background value exceeds carcinogenic PCT (highlighted in table).

(3) Some site levels exceed background but are within PCT.

\*Sediment samples were collected from the drainage ditches in 1990 (HSD) and 1992 (PSS).

\*\*Assumes chromium is present as the more potent hexavalent species.

\*\*\*Interim cleanup level established by EPA (1991).

+ No RID is available for this PAH; the RID for the most potent non-naphthalene PAH (pyrene) is used for comparison, only.

+ + Interim Region IV Guidance on Toxicity Equivalency Factor (TEF) methodology for carcinogenic PAHs based on each compounds relative potency to the potency of benzo(a)pyrene (EPA, February 1992). The following TEFs were used to convert the CSF for benzo(a)pyrene to an equivalent CSF for the particular carcinogenic PAH: benz(a)anthracene = 0.1, benzo(b)fluoranthene = 0.1, benzo(k)fluoranthene (0.1), chrysene (0.01), dibenz(ah)anthracene = 1.0, and indeno(1,2,3-cd)pyrene = 0.1.

Source: ESE.

### 3.3 GROUNDWATER

### 3.3.1 METALS

The concentrations of arsenic, chromium, and selenium detected in a 1990 groundwater sample from a shallow downgradient well (HMW-6) exceed Federal and State of Georgia MCLs. Lead levels detected in the 1990 samples from the same well, in addition to shallow downgradient well HMW-4 are above the EPA action level for lead. The 1990 concentrations of arsenic, barium, chromium, and lead detected in the shallow upgradient well (HMW-2) also exceed (or are equivalent to) their respective PCTs. No metals were detected above their PCTs in 1992. The results of sediment analyses are summarized in Table 3.4.

### 3.3.2 ORGANICS

Benzene was detected above its MCL (5  $\mu$ g/L) in several wells [HMW-3 (1990), HMW-4 (1992), HMW-6 (1990 and 1992), HMW-7 (1992), and HMW-9 (1992)]. Table 3.4 presents the results of analysis of groundwater samples taken during the 1992 field effort. The analytical results of both the 1990 and 1992 field investigations are provided in Appendix E. The lateral extent of benzene contamination was not delineated during this field effort. In addition to benzene, vinyl chloride was detected above its MCL in the 1992 sample from HMW-6. The only other chemicals measured in groundwater above PCTs were three PAHs, which were detected in the 1990 sample from HMW-6. PAHs were not detected above PCTs in any of the wells during the 1992 field effort (ESE,1993a). A site plan showing the location of monitoring wells with a superimposed visual interpretation of the extent of groundwater benzene contamination is provided as Figure 3-5.

PARAMETERS	UNITS	1-WMH	HMW-2	HMW-3	HMW-4	HMW-5	9-MMH	2-WMH	HMW-8	6-MMH	HMW-5DUP	HSOURCE	TRPBLK	EQPBLK
a S		03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92 03/12/92 03/12/92	03/12/92	03/12/92	03/12/92
		13:30	13:40	14:20	14:30	13:50	14:00	14:10	14:40	15:00		16:30		13:15
1,1,1-TRICHL'ETHANE	NG/L	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<25.00	<2.50	<13.00	<2.50	<2.50	<2.50	<2.50
1,1,2,2-TETRACHLORO- ETHANE	E UG/L	<1.50	<1.50	<1.50	<1.50	<1.50	<1.50	<15.00	<1.50	<7.50	<1.50	<1.50	<1.50	<1.50
1,1,2-TRICHL'ETHANE	NG/L	<2.80	<2.80	<2.80	<2.80	<2.80	<2.80	<28.00	<2.80	<14.00	<2.80	<2.80	<2.80	<2.80
1,1-DICHLOROETHANE	NG/L	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<25.00	<2.50	<13.00	<2.50	<2.50	<2.50	<2.50
1,1-DICHLOROETHYLENE	NG/L	<3.20	<3.20	<3.20	<3.20	<3.20	<3.20	<32.00	<3.20	<16.00	<3.20	<3.20	<3.20	<3.20
1, 2-DI CHLOROETHANE	NG/L	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<25.00	<2.50	<13.00	<2.50	<2.50	<2.50	<2.50
1,2-DICHLOROETHENE(TOTAL)	UG/L	<2.40	<2.40	<2.40	<2.40	<2.40	3.50	<24.00	<2.40	<12.00	<2.40	<2.40	<2.40	<2.40
1, 2-DI CHLOROPROPANE	UG/L	<2.00	<2.00	<2.00	<2.00	<2.00	<2.00	<20.00	<2.00	<10.00	<2.00	<2.00	<2.00	<2.00
2-CHLOROETHYLVINYL- ETHER	UG/L	<3.10	<3.10	<3.10	<3.10	<3.10	<3.10	<31.00	<3.10	<16.00	<3.10	3.10	<3.10	<3.10
ACENAPHTHENE	UG/L	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<10.00	<1.00	<1.00	<1.00	<1.00	NRQ	<1.00
ACENAPHTHYLENE	UG/L	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<10.00	<1.00	<1.00	<1.00	<1.00	NRQ	<1.00
ANTHRACENE	UG/L	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<10.00	<1.00	<1.00	<1.00	<1.00	NRQ	<1.00
ARSENIC, TOTAL	UG/L	6.40	<2.30	<2.30	2.30	2.70	14.70	11.30	<2.30	5.20	<2.30	<2.30	NRG	<2.30
BARIUM, TOTAL	NG/L	76.60	46.50	88.10	54.40	56.60	57.20	147.00	65.00	113.00	56.50	14.90	NRG	<1.10
BENZENE	NG/L	<1.00	<1.00	<1.00	18.00	<1.00	120.00	660.00	3.50	15.00	<1.00	<1.00	<1.00	<1.00
<b>BENZO(A)ANTHRACENE</b>	UG/L	<1.50	<1.50	<1.50	<1.50	<1.50	<1.50	<15.00	<1.50	<1.50	<1.50	<1.50	NRQ	<1.50
BENZO(A)PYRENE	UG/L	<2.00	<2.00	<2.00	<2.00	<2.00	<2.00	<20.00	<2.00	<2.00	<2.00	<2.00	NRQ	<2.00
BENZO(B) FLUORANTHENE	∩¢/r	<1.50	<1.50	<1.50	<1.50	<1.50	<1.50	<15.00	<1.50	<1.50	<1.50	<1.50	NRQ	<1.50
BENZO(GHI)PERYLENE	NG/L	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<25.00	<2.50	<2.50	<2.50	<2.50	NRQ	<2.50
BENZO(K) FLUORANTHENE	UG/L	<1.50	<1.50	<1.50	<1.50	<1.50	<1.50	<15.00	<1.50	<1.50	<1.50	<1.50	NRO	<1.50
BROMOD I CHLOROMETHANE	UG/L	<2.20	<2.20	<2.20	<2.20	<2.20	<2.20	<22.00	<2.20	<11.00	<2.20	<2.20	<2.20	<2.20
BROMOFORM	UG/L	<2.60	<2.60	<2.60	<2.60	<2.60	<2.60	<26.00	<2.60	<13.00	<2.60	<2.60	<2.60	<2.60

cical Parameters Detected in Groundwater Samples in 1992

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Table 3.4 ji

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PARAMETERS	UNITS	HMW-1	HMW-2	HMW-3	HMW-4	HMW-5	9-MMH	7-WMH	HMU-8	6-MMH	HMW-SDUP	HSOURCE	TRPBLK	EapBLK
		03/12/92	03/12/92	03/12/92	03/12/92	03/12/92 03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92
	-	13:30	13:40	14:20	14:30	13:50	14:00	14:10	14:40	15:00		16:30	54.	13:15
BROMOMETHANE	UG/L	<3.50	<3.50	<3.50	<3.50	<3.50	<3.50	<35.00	<3.50	<18.00	<3.50	<3.50	<3.50	<3.50
CADMIUM, TOTAL	UG/L	<4.40	<4.40	<4.40	<4.40	<4.40	<4.40	<4.40	<4.40	<4.40	<4.40	<4.40	NRQ	<4.40
CARBON DISULFIDE	UG/L	<4.40	<4.40	<4.40	<4.40	<4.40	<4.40	<44.00	<4.40	<22.00	<4.40	<4.40	<4-40	<4.40
CARBON TETRACHLORIDE	NG/L	<2.60	<2.60	<2.60	<2.60	<2.60	<2.60	<26.00	<2.60	<13.00	<2.60	<2.60	<2.60	<2.60
CHLOROBENZENE	NG∕L	<1.40	<1.40	<1.40	<1.40	<1.40	<1.40	<14.00	<1.40	<7.00	<1.40	<1.40	<1.40	<1.40
CHLOROETHANE	UG/L	<8.20	<8.20	<8.20	<8.20	<8.20	<8.20	<82.00	<8.20	<41.00	<8.20	<8.20	<8.20	<8.20
CHLOROFORM	∩c/r	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<25.00	<2.50	<13.00	<2.50	<2.50	<2.50	<2.50
CHLOROMETHANE	NG/L	<4.40	<4.40	<4.40	<4.40	<4.40	<4.40	<44.00	<4.40	<22.00	<4.40	<4.40	<4.40	<4.40
CHROMIUM, TOTAL	NG/L	17.60	<7.40	<7.40	<7.40	<7.40	<7.40	18.60	<7.40	9.10	<7.40	<7.40	NRG	<7.40
CHRYSENE	nc∕L	<1.50	<1.50	<1.50	<1.50	<1.50	<1.50	<15.00	<1.50	<1.50	<1.50	<1.50	NRQ	<1.50
CIS-1,3-DICHLORO- PROPENE	∩c∕L	<2.00	<2.00	<2.00	<2.00	<2.00	<2.00	<20.00	<2.00	<10.00	<2.00	<2.00	<2.00	<2.00
DIBEN' (A, H)ANTH' CENE	∩G/L	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<25.00	<2.50	<2.50	<2.50	<2.50	NRQ	<2.50
D 1 BROMOCHLOROMETHANE	∩G/L	<2.30	<2.30	<2.30	<2.30	<2.30	<2.30	<23.00	<2.30	<12.00	<2.30	<2.30	<2.30	<2.30
DICHLOROBENZENE, TOT.	NG/L	<4.00	<4.00	<4.00	<4.00	<4.00	<4.00	<40.00	<4.00	<20.00	<4.00	<4.00	<4.00	<4.00
DIETHYL ETHER, TOTAL	UG/L	<5.00	<5.00	<5.00	<5.00	<5.00	<5.00	<50.00	<5.00	<30.00	<5.00	<5.00	<5.00	<5.00
ETHYLBENZENE	UG/L	<1.30	<1.30	<1.30	<1.30	<1.30	82.00	130.00	<1.30	180.00	<1.30	<1.30	<1.30	<1.30
FLUORANTHENE	NG∕L	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<10.00	<1.00	<1.00	<1.00	<1.00	NRO	<1.00
FLUORENE	∩¢/r	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<10.00	<1.00	<1.00	<1.00	<1.00	NRQ	<1.00
INDENO(1,2,3-CD) PYRENE	∩c/L	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<25.00	<2.50	<2.50	<2.50	<2.50	NRO	<2.50
LEAD, TOTAL	UG/L	<63.80	<63.80	<63.80	<63.80	<63.80	<63.80	<63.80	<63.80	<63.80	<63.80	<63.80	NRQ	<63.80
MERCURY, TOTAL	UG/L	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	NRO	<0.18
METHYL ETHYL KETONE	∩6∕L	<10.00	<10.00	<10.00	<10.00	<10.00	<10.00	<100.00	<10.00	<50.00	<10.00	<10.00	<10.00	<10.00

ntinued, Page 2 of 3 , cical Parameters Detected in Groundwater Samples in 1992, Hunter AAF

Table 3- .

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Table 3- ..... .cal Parameters Detected in Groundwater Samples in 1992, Hunter AAFhr. Intinued, Page 3 of 3

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PARAMETERS	UNITS	HMW-1	HMW-2	HMW-3	4-WMH	HMW-5	9-MMH	7-WMH	8-WMH	HMW-9	HMW-5DUP	HSOURCE	TRPBLK	EQPBLK
		03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92	03/12/92
		13:30	13:40	14:20	14:30	13:50	14:00	14:10	14:40	15:00		16:30		13:15
METHYL ISOBUT'KETONE	1/9N =	<12.00	<12.00	<12.00	<12.00	<12.00	<12.00	<120.00	<12.00	<60.00	<12.00	<12.00	<12.00	<12.00
METHYLENE CHLORIDE	NG/L	<6.40	<6.40	<6.40	<6.40	<6.40	<6.40	<64.00	<6.40	<32.00	<6.40	<6.40	<6.40	<6.40
NAPHTHALENE	NG/L	<1.00	<1.00	<1.00	<1.00	<1.00	14.00	13.00	<1.00	33.00	<1.00	<1.00	NRG	<1.00
PHENANTHRENE	NG/L	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<10.00	<1.00	<1.00	<1.00	<1.00	NRQ	<1.00
PYRENE	NG/L	<1.00	<1.00	<1.00	<1.00	<1.00	<1.00	<10.00	<1.00	<1.00	<1.00	<1.00	NRO	<1.00
SELENIUM, TOTAL	NG/L	<2.00	<2.00	<2.00	<2.00	<2.00	2.10	6.50	<2.00	<2.00	<2.00	<2.00	NRQ	<2.00
SILVER, TOTAL	NG/L	<6.10	<6.10	<6.10	<6.10	<6.10	<6.10	<6.10	<6.10	<6.10	<6.10	<6.10	NRO	<6.10
TETRACHLOROETHENE	NG/L	<1.90	<1.90	<1.90	<1.90	<1.90	<1.90	<19.00	<1.90	<9.50	<1.90	<1.90	<1.90	<1.90
TOLUENE	UG/L	<1.70	<1.70	<1.70	<1.70	<1.70	1.80	<17.00	<1.70	<8.50	<1.70	<1.70	<1.70	<1.70
TRANS-1,3-DICHLORO-	PROPENE UG/L	<1.60	<1.60	<1.60	<1.60	<1.60	<1.60	<16.00	<1.60	<8.00	<1.60	<1.60	<1.60	<1.60
TRICHLOROETHENE	NG/L	<3.00	<3.00	<3.00	<3.00	<3.00	<3.00	<30.00	<3.00	<15.00	<3.00	<3.00	<3.00	<3.00
TRICHLOROFLUORO-	METHANE UG/L	<4.60	<4.60	<4.60	<4.60	<4.60	<4.60	<46.00	<4.60	<23.00	<4.60	<4.60	<4.60	<4.60
VINYL CHLORIDE	NG/L	<4.60	<4.60	<4.60	<4.60	<4.60	12.00	<46.00	<4.60	<23.00	<4.60	<4.60	<4.60	<4.60
XYLENES, TOTAL	nc/L	<3.70	<3.70	<3.70	<3.70	3.70	3.70	820.00	<3.70	950.00	<3.70	<3.70	<3.70	<3.70

Source: ESE.

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### 4.0 CLOSURE ACTIVITIES

Pursuant to Section 3004(u) of RCRA and 40 CFR 264.101, the fire training area will be closed to remove the source of a continuing release to the environment and contaminated environmental media (soils, sediments, and groundwater) will be remediated to achieve the cleanup targets presented in Section 3.0. Successful treatment of contaminated soils and sediments will reduce levels of volatiles to nondetect and semi-volatiles to less than the preliminary cleanup target (PCT). Soils contaminated with metals in excess of the selected PCTs (soils on and adjacent to the fire training pad) will be stabilized, as necessary, and disposed of off-site. Closure of the fire fighting training area will be accomplished in the following phases:

a)	Phase I	-	Site Preparation
b)	Phase II	-	Contaminated Soil and Sediment Remediation
c)	Phase III		Groundwater Remediation
d)	Phase IV	-	Site Restoration

#### 4.1 PREPARATION

### 4.1.1 TEMPORARY FACILITIES AND SITE CONTROL

Prior to any disturbance of site soils, temporary facilities will be set up and boundaries will be marked to prevent the spread of contamination and exposure of personnel by construction activities. Temporary facilities include the equipment and personnel decontamination area, excavated soil staging area, and thermal treatment area. Since the site is on a military reservation, adequate site control can be achieved by marking the work site boundaries with tape and rubber cones. The arrangement of remediation work areas is shown in Figure 4-1.

### 4.1.2 FUEL TANK CLOSURE

#### 4.1.2.1 Tank Contents:

Tank contents will be sampled and analyzed for evidence of hazardous constituents (total halogens and total metals). The tank contents will be drained and disposed of

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at a licensed commercial facility as either off-specification fuel or hazardous waste, depending upon the results of the characterization analyses. The tank atmosphere will be inerted by forced ventilation until the tank interior registers less than 10 percent of the lower explosive limit (LEL), as measured by an explosimeter. The tank interior will be steam cleaned and the residue will be disposed of at a licensed commercial facility.

## 4.1.2.2 <u>Tank:</u>

The emptied and cleaned tank will be cut up and disposed of as scrap steel through the Defense Reutilization and Marketing Office (DRMO).

## 4.1.2.3 Fuel Piping:

The fuel piping will be flushed with a small quantity of water and the residue disposed of along with the tank-cleaning residues. The entire length of piping will be excavated and removed (after demolition of the fire training pad, as described in Paragraph 4.1.3). The piping will be visually inspected for leaks after excavation. All joints and fittings will be inspected for evidence of holes or leakage. All revealed surfaces of the pipe trench excavation will be inspected for evidence of leakage. Evidence of leakage would include stained soil, areas of free product, etc. Where evidence of a release from the piping is uncovered, the contaminated soils will be identified and excavated as described in Paragraphs 4.2.5.2. All excavated soils will be stockpiled for thermal treatment as described in Paragraph 4.2.7.

#### 4.1.2.4 Tank Pad:

The tank pad will be demolished and the rubble disposed of in the on-site construction debris landfill.

## 4.1.3 FIRE TRAINING PAD CLOSURE

## 4.1.3.1 Simulated Aircraft:

The simulated aircraft, constructed of a steel tank, will be steam cleaned (to remove petroleum residues), cut up, and disposed of as scrap steel through DRMO.

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## 4.1.3.2 Pad Cover Soils:

All cover soils will be consolidated onto one corner of the pad. The leadcontaminated soils will be excavated from the areas shown in Figure 3-4 and will be combined with the cover soils. The soils will be blended by mixing with a frontloading tractor or other excavation equipment until a homogeneous-appearance is achieved. The stockpile will then be relocated onto plastic sheeting on the adjacent runway pavement in preparation for pad decontamination. Sediments from the sump, after pad decontamination per Paragraph 4.1.3.3, will be added to the pad cover-soil stockpile. A representative sample will than be taken and analyzed by Toxicity Characteristic Leaching Procedure (TCLP). Depending upon the outcome of the characterization analysis, the soils will be treated and/or disposed of separately from other site soils, as described in the applicable portions of Paragraphs 4.2.7 through 4.2.9. Prior to treatment or disposal, the stockpiled soils will be covered with 10-mil "visqueen" except when being handled or sampled.

#### 4.1.3.3 Pad Decontamination and Demolition:

After all bulk soils have been removed from the pad, the pad surface will be decontaminated by pressure-washing or steam-cleaning. All wash water will be swept into the pad's drain sump, pumped out, and disposed of by a licensed commercial waste facility. Sediments from the sump will be added to the cover-soil stockpile per Paragraph 4.1.3.2. Concrete samples will be taken from four randomly selected locations on the pad surface by means a hand-held pin scabbler with a high-efficiency particulate absolute (HEPA) vacuum attachment (Pentek or equivalent). The consolidated sample will be analyzed by TCLP for hazardous characteristics. If non-hazardous, the pad will then be demolished. If the sample is found to be hazardous, 1/2 inch of the concrete surface will be removed by vacuum scabbling. The scabbling residue will be disposed of as hazardous waste. The pad will then be demolished and the rubble disposed of in the on-site construction debris landfill.

# 4.2 <u>SEDIMENT/SOIL REMEDIATION</u>

## 4.2.1 TREATABILITY TESTING

Samples of soils and sediments which are representative of the most highly contaminated areas (soils from the vicinity of HSB-2, PSB-6, and PSB-7 and sediments from the vicinity of PSS-2) will be bench-treatability tested prior to mobilization of construction equipment and the thermal treatment systems. Testing will determine the required temperature and residence time to achieve non-detect levels of the volatile and semi-volatile contaminants of concern in the soil and sediment samples.

## 4.2.2 PRELIMINARY GROUND SURFACE SAMPLING

Soil samples will be taken from the ground surface to the west of the "woods line" to determine the westward extent of semi-volatile contamination of surface soils. Sampling procedures, documentation, and quality control will be as presented in Section 5.0 and the existing CDAP. Samples will be taken at 50-foot intervals along three east-west lines and at four locations to the south of the pad, as shown in Figure 4-2. Sample locations will be staked and labeled to facilitate the identification of the limits of clearing and grubbing and limits of excavation after analysis. If two or more of the samples from the south side of the pad are found to be uncontaminated, further sampling will be performed to better define the limits of contamination. If three or more samples are contaminated, the entire ground surface will be assumed to be contaminated to the ditch on the south and to the first uncontaminated sample to the west of the "woods line" on the west.

## 4.2.3 EROSION AND SEDIMENT CONTROL

Prior to disturbance of any soils or sediments, silt fences will be installed across the north and south ditches every 200 feet, starting just west of the limits of excavation and continuing at least to the location of the first uncontaminated ditch sample to the



west. Immediately after clearing and grubbing in the wooded area, silt fencing, hay bales, and other erosion protection will be installed along the down-slope edge of the cleared and grubbed area.

#### 4.2.4 CLEARING AND GRUBBING

Clearing and grubbing, separate from excavation, will only be required for site soils to be excavated beyond the "woods line" shown in Figure 3.1. The limits of clearing and grubbing will be from the "woods line" to a line drawn between locations of the nearest westward soil samples which contain less than the PCT of all volatile and semi-volatile contaminants of concern. Trees, brush, and other vegetative matter will be cut down to as close to the ground surface as possible. This material will be disposed of as solid waste. Large roots and vegetative material (over 1/4 inch diameter) taken from beneath the soil will be separated from the soils by vibratory screening. The roots will be chipped and disposed of as solid waste. Soils containing only grass and smaller roots can be thermally treated without separating out vegetative matter. Where debris or wreckage is encountered, it will be steam cleaned on the equipment decontamination pad, to remove any adhering soils, and transferred to DRMO for disposal as scrap or solid waste.

#### 4.2.5 EXCAVATION OF CONTAMINATED SOILS

#### 4.2.5.1 Excavation of Surface Soils

Surface contamination has been identified by previous sampling to be present in the interval of 0-1'bgs over the majority of the land surface in the closure area. Contamination with toxic metals is closely confined to the area immediately around the fire training pad. Semi-volatile contamination is expected to be present over the ground surface of most of the remainder of the closure area. Because the semi-volatile surface contamination is closely associated with soot, it is highly likely that the contamination is actually confined to the interval of 0-6" bgs. To minimize the

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volume excavated and treated, all surface soils within the confirmed limits of surface contamination will initially be excavated to a depth of 6 inches. The exposed ground surface (except where deeper excavation is known to be required) will be sampled as described in Section 5.0. Each grid area where contamination is detected in excess of PCTs will be excavated an additional 6 inches in depth and the excavated surface resampled and analyzed. The known and probable extents of surface contamination are shown in Figure 3.2. Excavation and transport equipment will not leave the contaminated area without being decontaminated as described in paragraph 4.4. Excavated soils will be transported to stockpiles in the thermal treatment area or will be directly transferred to the feed hopper of the thermal treatment unit. To minimize erosion problems and maintain manageable stockpile volumes, the entire ground surface will not be excavated in one single operation. The site surface will be divided into 3 areas: the area south of the pad centerline west to the "woods line," the cleared area north of the pad centerline, and the area west of the "woods line" determined to be contaminated by preliminary ground surface sampling. Excavation will proceed from the south ditch to the north and west. Contaminated soils will be hauled to the treatment zone across the unexcavated northern area and over the decontamination pad. Once all contaminated soils have been removed from an adequate portion of the south area, treated soils from the LTVS will be transported down the paved road and staged on the clean portions of the south area. Backfilling will proceed by pushing clean soils to the north in 8- to 12-inch loose lifts onto adjacent areas where removal of contaminated soils has been certified as complete.

#### 4.2.5.2 Excavation of Deeper Soils (1-6 feet bgs)

Excavation of deeper soils must be performed in the vicinity of HSB-2 on the north side of the pad and HSB-5 on the south. The limits of soil contamination will be determined by a three-step process. First, visual and olfactory examination (if conditions prevent this due to risk of exposing workers to hazardous vapor

concentrations, an FID can be used to "sniff" a newly-exposed soil surface) will be made of the sides of the excavation. When the excavation has proceeded into soils which no longer appear contaminated to the senses, a screening sample will be taken and tested for headspace vapor concentration using a flame ionization detector (FID) per paragraph 4.2.7. Where the excavation has been completed to groundwater, samples will be taken from the backhoe bucket at 25-foot intervals along the side and from near the bottom of the excavation. In areas where the excavation stops short of groundwater, samples will also be taken from the bottom of the excavation on 25-foot centers. The samples will be placed in pint jars and covered with aluminum foil. After the soil temperature is allowed to equilibrate for a period of approximately 5 minutes, the sample headspace vapors will be field-analyzed by puncturing the aluminum foil with the tip of a FID probe. If the sample headspace reading is less than 10 ppm non-methane TOV, the sample will be presumed clean, pending confirmatory laboratory analysis. If the headspace reading exceeds 10 ppm, the excavation will be advanced by a distance selected by the site manager and another headspace sample will be analyzed.

#### 4.2.5.3 Excavation Hazards

No elevated organic vapor levels have been detected in surface soils, but worker protection from exposure to dust-borne toxic metals and carcinogenic semi-volatiles must be provided during surface excavation. During deeper excavation, the potential exists for elevated levels of contaminant vapors in the excavation. Soil gas levels were measured in excess of 1,000 ppm total organic vapor (TOV) during the 1990 field investigation at most locations within approximately 20 feet of the edge of the pad and also near HSB-4. Soil headspace vapor concentrations (see boring logs attached to Appendix B) ranged up to 500 ppm TOV in HSB-2, with HSB-2, -3, and -4 and PSB-1, -4, and -6 reading in excess of 100 ppm. Levels of breathing protection

required during excavation must be determined by the site safety officer in response to real-time air monitoring of the excavation area.

#### 4.2.6 EXCAVATION OF CONTAMINATED DITCH SEDIMENTS

After all contaminated soils have been excavated, contaminated ditch sediments will be removed to a depth of 6 inches. If necessary, base flows due to surface drainage and upstream seepage will be diverted around the contaminated reaches of the ditches by installation of sandbag coffer-dams at the culvert outfalls and by piping the base flows around the excavation areas. During dry weather conditions, it may be possible to excavate the majority of the ditch bottoms without any water diversion. Excavation will begin at the edges of the concrete aprons at the culvert outlets and proceed westward. Excavation will be completed upon reaching the first silt fence beyond the sample point where contaminant levels are below the PCTs or are non-detectable (termination point), as determined by preliminary sediment sampling per paragraph 4.2.6. Silt fences will remain in place in the ditches during excavation, with each successive fence removed as the excavation reaches it. When the excavation of sediments has been completed to the termination point, excavation will stop and confirmatory samples will be taken. One sample will be taken from immediately downstream of the silt fence at the termination point and another from immediately upstream of the next downstream fence. Since low levels of semi-volatiles, which comprise the primary sediment contamination, are not detectable by field methods, samples must be analyzed in the laboratory and excavation must be halted until results of analyses are available. If the samples are found to be uncontaminated (no contaminants present in excess of PCTs) the excavation is complete. If contamination is detected downstream of the termination point, excavation will continue to the next fence and confirmatory sampling will be repeated. Silt fences will remain in place until site restoration has established adequate vegetative cover of the site to prevent significant erosion.

Sediments present very little hazard to workers, since only dilute concentrations of semi-volatiles are present. The primary exposure pathway is by ingestion, unless the sediments are permitted to dry to the point where respirable dusts can be generated.

# 4.2.7 THERMAL TREATMENT OF SOILS AND SEDIMENTS

## 4.2.7.1 <u>Treatment System Description</u>

Soils will be treated by a low-temperature volatilization system (LTVS), similar to a rotary kiln, which indirectly heats soils to a maximum exit temperature of 600°F, to vaporize and remove volatile and semi-volatile organic contaminants. The system is an integrated process, which includes all air emissions control processes, instrumentation, piping, utilities and material handling equipment necessary to successfully treat soils. The LTVS may include, but is not limited to, the following components: feed hopper and screening equipment, conveyor system, desorption processing unit, appropriate air pollution control devices, continuous emissions monitors, cyclone, afterburner, evaporator, cooler, condensers, baghouse, fans, connective ductwork, ancillary piping, wiring, and controls. Typical throughput capacities of available systems range from 1,000 to 15,000 lb per hour (0.4 to 5 cy per hour). A flow diagram for a typical system is shown in Figure 4-3. Since remediation must be performed under a competitively bid contract and the government cannot unnecessarily restrict competition, the actual configuration, size, and throughput capacity of the system which will be used cannot be predicted at this time.

The system will be located in the uncontaminated grassy area to the north of the fire training area, as shown in Figure 4-2. Stockpiles of soils to be treated will be maintained in covered roll-off containers or placed on a 60-mil HDPE liner and covered with a 10-mil plastic cover to prevent erosion and creation of contaminated runoff and to minimize volatilization of contaminants from the stockpiles to the atmosphere. After completion of treatment of all excavated and stockpiled soils, and



prior to demobilization of the thermal treatment system, the exposed ground surface in the treatment area and the ground surface in the stockpiling area will be sampled and analyzed. Any areas with contaminant levels exceeding PCTs will be excavated to a depth of 3 to 6 inches and resampled. The excavated material will be treated in the LTVS and returned to the area from which it was taken. Soils which are only accessible after dismantling the LTVS will be tested after removal of the system, and if found to be contaminated, will be excavated and transported for off-site disposal.

#### 4.2.7.2 System Performance

The system selected must be capable of treating site soils and reducing concentrations of hazardous waste constituents (40 CFR 262, Appendix VIII: benzene, ethylbenzene, xylene, toluene, trichlorofluoromethane, methyl-ethyl ketone, and methylene chloride) to non-detectable levels (less than approximately 5  $\mu$ g/kg for most constituents) while meeting all applicable air emission standards with its treated off-gas. Semi-volatile contaminant concentrations must be reduced to less than PCTs. The operating temperature and residence time derived from treatability testing under paragraph 4.2.1 will be provided to bidders as a guideline for how successful treatment might be achieved, but the treatment system operator will be free to operate at other temperatures and speeds, provided that he adequately demonstrates that the system meets the treatment goals under the proposed operating conditions. The preceding is provided for general information only. Specific treatment system performance parameters and compound-specific treatment goals will be developed during system design. Treatment system capability will be demonstrated in two steps prior to commencement of full-scale operation:

#### Clean Soils Demonstration:

The LTVS will be set up on site completely as it would be for actual contaminated soils treatment. The operator will demonstrate the mechanical operation of LTVS, complete in all respects, while operating at design parameters with clean borrow soil from offsite for a period of 48 hours. The operator will add sufficient water to the soils to arrive at a moisture range of 20 to 30 percent,

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to be representative of the soils at the site. After successful demonstration, the clean soils will be stockpiled for use as backfill to replace metals-contaminated soils which must be disposed of off site.

#### Contaminated Soils Demonstration:

After successful demonstration of mechanical operation with clean soils, the operator will then operate the system for a limited period, using contaminated site soils, to demonstrate satisfactory operation of the LTVS, including the removal of organic compounds from soils to acceptable concentrations and compliance with air emission control requirements. Approximately 500 cy of contaminated soils from the vicinity of HSB-2 and PSB-6 will be used for this demonstration, as representative of the worst-case concentrations of most organic contaminants likely to be encountered in any portion of the site.

## 4.2.7.3 Air Emissions Control

The LTVS will contain a unit process or processes to remove the organic contaminants from the exhaust gas to meet EPA and the State of Georgia requirements for emission of the detected contaminants listed in Table 3.1. Usually this consists of an afterburner, which operates with a gas residence time of at least 0.5 second at a minimum temperature of 1800°F. The LTVS provides additional emission control by incorporation of an induced draft fan that maintains a negative pressure at all times throughout the system in order to minimize fugitive emissions. Particulate emission controls are provided by use of a baghouse, cyclone, or electrostatic precipitator. Permitting and air monitoring conditions cannot be determined until after a system is selected and its configuration, emission control equipment, and throughput are known. An air emission sampling plan will be developed as part of the permitting process, after selection of a system.

### 4.2.7.4 <u>Treatment</u>:

Contaminated soils will be treated and then temporarily stored in the post-treatment storage area until analytical results indicate that the soils meet the criteria for placement back into the excavation area.

## 4.2.7.5 Post-treatment:

## Sampling:

Analyses for volatile and semi-volatile organic compounds and metals will be performed at the frequency indicated by Table 5.1 on a randomly obtained discrete sample. Soils will be tested and certified as clean if they are found to contain less than the maximum allowable contaminant levels stated in paragraph 4.2.7.2. Higher contaminant levels will result in retreatment of the soil batch from which the sample was taken.

#### **Retreatment:**

The operator will reprocess, retreat and reanalyze soils which do not meet the criteria for organic compounds to be backfilled into the excavation area. The reprocessing and retreating of these soils or sediments will be continued repetitively until analytical results indicate the residual organic compounds present in the soils or sediments are below criteria established for onsite use as backfill.

#### Segregation:

Soils requiring retreatment will be segregated from treated soils. The quantity requiring retreatment will be reported and subtracted from the daily production rate when calculating treatment volumes for the day to prevent double-accounting. Soils which exceed inorganic PCTs will be segregated for off-site disposal.

#### 4.2.8 Disposal of Clean Treated Soils and Sediments

Soils which have been adequately treated (RCRA Appendix VIII constituents nondetectable and all other contaminant concentrations below PCTs per paragraph 4.2.7.2) will be backfilled into the completed areas of the excavation. Backfilled soils will be protected from contamination by unexcavated soils by maintaining a 20-foot buffer zone between clean backfill material and soils requiring further excavation. Excess quantities of clean fill can be placed temporarily on areas where only surface soils required excavation and no deeper contamination exists.

## 4.2.9 Disposal of Metals-Contaminated Soils

Soils contaminated with inorganics in excess of PCTs will be transported for off-site disposal in a licensed solid- or hazardous-waste facility. Characterization of the soils will be made pending the results of TCLP analyses.

### 4.3 GROUNDWATER REMEDIATION

#### 4.3.1 GROUNDWATER MONITORING

An expanded groundwater monitoring program must be performed both to determine the westward limit of existing groundwater contamination and to monitor the effectiveness of groundwater remediation. Groundwater monitoring will be performed per the Groundwater Monitoring Plan, which is included in this plan as Appendix B.

## 4.3.2 RECOVERY SYSTEM DESIGN

Groundwater flow past the site is estimated based on the hydraulic conductivity of the shallow aquifer, as determined by slug testing, and the average groundwater gradient,

Well Number	NORTHING	EASTING	Top of Casing Elevation (ft-msl)	Depth to Water 3/92 (ft toc)	Groundwater Elevation 3/92 (msl)	
1 1 1	734794.34	816370.12	38.51	12.94	25.57	
HW-2	734786.58	816363.02	38.02	11.12	26.90	
IMW-3	734719.25	816011.95	29.85	. 7.24	22.61	
IMW-4	734718.68	816018.22	30.49	6.51	23.98	
1HW-5	734494.62	816074.63	32.02	8.05	23.97	
HW-6	734497.34	816067.77	31.60	6.15	25.45	
IHW-7	734579.79	816022.48	29.95	4.70	25.25	
IMW-8	734779.81	816009.36	27.59	7.32	20.27	
MW-9	734790.68	816129.62	34.50	8.10	26.40	

Table 4.1 Summary of Groundwater Elevations, March 1992, Hunter AAFTA

Notes: ft-msl = feet mean sea level ft toc = feet below the top of casing

based on measured static water levels in the existing monitoring wells (Table 4.1) and the surveyed ditch-bottom elevations (see Figure 1-5 in Appendix B). Groundwater flow calculations presented in Appendix D predict a groundwater flow velocity of 7 x 10<sup>-5</sup> feet per minute. Assuming a soil porosity of 0.30, a conservative 50-foot thickness for the contaminated groundwater layer, and a 400-foot plume width (the distance between the ditch outfalls), the flow rate in the contaminated zone is estimated at less than 5 gpm. This is the minimum recovery rate required to capture all contaminated flows passing through the site, with no recovery of any plume which might be present to the west of the ditch confluence. The actual recovery system flow rate will be determined after the westward extent of the groundwater benzene contamination has been determined by implementing the monitoring plan. A preliminary assumption of a recovery system flow rate of 25 gpm is made for this closure plan until further monitoring can be performed. This assumption is made to account for uncontaminated flows from the north and south, and increased infiltration after precipitation. The recovery system is presently assumed to consist of two horizontal wells, paralleling the two drainage ditches to capture surface seepage before it can enter the ditches, and one 50-foot recovery well near the ditches' confluence to recover contaminated water from the deeper strata.

## **4.3.3 GROUNDWATER TREATMENT**

Recovered groundwater will be treated by air stripping to remove benzene contamination, which has been detected at concentrations up to 660  $\mu$ g/L. Air stripping passes an air stream over the surface of the water to be treated, removing volatiles with the air stream. This closure plan incorporates a vertical packed tower where contaminated water flows downward over the packing media and air is blown upward counter to the direction of water flow. Removal of benzene and other volatile petroleum hydrocarbons has been well established over recent years of experience remediating gasoline releases from underground storage tanks. Depending upon the treatment rate, and contaminant concentrations, air emission permits are sometimes required. The relatively low concentrations encountered at this site (660  $\mu$ g/L maximum, with perhaps 50  $\mu$ g/L as an average treatment influent concentration) will result in low daily mass emission rates for benzene (0.2 pounds per day at 660  $\mu$ g/L and 25 gpm). The AIRSTRIP model calculations are presented in Appendix C. In spite of the low estimated emissions, benzene is a toxic air pollutant and GDNR may require best-available-control-technology (BACT), i.e. vapor-phase carbon adsorption or off-gas combustion. An air emission permit-to-construct will be required prior to commencement of groundwater treatment.

Operation and maintenance (O&M) will include routine repair of pumps and ancillary equipment, influent and effluent quality monitoring, and routine adjustment and checking by a qualified operator. Average life for pumps, blowers, and packing is estimated at 5 to 10 years. Since the extent of groundwater contamination is not yet known, the duration of treatment cannot be estimated, but it is highly likely to be less than 5 years. It is assumed that acid washing of the media will be required every 6 months. Treatment system influent and effluent will be sampled and analyzed monthly for the duration of the remediation, with daily samples required during system startup (approximately 2 weeks). All water samples will be analyzed by the methods and for the parameters specified in Appendix B to monitor the performance of the treatment system and determine when cessation of treatment is appropriate. If, during the course of remediation, it can be established that only benzene has been encountered at levels of concern, a request will be made to GDNR to reduce the number of analytical parameters for routine monitoring to volatiles only, with an annual test for the full range of priority pollutants. When groundwater treatment is completed, the system will be decontaminated, dismantled, and disposed of as nonhazardous scrap.

# 4.3.4 DISPOSAL OF TREATED GROUNDWATER

Disposal of treated groundwater will be provided by a percolation pond located on the north side of the training area, adjacent to the soils treatment area.

## 4.4 EQUIPMENT CONTROL AND DECONTAMINATION

All equipment which operates in the closure area after excavation begins and before an area is certified as having all contaminated soils removed, will be considered to be contaminated and will not leave the excavation area without decontamination. Decontamination will be performed by steam- or high-pressure water-cleaning to remove all adhering soils. A reinforced-concrete decontamination pad will be constructed at the northern boundary of the exclusion zone, where it adjoins the treatment zone (see Figure 4-1). The pad will be designed to collect all water and sediments in a sump and pump the contaminated water to a storage tank for off-site disposal. Sediments will be added to the contaminated soils for treatment in the LTVS. At the conclusion of closure activities, the pad surface and collection sump will be pressure-washed and the pad will then be demolished and disposed of in the on-site construction debris landfill.

#### 4.5 SITE RESTORATION

After all treatment and backfilling of soils has been completed, the site soils will be regraded to within 1 foot of the contours existing prior to remediation. The upper 6 inches of the treated and replaced soils will be mixed with peat to create a suitable topsoil and the area will be seeded with quick-rooting grass species. Erosion control measures on the area side slopes and drainage ditches will be maintained until sufficient growth is achieved to prevent erosion. Areas damaged by erosion will be repaired and reseeded as necessary.

## 5.0 ENVIRONMENTAL MONITORING

## 5.1 CONFIRMATORY SOIL SAMPLING AND ANALYSIS

Sampling, analysis, and analytical quality assurance/quality control (QA/QC) will be in accordance with the existing Chemical Data Acquisition Plan for Fort Stewart Fire Training Areas, Savannah, Georgia (ESE, 1989), except as follows (The number of samples anticipated is shown in Table 5.1.):

#### 5.1.1 SOIL SAMPLING

#### 5.1.1.1 Sampling and Sample Custody Procedures

Soil samples to be taken are environmental (dilute) rather than hazardous (or concentrated) samples. Grab sampling techniques will be used to collect environmental samples.

Quality Control (QC) samples (sent to the AE lab) consisting of duplicates and field controls will be taken in the same sample containers and handled in the same manner as the field samples. The duplicate sample ratio is one in ten. Soil sample duplicates are actually split samples taken from one sampling location. Travel blanks will be containers filled with deionized water, transported to the site and handled like a sample. Deionized water will be added to compensate for any loss. Sampling blanks will be made with reagent water which is passed through the sampling equipment and transferred to sample containers.

Quality Assurance (QA) samples (sent to the USACE MRD lab) will consist of duplicates and field controls for the appropriate matrix type (i.e., soil) taken in the same sample containers and handled in the same manner as the field samples. The duplicate sample ratio is one in ten. As with the QC sample, the soil sample duplicates are actually split samples taken from one sample location.

B:HTR-CLOS.V.1 July 22, 1993

#### TABLE 5.1

# TYPE, LOCATION, METHOD OF ANALYSIS, AND NUMBER OF SOIL SAMPLES TO BE COLLECTED FOR ANALYSIS FOR THE HUNTER AAFTA CLOSURE

	EPA Method	Estimated Total Quantity	Total No. of Field	No. o Samp		No. o Samp	
Туре	(SW-846)	(CY/SF)	Samples	EB	DUP	EB	FI
UNTREATED SOILS AND SEDIMENTS "Woods Line" Delineation Samples Semi-volatiles	8270	NA	12	1	1	1	×
Training Pad Cover and Surroundir Area Characterization Soil Samp Metals Semí-volatiles		300 CY	3 3	0	0 0	0 0	
Training Pad and Surrounding Area Confirmatory Soil Samples Metals VOCs Semi-volatiles	(1) 8240 8270		18 18 18	2 2 2	2 2 2	2 2 2	
Ground Surface Excavation Confirmatory Soil Samples Metals VOCs Semi-volatiles	(1) 8240 8270		120 120 120	12 12 12	12 12 12	12 12 12	1 1 1
Deeper Excavation Perimeter Confirmatory Samples Metals VOCs Semi-volatiles	(1) 8240 8270		24 24 24	2 2 2	2 2 2	2 2 2	
THERMALLY TREATED SOILS AND SEDIM TCLP Metals VOCs Semivolatiles	ENTS (*) TCLP 8240 8270	10,000	33 33 33	3 3 3	3 3 3	3 3 3	
DFFSITE BORROW SOILS (**) Total Metals VOCs Pesticides/PCBs Semivolatiles	(1) 8240 8080 8270	300	3 3 3 3	0 0 0 0	0 0 0	0 0 0 0	*

\*Frequency is 1 per 300 CY at a minimum of once per LTVS operating day. \*\*Frequency is 1 per 100 CY per soil type per source.

Notes:

CY = cubic yard. EB = equipment blank. FD = field duplicate. SF = square feet.

(1) Metals shall consist of arsenic (SW 7060), chromium, (SW 6010), lead (SW 7421), mercury (SW7470/7471), nickel (SW6010), zinc (SW 6010), barium (SW 6010), and cadmium (SW 6010).

Sample chain-of-custody procedures and packaging guidelines will be followed explicitly. The QA samples will be sent to a laboratory selected by the USACE.

## 5.1.1.2 <u>Sample Location</u>

Samples will be collected in the locations specified in Section 4.2 and in Table 5.1. The precise location of samples will be left to the discretion of the Site Manager.

#### 5.1.1.3 Sampling Procedures

Grab samples will be collected using a stainless steel hand auger. Each piece of stainless steel soil sampling equipment will be pre-cleaned before use to minimize potential cross-contamination. Pre-cleaning will consist of steam cleaning or the following procedure: (1) remove gross contamination from the auger using scrapers, (2) wash the auger with a brush in a bucket filled with an Alconox soap solution, (3) rinse in a second bucket containing tap water and a brush, (4) spray the auger with methanol, (5) rinse with deionized water, and (6) air dry. Sampling will follow the procedure outlined below.

- a. <u>Collect Sample</u> The samples will be collected with the hand auger from a depth of approximately six inches. Auguring will proceed until sufficient soil has been collected to satisfy sampling requirement. Soil samples for volatiles analysis will not be mixed; these samples will be duplicates. QA and QC samples for volatiles analysis will be taken in the same manner. The sampler will check that a Teflon liner is present in the cap and secure the cap tightly. After each sample has been collected, all of the sampling equipment, hand auger, mixing bowl, and spoon, will be cleaned to prevent cross contamination.
- b. <u>Label Sample</u> Once the sample is collected, each container will be labeled with the following data: sample identification number, project number, date, time,

analysis requested, preservation, and person sampling. The label will be covered with transparent plastic tape. Sample containers will be sealed with custody tape. Sample identification information will be recorded in the bound site log book and complete all chain-of-custody documents. The bound field note book will have prenumbered pages and entries will be made in indelible ink.

c. <u>Custody, Handling and Shipping</u> - The properly labeled and sealed containers will be sealed in a plastic "Ziplock" type bag. Approximately three inches of inert cushioning and absorbing material (i.e. vermiculite) will be placed in the bottom of the cooler. Sample bags will be arranged in the metal cooler so that they do not touch. The remaining space will be packed with ice (also in bags) and styrofoam packing beads, bubble wrap or vermiculite. Samples should be packed so as to maintain a temperature of 4°C. Chain-of-custody and request for analysis documents will be sealed in air-tight plastic bags and taped to the inside of the cooler's lid. "This side up" and "Fragile" labels will be placed on the cooler, and it's drain will be taped shut. The lid of the container should be taped shut with custody seals. Samples will be shipped on the day they are collected from the site directly to the laboratory by overnight courier. The laboratory will be notified by phone of the sample shipment.

#### 5.1.2 Sediment Sampling

Preliminary samples will be taken at 200-foot intervals in the north and south ditches, beginning at a point 100 feet west of PSS-2 and PSS-4 (450 feet west of the edges of the culvert outfall concrete aprons). All sediment samples will be taken using a stainless steel Oakfield sampler. The sampler will be advanced approximately 6 inches into the sediment, between the submerged edge and the deepest portion of the ditch at the locations described above.

The sample sequence will be such that stations farthest downstream will be sampled first to prevent any upstream sediment from compromising the downstream sample quality. All sample locations will be approached from the downstream side for the same reason.

## 5.2 GROUNDWATER SAMPLING AND ANALYSIS

The monitoring of groundwater elevations and contaminant concentrations within and adjacent to the closure area is necessary to identify the extent of groundwater contamination and its rate of migration, to determine the sizing and placement of the elements of the groundwater recovery system, and to gauge the effectiveness of the closure in protecting groundwater resources. All elements of groundwater monitoring for this closure are presented in the Groundwater Monitoring Plan, which is Appendix B to this closure plan.

## 6.0 RECORD KEEPING AND SCHEDULE

## 6.1 <u>RECORDS AND REPORTS</u>

## 6.1.1 RECORDS

Daily reports will be kept in a logbook at the site during closure. The logbook will be permanently bound with numbered pages. Copies of log pages may be made for inclusion in reports, but the current original log will remain at the site until completion of closure. As logbooks are filled and a new log is started, the completed books will be stored either in the field office at the closure site or at the Fort Stewart Environmental Affairs Office. The daily log entry will include, as a minimum, the following:

- o The current excavation area (eg. south, west, or north sector),
- The quantity excavated that day (truckload volumes or calculated volume from an excavation quantity survey),
- o The cumulative quantity excavated from project start,
- o Hours of operation and times of shift changes,
- o Names of equipment operators,
- o Weather conditions,
- o Confirmatory soil samples and treated soil samples,
  - locations (relative site coordinates for confirmatory samples),
  - sample identification numbers,
  - chain-of-custody sheet reference (actual custody sheets will be kept and filed in accordance with the CDAP),
- o Waste shipments sent off-site with manifest numbers, as applicable,
- o Reports of accidents, near misses, or other events with notable site safety implications.

## 6.1.2 CLOSURE CERTIFICATION REPORT

A closure certification report will be produced including a summary of closure activities, copies of analytical results and QC reports, and stating whether all closure goals have been met for soils and groundwater.

6-1

## 6.2 <u>SCHEDULE OF CLOSURE</u>

The following schedule of closure has been based upon the model timetable presented in 40 CFR 265.113 and EPA's "Clean Closure Guidance Manual for Hazardous Waste Management Units," except that time intervals and events has been inserted between agency approval and commencement of physical closure to allow for conversion of the approved closure plan to contract plans and specifications and the advertisement and award of a closure construction contract. The schedule is shown in Table 6.1.

<u>Time</u>	Event
Day 1	Closure plan submitted to GDNR
30	GDNR requests public comments
90	GDNR approves, modifies, or disapproves plan
120	Army submits revised plan, if necessary
180	GDNR approves or modifies closure plan; clean closure begins
210	Army develops contract plans and specifications from the approved closure plan
270	Closure construction contract advertisement period begins
315	Closure construction contract is awarded and contractor begins mobilization
360 [	Closure construction begins
540 [	Clean closure is completed in accordance with approved plan or post-closure begins
600 [	Closure is certified

Table 6.1: Schedule for Clean Closure of Hunter Army Airfield Fire Training Area

APPENDIX A

TOPOGRAPHIC SURVEY

REPLACE THIS PAGE WITH SCANNED MAP!

APPENDIX B

.

GROUNDWATER MONITORING PLAN

## GROUNDWATER MONITORING PLAN FOR HUNTER ARMY AIRFIELD FIRE TRAINING AREA (AAFTA) FORT STEWART, GEORGIA

Prepared for:

## UNITED STATES ARMY CORP OF ENGINEERS (USAEC) Kansas City, Missouri

Prepared by:

ENVIRONMENTAL SCIENCE & ENGINEERS, INC. Gainesville, Florida

ESE No. 3912015G

July 1993

Note: Wherever "Appendices" are referred to in the text of this document, only the appendices to this Groundwater Monitoring Plan are intended and not those of overall Closure Plan.

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# APPENDIX C--MISCELLANEOUS FORMS

Note:

Wherever "Appendices" are referred to in the text of this document, only the appendices to this Groundwater Monitoring Plan are intended and not those of overall Closure Plan.

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## **1.0 SITE SPECIFIC CONDITIONS**

This groundwater monitoring plan describes protocol for groundwater monitoring at the Fort Stewart, Hunter Army Airfield Fire Training Area (AAFTA) as required by the State of Georgia Department of Natural Resources, Environmental Protection Division. This report includes the groundwater sampling and analytical methodologies used to determine the impact of the facility on the groundwater in the vicinity of Hunter AAFTA. Included in this plan are:

- 1. A brief physical description of the site including geology and hydrogeology;
- 2. A brief discussion of a previous groundwater analytical sampling event;
- 3. Selected monitor well network description;
- 4. Groundwater sampling methodology, parameter list, and sampling frequencies;
- 5. Chain of Custody and shipping procedures;
- 5. Groundwater analytical procedures;
- 6. Groundwater data analysis and reporting procedures; and
- 7. Corrective action program.

This groundwater monitoring plan is divided into three sections. Section 1.0 presents the sitespecific conditions at the Hunter AAFTA and presents a description of the groundwater monitoring system. Section 2.0 presents the groundwater monitoring protocol and sampling procedures including Quality Assurance (QA) procedures. Section 3.0 presents groundwater analytical data evaluation and reporting protocol including corrective measure procedures.

This groundwater monitoring plan meets RCRA and State of Georgia Department of Natural Resources; Environmental Protection Division (Chapter 391-3-4-.14 of the Solid Waste Management Rules) closure and monitoring requirements for solid waste management unit (SWMU). The sampling procedures presented in this document are in accordance with Environmental Protection Agency (EPA) Region IV Engineering Support Branch Standard Operating Procedures and QA Manual, dated February 1, 1991.

1-1
## **1.1 SITE DESCRIPTION**

The following subsections summarize site conditions at the Hunter AAFTA. This summary includes a brief description of the site location, site specific subsurface and surface conditions, and a description of the groundwater monitoring system.

## **1.1.1 SITE CONDITIONS**

Hunter Army Airfield is located on 5,400 acres of land in Chatham County, Georgia, just southwest of Savannah (Figures 1-1 and 1-2). The airfield is bounded on the north by lightly populated areas, on the east and south by residential and light commercial areas, and on the west by the Little Ogeechee River. The Hunter AAFTA consists of a 6,400-square foot (ft<sup>2</sup>) concrete pad, located on the northwest portion of the airfield, approximately 800 feet (ft) north-northwest of the control tower (Figure 1-3).

The study area is located within the Southern Atlantic Coastal Plain Physiographic Province. Most of the land within Fort Stewart is flat, planted pine woods interfingered with freshwater swamps and tidal creeks with elevations ranging from 10 to nearly 100 feet above mean sea level (ft-msl). However, the northwestern portion of the reservation is characterized by rolling hills that rise to an elevation of approximately 180 ft-msl.

The ground surface at the Hunter AAFTA, at an elevation of approximately 30 ft, slopes gently to the west and drains toward a small canal. The canal runs west approximately 400 ft then southeast approximately 1,500 ft, where it empties into the Little Ogeechee River tidal floodplain.

### **1.1.2 SITE HISTORY AND FEATURES**

The Hunter AAFTA consists of a bermed, soil-covered concrete pad with a simulated aircraft constructed from a used steel storage tank. The fire training pad is located on a grassy slope approximately 2200 feet north of the center of the airfield's east-west runway. The area was used for training of the airfield's firefighters from its construction until 1992.

Fuel for training fires is provided by underground piping from an above-ground fuel storage tank located approximately 100 feet north of the training pad. Fuels are mostly water-contaminated jet

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fuel (JP-4) and diesel fuel; however, waste oils have reportedly also been used (USAEHA, 1987). During training exercises, jet fuel (JP-4) was pumped onto the surfaces of the simulated aircraft and ignited. Firefighting trainees extinguished the fire with water or foam. The water was contained by the berms around the fire training pad and sump. Some of the water (and fuel) occasionally ran over the concrete berms onto the adjacent soil, and some may have been splashed over the berms by the spray from the firefighting hoses. The AAFTA has apparently been used for fire training in the interim between 1990 and 1992, although the fire department personnel interviewed had no first-hand knowledge of such use.

## 1.2 CLIMATE

The study area has a moist and temperate climate year round. Average temperatures range from 52 degrees Fahrenheit (°F) in winter to 80°F in summer. Average annual rainfall is approximately 48 inches (Headquarters, 24<sup>th</sup> Infantry Division, 1977), 60 percent of which usually falls during the period April through September. Prolonged drought is rare in the study area.

Climatic data for the period July through December 1991 was presented in Appendix A of the Significance of Contamination Report. The data include the minimum and maximum temperature, daily mean temperature, total precipitation water equivalent, and maximum windspeed and direction.

### 1.3 <u>REGIONAL GEOLOGY</u>

The coastal plain region of Georgia is underlain by a thick wedge of unconsolidated and semiconsolidated sediments that range in age from Recent to Cretaceous (Herrick and Vorhis, 1963). This sedimentary wedge thickens and slopes toward the east with a dip of less than 1 degree (°). Underlying these sediments in the Savannah area is a basement of crystalline igneous rocks of the Piedmont Formation, and various metamorphic and consolidated sedimentary rocks of Triassic to Precambrian age.

From youngest to oldest, the Recent and Pleistocene deposits consist of discontinuous units of sand, silt, and clay. These units are undifferentiated in the site region, with thicknesses of

approximately 60 feet. Underlying the Pleistocene deposits is the Duplin Marl (Upper Miocene), consisting of green, stiff, phosphatic and calcareous sandy clay. The Duplin Marl is approximately 60 feet thick at the site region. The Hawthorn Formation (Middle Miocene) consists of green to buff phosphatic sandy clay and dolomitic limestone. The Hawthorn Formation is approximately 50 feet thick in the site region. The Tampa Limestone equivalent underlies the Hawthorn Formation and is of Lower Miocene age. The Tampa Limestone is approximately 10 feet thick and is dolomitic with seams of green sandy clay at its base. Underlying the Tampa Limestone is a thick sequence of limestone units ( The Floridan Aquifer) which include an undifferentiated Oligocene unit, the Ocala Limestone, the gosport sand, and the lisbon formation. These units extend to approximately 850 feet below the ground surface in the vicinity of the site. Figure 1-4 is a composite geologic column for the Savannah area. Deep borings performed during previous investigations [ESE, 1982; U.S. Army Environmental Hygiene Agency (USAEHA), 1987, Hunter/ESE 1990, ESE 1993a] at or in the vicinity of Hunter AAFTA indicate that the site is underlain predominantly by sand, silty-sand, and some clayey sand deposits to a depth of at least 50 feet below land surface (ft-bls). Shallow borings performed during previous investigations (USAEHA, 1987; ESE, 1990; ESE 1993a) at the Hunter AAFTA indicate that the site is underlain predominantly by fine-grained sand deposits to a depth of at least 10 ft.

### 1.4 HYDROGEOLOGY

The two principal aquifer systems in the Georgia coastal plain are the artesian Floridan aquifer and the overlying (younger) surficial aquifer (water-table aquifer). The Floridan aquifer is comprised of Middle-Upper Eocene (Ocala Group) and Oligocene (undifferentiated) limestones. The overlying Lower-Miocene Tampa Limestone, which may include beds of sandy clay, may also form part of the Floridan aquifer. In the Savannah area, the top of the Floridan aquifer is approximately 150 to 200 ft-bls.

The Floridan aquifer is the major source of groundwater for the Coastal Plain of Georgia and adjoining states (Krause and Gregg, 1972). The Floridan aquifer in Georgia provides the

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majority of water for industrial and domestic use [500 million gallons per day (mgd) statewide in 1978].

The Middle and Upper-Miocene Hawthorn Group and Duplin Marl, comprised of clay with occasional limestone beds, forms a confining unit that hydraulically separates the Floridan aquifer from the overlying surficial aquifer.

The Pleistocene to Recent deposits above the Miocene deposits consist of discontinuous units of sand, silt, and clay. The surficial aquifer is comprised of discontinuous beds and lenses of sand within these deposits. The depth to the water table in the Savannah area is approximately 3 to 10 ft-bls. The vertical extent of the surficial aquifer is not known, though Kundell (1978) reports that the aquifer may be up to 120-ft thick in the study area. Approximately 5-feet of soil fill was brought to the Hunter Army Airfield to raise the airfield and fire training pad above the level swamp which existed in the area prior to the construction of the Airfield.

There is no record of extended usage of the surficial aquifer in the study area; however, statewide usage amounted to 500,000 gallons per day (gpd) in 1978.

## 1.5 SUMMARY OF AQUIFER CHARACTERISTICS

Groundwater levels were monitored continuously from July through December 1991 with a Telog<sup>®</sup> logging device which was installed at HMW-6 to take hourly records of the water level fluctuations. The water level records were retrieved from the data logger once a month while water level data from each well were manually collected once a month by ESE personnel. July, August, and September generally have the most precipitation at the Hunter AAFTA, and October, November, and December are generally dry (Hunter/ESE, 1989). Rainfall data for the 6-month period were received from the Hunter Army Airfield weather station for comparison with groundwater fluctuations.

The Telog<sup>®</sup> data, presented in the Significance of Contamination Report (ESE, 1993) shows a slight cyclic fluctuation recurring less than 24 hours between crests. These fluctuations, possibly

due to tidal influences, are minor [approximately 0.2 foot per day (ft/day)], and have little effect on the overall groundwater gradient. The data also show sudden water-level increases over short periods of time, followed by gradual decreases. These fluctuations appear related to rainfall events that occur periodically at the site.

The maximum water height above the Telog<sup>®</sup> pressure transducer in HMW-6 was 9.42 ft measured July 21, 1991; the lowest height of water was 5.63 ft measured December 19, 1991. The maximum groundwater fluctuation as determined by the Telog<sup>®</sup> data was 3.79 ft.

## 1.5.1 HYDRAULIC GRADIENT IN MARCH 1992

Water-table elevations for the March 1992 field effort were calculated using the new survey data for the monitor wells. The data are summarized in Table 1-1. A water-table contour map for the upper part of the surficial aquifer at Hunter AAFTA is presented in Figure 1-5. A similar map for the deeper portion of the aquifer is presented in Figure 1-6. The maps show that groundwater flow in both the upper and deeper zones of the surficial aquifer is to the northwest, which is consistent with the previous site reports.

## **1.5.2 GROUNDWATER FLOW DIRECTION AND VELOCITY**

The results of the hydrogeologic evaluation indicate the water table gradient is generally toward the northwest at the Hunter AAFTA site. The gradient was fairly constant to the northwest in both the deep and shallow zones, with the shallow zone showing slightly greater seasonal fluctuations.

Based on the data from HMW-2, HMW-4, and HMW-6, the average shallow groundwater gradient is approximately 0.015 feet per foot (ft/ft) to the northwest. Assuming an aquifer porosity of 30 percent and a hydraulic conductivity of 0.0013 ft/min (based on the slug tests) the linear groundwater flow velocity is estimated to be 35.9 feet per year (ft/yr). The formulae and calculations are included in Appendix E of the Significance of Contamination Report (ESE, 1993a).

Table 1-1. Summary of Groundwater Elevations, March 1992, Hunter AAFTA.

Well Number	NORTHING	EASTING	Top of Casing Elevation (ft-msl)	Depth to Water 3/92 (ft toc)	Groundwater Elevation 3/92 (msl)
HMW-1	734794.34	816370.12	38.51	12.94	25.57
HMW-2	734786.58	816363.02	38.02	11.12	26.90
HMW-3	734719.25	816011.95	29.85	7.24	22.61
HMW-4	734718.68	816018.22	30.49	6.51	23.98
HMW-5	734494.62	816074.63	32.02	8.05	23.97
HMW-6	734497.34	816067.77	31.60	6.15	25.45
HMW-7	734579.79	816022.48	29.95	4.70	25.25
HMW-8	734779.81	816009.36	27.59	7.32	20.27
HMW-9	734790.68	816129.62	34.50	8.10	26,40

Notes: ft-msl = feet mean sea level

ft toc = feet below the top of casing





## 1.5.3 SUBSURFACE LITHOLOGY

The subsurface soil conditions encountered during this investigation and the previous investigation (Hunter/ESE, 1990) may be categorized into two general strata based on geologic and engineering characteristics. Stratum I soils extend from the surface to approximately 35 ft-bls and consist of gray to brown, medium to coarse-grained, loose to medium-dense silty sand, with interbedded layers of clayey sand and poorly graded sand. The sand contains approximately 6 to 13 weight-percent particles finer than No. 200 mesh. The fines are generally nonplastic, and the soil is classified as silty sand according to Unified Soil Classification System (USCS). Moisture contents in the Stratum I soils ranged from 36 to 40 percent. For a typical clean, poorly graded sand as found in the stratum, the estimated conductivity between 1 x  $10^{-2}$  and 1 x  $10^{-4}$  cm/sec (Peck, Hanson, and Thornburn, 1974). Slug testing confirmed a conductivity of 6 x  $10^{-4}$  cm/sec (1.2 x  $10^{-3}$  ft/min).

Stratum II soils begin at approximately 35 ft-bls and continue to an unknown depth; the soils consist of gray, fine to medium-grained, loose to medium-dense, poorly graded sand. The sand contains approximately 2 to 3 weight-percent particles finer than No. 200 mesh. The soil is classified as poorly graded sand (SP) according to the USCS. Moisture contents in the Stratum II soils ranged from 32 to 44 percent. For a typical loose to medium-dense, poorly graded sand as found in this stratum, the estimated conductivity is between  $1 \times 10^{-2}$  and  $1 \times 10^{-4}$  cm/sec (Peck, Hanson, and Thornburn, 1974). Slug testing confirmed a conductivity of  $9 \times 10^{-4}$  cm/sec (1.8 x  $10^{-3}$  ft/min). Both Stratum I and Stratum II are of undifferentiated Pleistocene to Recent age.

## **1.6 SUMMARY OF PREVIOUS GROUNDWATER ANALYTICAL RESULTS**

The concentrations of arsenic, chromium, and selenium detected in a 1990 groundwater sample from a shallow downgradient well (HMW-6) exceed Federal and State of Georgia MCLs. Lead levels detected in the 1990 samples from the same well, as well as shallow downgradient well HMW-4 are above the EPA action level for lead. The concentrations of arsenic, barium, chromium, and lead detected in the shallow upgradient well (HMW-2) also exceed or are equivalent to their respective PCTs.

Benzene was detected above its MCL in several wells [HMW-3 (1990), HMW-4 (1992), HMW-6 (1990 and 1992), HMW-7 (1992), and HMW-9 (1992)]. Fig. 1-7 presents benzene concentrations detected in groundwater samples during the 1992 field effort. The lateral extent of benzene contamination was not delineated during this field effort. Also, vinyl chloride was detected above its MCL in the 1992 sample from HMW-6. The only other chemicals measured in groundwater above PCTs were three PAHs, which were detected in the 1990 sample from HMW-6 PAHs were not detected above PCTs in any of the wells during the 1992 field effort (ESE, 1993a).

### 1.7 PROPOSED MONITORING NETWORK

The groundwater monitoring network at the Hunter AAFTA consists of 2 (HMW-1(deep) and HMW-2(shallow)) upgradient and 7 downgradient monitor wells. Monitor wells HMW-3 and HMW-5 were constructed downgradient of the fire training pad and are screened at an approximate depth of 49 feet below the ground surface (STRATUM II). Monitor wells HMW-4, HMW-6, HMW-7, HMW-8, and HMW-9 were constructed downgradient of the fire training pad and were all screened at an approximate depth of 3 to 13 feet below the ground surface, except for HMW-9 which is screened from 5 to 15 feet below the ground surface (STRATUM I). Well construction details for these existing wells are summarized in Table 1-2. Boring logs and well construction details for all the wells existing at the site are included in Appendix **B** of the Operations and Maintenance Plan.

Additionally, the construction of at least two wells may be needed to determine the horizontal extent of contamination. The locations of these new wells will be determined based on the results of field screening activities to be implemented as part of this groundwater monitoring plan. A description of the field screening activities and well construction details are provided in Section 2 of this groundwater monitoring plan. The locations of the existing and preliminary locations of proposed monitor wells are shown in Figure 1-8.



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Table  $1\!-\!2$  Monitor Well Completion and Location Survey Summary, Hunter AAFTA

Well	2 1		Top of Casing Elevation	Boring Diameter	Boring Depth	Sandpack Interval	Bentonite Seal	Screen Interval	Well Diameter	Grout Interval
Number	Northing	Easting	(ft-msl)	(inches)	(ft bls)	(ft bls)	(ft bls)	(ft bls)	(inches)	(ft bls)
1-WMH	734794.34	816370.12	38.51	10.25	50.00	35.0 - 50.0	33.0 - 35.0	38.0 - 48.0	2	0.0 - 33.0
НМИ-2	734786.58	816363-02	38.02	10.25	15.00	3.1 - 15.0	2.1 - 3.1	4.6 - 14.6	2	0.0 - 2.1
НММ-3	734719.25	816011.95	29.85	10.25	50.00	37.0 - 50.0	35.0 - 37.0	39.0 - 49.0	2	0.0 - 35.0
4-WMH	734718.68	816018.22	30.49	10.25	15.00	2.0 - 15.0	1.0 - 2.0	3.0 - 13.0	2	0.0 - 1.0
HMW-5	734494.62	816074.63	32.02	10.25	50.00	35.0 - 50.0	33.0 - 35.0	39.0 - 49.0	2	0.0 - 33.0
9-MMH	734497.34	816067.77	31.60	10.25	15.00	2.0 - 15.0	1.0 - 2.0	3.0 - 13.0	2	0.0 - 1.0
7-WMH	734579.79	816022.48	29.95	8	14.00	1.5 - 14.0	0.0 - 1.5	3.0 - 13.0	2	:
8-11MH	734779_81	816009.36	27.59	Ø	15.00	1.5 - 15.0	0.0 - 1.5	3.0 - 13.0	2	ł
6-MMH	734790.68	816129.62	34.50	8	15.00	3.0 - 15.0	0.5 - 3.0	5.0 - 15.0	2	ł
					2					

Note: ft bls = feet below land surface. ft-msl = feet mean sea level.

-- = bentonite seal installed to surface.

\*Boring diameter presented is the diameter of the boring in the sand pack zone only.

Source: ESE.



## 2.0 GROUNDWATER MONITORING

### 2.1 DETERMINATION OF THE EXTENT OF CONTAMINATION

The extent of groundwater contamination will be determined using temporary well points, a geoprobe groundwater sampling system, or other temporary groundwater sampling system. The system will be purged and groundwater samples will be taken from the sampling location and analyzed in the field using a Photovac portable Photoionization Detector (PID)/Gas Chromatograph (GC). The samples will be analyzed for benzene, toluene, ethylbenzene, and total xyllenes (BTEX).

QA samples will be collected at this site to verify the results of the groundwater screening. These samples will include VOA trip blanks, field equipment blanks, duplicate samples, and sample splits to be sent to the USACE Missouri River District Laboratory. A discussion of the QA samples is provided in section 2.5.6 of this groundwater monitoring plan.

The first groundwater sampling points will be located at the locations provided for the two additional wells at the site (See Figure 1.8). If these locations are found free of BTEX contamination, the wells will be installed at these locations. If contamination is found during the screening, an alternate location will be tested in the field. After two downgradient locations free of contamination are found, wells will be installed at these locations as per Section 2.2 of this monitoring plan.

### 2.2 ADDITIONAL MONITOR WELL CONSTRUCTION

The locations of two additional groundwater monitor wells will be determined based on the data presented in the Significance of Contamination Report (ESE, 1993a) and the results of the groundwater screening (Section 2.2). These locations will be downgradient of the plume and are expected to be free of contamination.

The monitor well boreholes will be drilled using 4-7/8-inch inside-diameter (ID) hollow-stem augers. Soil samples will be obtained from the well boreholes using a CME continuous split-

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barrel sampler or using a 1-7/8-inch ID split-spoon sampler in accordance with American Society for Testing and Materials (ASTM) D-1586. The soil samples obtained during the drilling process will be used to prepare lithologic logs of the boreholes. Copies of typical field lithologic logsheets and well construction detail logsheets are presented in Appendix C of the Closure Plan.

Groundwater monitor wells will be constructed inside the hollow-stem augers. The wells will be constructed of 2-inch-diameter Schedule 40 PVC casing with threaded joints and 10 ft of 0.010-inch slot well screen. The top of the well screen will be placed above the water table and approximately 3 or 5 ft-bls (depending upon the depth of the water table) to intercept phase-separated hydrocarbons (if present) on the water table.

The annular space surrounding the screen will be backfilled with clean, 20/30 silica sand to at least 1.5 ft above the top of the screen using a tremmie pipe. As the sand will fill the augers, the augers will be slowly lifted, allowing the sand to empty from the augers and flow into the annulus between the borehole and the well casing.

A seal consisting of Volclay<sup>®</sup> bentonite grout or other commercially acceptable pure bentonite grout will be placed above the sand pack. The grout was mixed according to the manufacturer's specifications and allowed to cure at least 24 hours prior to the installation of the antipercolation pad.

The monitor wells will be completed at the ground surface with 3-ft by 3-ft concrete antipercolation pads and protected abovegrade with locking steel protective casings. One-eighthinch-diameter drain holes will be drilled in the protective casings approximately 6 inches above the concrete pads. The tops of the pads will be sloped away from the protective casings to prevent water from ponding and infiltrating the joints between the protective casings and the pads. The tops of the wells will be capped inside the protective casings to keep airborne particulates and insects from entering the wells. The caps were vented to prevent air pressure

buildup in the wells due to water-level changes. The general well construction details are presented in Figure 2-1.

Three protective posts will be installed around each well. The posts will be 5-ft long by 2 1/2-inch-diameter steel pipe, and are set in concrete in 1 ft-deep by 4.5-inch-diameter holes. The pipes will be filled with concrete and painted to make them visible to traffic. State Plane Coordinates and elevations of the monitor wells at Hunter AAFTA will be measured during a control survey performed by a State of Georgia Registered Surveyor.

The monitor well development will be performed no sooner than 48 hours after well installation. The monitor wells will be developed using a surge block with alternate purging using a submersible pump, centrifugal pump fitted with a check valve, a bailer, or other purging equipment. The following procedures will be followed:

- 1. The initial sand and silt in the bottom of the well will be removed by pumping.
- 2. The surge block will be lowered to approximately 3 to 5 ft below the water table and gently moved up and down in 3-ft strokes.
- 3. The surge block will be removed from the well and sand and fines allowed to settle.
- 4. The well will be pumped to remove the sand and fines from the bottom and pH, temperature, and conductivity readings were taken.
- 5. Surging will be continued at a slightly lower level with an increase in the surging force.
- 6. The surging and pumping will be continued for a minimum of 4 hours and until the pH and conductivity stabilize and the sediment is no longer present in the discharge water.

Temperature, pH, and specific conductance will be monitored to ensure the water quality had stabilized. The total amount of water purged, pH, specific conductance, and temperature will be measured and recorded on well development forms in the field notebook. A copy of a Typical well development form is included in Appendix C of the Closure Plan.



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Each new well to be added to the groundwater monitoring system will be sampled for all EPA Appendix IX parameters to verify the wells were installed downgradient of the plume.

## 2.3 MAINTENANCE OF THE GROUNDWATER MONITORING NETWORK

Each well in the groundwater monitoring network will be maintained in operational condition for the full monitoring period. Each well will be inspected quarterly for tampering, surficial damage, silting, and screen damage. If damage or evidence of tampering of a well in the monitoring system is observed, the damage will be described in a letter addressed to the Fort Stewart Department of Environmental Health in care of Mr. Thomas Huston. The letter will include a description of the damage and the effect the damage will have on the operation of the well, and a plan to repair or replace the well.

If a monitor well is found dry during sampling, it should be noted in the field logbook and immediately reported to The Hunter Army Airfield Department of Environmental Health and the Georgia Department of Natural Resources, Environmental Protection Department (GDNREPD). GDNREPD will review the monitoring system to determine whether the well will be replaced with another groundwater monitoring well installed in a deeper aquifer. If levels of monitored constituents fall to background levels and remain at these levels for at least three years, the Ft. Stewart Department of Environmental Health may petition the GDNREPD to discontinue monitoring of this site. The SWMV permit is for a ten year period. A new permit must be obtained if the monitoring period exceeds ten years due to the continued detection of elevated dissolved constituents in the groundwater.

If it is necessary to replace an existing monitor well, the well will be abandoned using methods approved by the GDNREPD and the ACOE.

Typical groundwater monitoring costs are calculated based on a yearly rate escalated at a rate of 3 percent for the 10-year monitoring period. This cost includes projected O&M and sampling costs. ESE estimates groundwater monitoring costs, of approximately \$527,000/10 year

monitoring period. The cost for additional groundwater screening, installation of two wells, and sampling the groundwater for Appendix IX paramaters will be approximately \$15,000.

### 2.4 SAMPLING FREQUENCY AND ANALYTICAL PARAMETERS

The analytical parameters used for groundwater sampling was determined based on requirements for solid waste management unit closure monitoring as required in 40CFR 264 Subpart F and based on the findings reported in the Significance of Contamination Report (ESE, 1993a). Table 2-1 presents three groups of analytical parameters which will be sampled.

Group 1 includes general groundwater contamination detection parameters.

Group 2 includes site-specific contaminants and appropriate groundwater quality parameters. Included in this Group are parameters found above ambient water quality criteria detected in the March 1990 sampling event.

Group 3 parameters comprise VOCs included in the Clean Water Act Priority Pollutant List. These parameters must be analyzed annually.

Groundwater analytical samples will be obtained quarterly from each well of the groundwater monitoring network. One quarterly groundwater sample will be obtained during each of the 4 periods from January to March, April to June, July to September, and October to December. Subsequent samples will not be collected for at least 60 days following a previous sampling event. The quarterly groundwater samples obtained at each well will be analyzed for all parameters presented from Groups 1 and 2 in Table 2-1. Group 3 parameters will be analyzed annually.

After the initial four quarters of background sampling has been analyzed, The Georgia Environmental Protection Division will review the results to determine whether the frequency of sampling may be reduced and prepare a reduced parameters list to be analyzed.

### Table 2-1. Groundwater Monitoring Parameters

#### BACKGROUND WATER QUALITY PARAMETERS

Group 1

Arsenic Barium Cadmium Calcium Chloride Chromium Hardness as CaCO<sub>3</sub> Lead Mercury pН Selenium Silver Specific Conductance Total Organic Carbon Total Organic Halogen Total Dissolved Solids Total Suspended Solids Total Alkalinity Total Phenols

SITE-SPECIFIC GROUNDWATER PARAMETERS

Group 2

Benzene Vinyl Chloride

<u>Group 3</u>

Acrolein Acrylonitrile Benzene Bromoform Carbon tetrachloride Chlorobenzene Chlorodibromomethane Chloroethane 2-Chloroethylvinyl ether Chloroform Dichlorobromomethane 1,1-Dichloroethane Table 2-1. Groundwater Monitoring Parameters (Continued, Page 2 of 2)

1,2-Dichloroethane 1,1-Dichloroethylene 1,2-Dichloropropane 1,3-Dichloropropylene Ethylbenzene Methyl bromide Methyl chloride 1,1,2,2-Tetrachloroethane Tetrachloroethylene 1,2-Trans-dichloroethylene 1,1,1-Trichloroethane 1,1,2-Trichloroethane Trichloroethylene Vinyl chloride

Source: ESE

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### 2.5 <u>SAMPLING METHODOLOGY</u>

Included in this subsection are procedures for equipment decontamination; groundwater sampling; quality assurance sampling; and the preservation, handling, and shipment of samples. All procedures in this section are in accordance with EPA Region IV Engineering Support Branch Standard Operating Procedures and Quality Assurance Manual dated February 1, 1991.

## 2.5.1 DEFINITIONS

The following definitions will be referenced throughout this section:

<u>Deionized (DI) Water</u>--Water which has been treated by being passed through a standard water column and an activated carbon unit. The water contains no detectable heavy metals or inorganic compounds of analytical interest and is relatively free of organic compounds.

<u>Tap Water</u>-- Potable water from an approved source which meets or exceeds EPA Drinking Waster Standards.

<u>Ultra Pure Water</u>--Water that has been additionally treated through a barnstead carbon treatment system and contains no organic compounds of analytical interest above the analytical laboratories routine detection limits.

## 2.5.2 SAMPLE CONTAINER CLEANING PROCEDURES AND LABELING

Standard sample container cleaning will be performed by the analytic laboratory in accordance with Section B-9 of the EPA Region IV Engineering Support Branch Standard Operating Procedures (and Quality Assurance Manual) dated February 1, 1991. Sample container cleaning procedures are presented in Table 2-2. Commercially cleaned containers using the referenced methods will be acceptable for sample containment.

A label must be placed securely on all groundwater sample containers in order to identify each sample fraction. The following information shall be included on each sample label:

1. Project number,

# Table 2-2. Sample Container Cleaning Procedures Within the Laboratory

	£	· · · · · ·		
Analysis/Parameter	Container Type	Matrix	Cleaning Protocol*	
Organic extractables	Glass jar with Teflon -lined cap	Water	Α	
Organic purgeables	Glass septum vial with Teflon -lined septum	Water	В	
Metals ,	Linear polyethylene cubitainer with polyethylene cap	Water	C	
Inorganics	Linear Polyethylene cubitainer with polyethylene cap.	Water	D	

Note: Glass = amber for all water analyses.

TOX = total organic halide

*Cleaning Protocol	*CI	eaning	Protocol	
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	A	В	С	D	· · · · · · · · · · · · · · · · · · ·
	x	X	x		Wash with hot tap water using laboratory-grade, nonphosphate detergent.
	x	x	x		Rinse 3 times with tap water.
	x		x		Rinse with 1:1 nitric acid (reagent-grade nitric acid diluted with ASTM Type 1 deionized water).
	х	х	x		Rinse 3 times with ASTM Type 1 deionized water.
	x				Rinse with pesticide-grade methylene chloride using 20 mL per 64-oz bottle, 10 mL per 32- or 16-oz bottle, or 5 mL per 8- or 4-oz bottle. Methylene chloride is used as oganics rinse.
	x	x			Oven dry, using a forced air oven, at 105 to 125 C for 1 hour.
	Ω.		x		Invert and air dry in contaminant-free environment.
2				x	No cleaning required; use new cubitainers only.

Source: ESE, 1991.

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- 2. Sample station identification number,
- 3. Type of sample (groundwater),
- 4. Signature(s) of the sampling technician(s),
- 5. Sample Preservation Method,
- 6. Analyses to be conducted on sample,
- 7. Time and date of collection, and
- 8. Any comments (filtration, pH, spec. conductance, etc.).

## 2.5.3 FIELD DECONTAMINATION

Decontamination procedures presented in the following subsections will be followed for all nondedicated sampling equipment that contacts the sample matrices.

## 2.5.3.1 Decontamination Procedures for Groundwater Purging Equipment

All downhole purging equipment including submersible pumps, drop pipe, hoses, and water level sounding equipment will be decontaminated using the following procedure:

- 1. Using a brush, wash with standard nonphosphate laboratory detergent mixed in tap water; acceptable phosphate-free substitutes shall be Detergent 8 and Citranox available from Baxter Scientific or equal products from other sources;
- 2. Rinse with tap water;
- 3. Rinse with Deionized water;
- 4. Equipment should be placed in a polyethylene bag or wrapped with polyethylene film to prevent contamination during storage or transit.

## 2.5.3.2 Decontamination Procedure for Groundwater Sampling Equipment

Teflon Bailers will be used to obtain samples. Decontamination procedures for the bailers will include:

- 1. Rinse equipment thoroughly with tap water in the field as soon as possible after use.
- 2. The equipment will be washed thoroughly with laboratory detergent and tap water using a brush to remove any particulate matter or surface film;
- 3. The equipment will be rinsed thoroughly with tap water;

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- 4. Rinse the equipment with at least 10 percent nitric acid solution;
- 5. Rinse equipment thoroughly with tap water;
- 6. Rinse equipment thoroughly with deionized water;
- 7. Rinse equipment twice with pesticide grade isopropanol and allow to air dry;
- 8. Wrap equipment completely with aluminum foil to prevent contamination during storage and/or transport to the field; and

## 2.5.4 GROUNDWATER SAMPLING

The following procedures will be used in the collection of groundwater samples:

- 1. pH, conductivity, and temperature meters will be calibrated in accordance with the manufacturers instructions and documented on calibration forms in the field notebook.
- 2. Immediately prior to purging a well, the static water level below the top of the well casing will be measured to the nearest 0.01 ft using an electric (conductive) well probe. The probe cable will include electric wire which will conduct electricity to the conductivity probe tip. When the tip encounters water, the circuit will be completed, setting off a visual and audible signal. The cable will be calibrated in 0.1-ft increments. The depth to water will be read directly from where the tape contacts the top of casing mark on each well and recorded in the field notebook. A typical groundwater sampling form is included in Appendix C of the closure plan.
- 3. The volume of water in the well, including the saturated pore volume (assumed 30%) of the sand packed annulus, will be calculated based on the static water level and the well construction information. Well volume calculations will be placed in the field notebook.
- 4. The monitor well will be purged a minimum of five well volumes until pH and specific conductance measurements stabilize. Purging will be performed using a centrifugal pump with stainless steel drop pipe, stainless steel submersible pump, or a bailer. The pump must be equipped with a check valve to prevent water from running back down into the well when the pump is shut off. The hose or tubing used with the pump and the drop pipe must be adequately decontaminated prior to use at

each well site. Temperature, pH, and specific conductance will be monitored to ensure the water quality has stabilized to within 10 percent of the previous reading for at least three readings taken at least 0.5 well volumes apart. If a pump is used the rate of pumping must be determined and noted in the field logbook. The total amount of water purged, pH, specific conductance, and temperature will be measured and recorded in the field notebook. Purging equipment other than that stated above may be used with the approval of the ACOE project manager.

- 5. Extremely slow recharging wells will be purged dry, allowed to recharge at least 80 % of its initial depth, and purged dry a second time, and then purged dry a third time prior to sampling. If excessive time is required for the well to recharge to 80 percent, the consultant's project manager and the ACOE project manager will be notified prior to classifying the well as dry. If a well has insufficient recharge water after being purged dry, that well will be sampled as soon as enough water is in the well to obtain a sample. The total amount of fluid purged will be measured and recorded in the field notebook.
- 6. Monitor wells will be sampled immediately after purging using decontaminated closed top teflon bailers. The bailers will be decontaminated in accordance with Section 2.4.3 of this document. No glue or solvents may be used for bailer construction. The type of bailer used for sampling (closed top) must be noted in the field notebook. A teflon coated wire leader shall be used to prevent the rope from coming into contact with the water.
- 7. All sampling equipment will be protected from contaminated soil surfaces to prevent contamination of the samples (e.g., equipment may be placed on disposable polyethylene plastic sheeting).
- 8. The bailer will be rinsed at least once with well water (i.e. the first bail is discarded) prior to collecting a sample.

Groundwater sampling data (including sample number, location, quantity of water purged, field parameters, site conditions, etc.) must be documented in a field notebook.

## 2.5.5 PURGE WATER AND DECONTAMINATION WATER DISPOSAL

During each sampling event all purge water and decontamination water will be disposed of on the ground downgradient from the wellsite. Containerization of the water will not be necessary.

### 2.5.6 QUALITY CONTROL SAMPLES AND SAMPLING PROCEDURES

The following subsections will describe quality control sampling as required in the EPA Region IV Engineering Branch Standard Operating Procedures and Quality Assurance Manual. Quality Control samples required at each monitored area include: duplicate samples, preserved and unpreserved field blanks, volatile organic aromatic trip blanks, metals and inorganic preservative blanks, rinse water blanks, equipment blanks, and spike and blank samples.

### 2.5.6.1 **Duplicate Samples**

Two sets of duplicate samples will be obtained as a measure of the precision of the sample collection process. One set will be placed in sample containers supplied by, and the samples submitted to the ACOE Missouri Division Laboratory (MRDL). A second duplicate sample will be sent to the contracting laboratory for analysis. These samples will be collected at the same time, using the same procedures, and the same equipment as the required samples. No more than 10 percent of all required samples will be duplicated during any sampling event. The MRDL point of contact will be:

Laura Percifield Missouri River Division Laboratory HTRW Chemistry Branch CEMRD-ED-LC 420 S. 18th Street Omaha, Nebraska 68102 (402) 444-4314

The MRDL point of contact must be notified at least 1 week prior to sample collection.

### 2.5.6.2 Metals and Inorganic Preservative Blank

Metals and general inorganic sample containers will be filled with ultra-pure water and preserved in the field to check the preservatives for analyzed parameters. These blank samples will be

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preserved using the same batch of preservatives as used to preserve the samples collected. No more than one preservation blank will be necessary per 10 percent of all sample fractions requiring preservation per field sampling event.

## 2.5.6.3 Rinse Water Blank

A minimum of one sample of the deionized water used to decontaminate the sampling equipment will be taken per sampling event. The samples will be taken directly from the sprayer or container used to decontaminate the equipment and submitted to the analytical testing laboratory for a standard ICP scan. When field deionized water is used, one sample will be submitted to the analytic laboratory per week of sampling.

### 2.5.6.4 VOA Trip Blank

Trip blanks will be prepared in the laboratory prior to sending field kits into the field. VOA sample jars will be decontaminated and filled with ultra-pure water. One sample per day will be shipped back to the office each day VOA samples are obtained. One VOA trip blank will be shipped with each cooler containing water samples for VOA analysis. These jars are not to be tampered with and will be used as a check of the VOA sample bottle decontamination procedures.

### 2.5.6.5 Equipment Blank

The effectiveness of the field decontamination procedures will be monitored by rinsing field cleaned equipment with ultra-pure water and collecting the rinse water in standard sample containers. The equipment blank will be analyzed for the same parameters as required by the well sampling. At least one sample and no more than 5% of the equipment cleaned during the field sampling effort will be sampled.

### 2.5.6.6 Spike and Blank Samples

Spike and blank samples will be provided by the ACOE Missouri River Division laboratory in Omaha Nebraska. These samples will be sent along with the field samples to the appropriate contracting laboratory. These samples will be given fictitious sample identification similar to the

actual well designations found on all sampling forms and labels. The samples will be only identified as a blank or a spike in the field notebook.

### 2.6 ANALYTICAL PROCEDURES, SAMPLE PRESERVATION, AND HOLDING TIMES

Table 2-3 identifies the analytical methods, proper containers, preservation techniques, and maximum holding times established by EPA (50 Federal Register, January 1985). These procedures and holding times must be met to validate the analytical data.

### 2.7 CHAIN OF CUSTODY, HANDLING, AND CUSTODY SEALS

The primary purpose of sample chain of custody is to create an accurate, written, verified record which can be used to trace possession and handling of the samples from the moment of collection until receipt by the laboratory. Adequate sample custody will be achieved by means of an approved chain-of-custody form. A typical chain-of-custody form is enclosed in Appendix C.

The chain of custody form will be filled out at each well site immediately after the sample fractions are taken. The following information must be included on the Chain-of Custody form:

- 1. Project name and number,
- 2. Sample station identification number,
- 3. Type of sample (groundwater),
- 4. The sampler's signature,
- 5. Whether sample was preserved,
- 6. Analyses to be conducted on sample,
- 7. Time and date of collection, and
- 8. Any comments (filtration, pH, spec. conductance, etc.).

After each sample container is filled, the samples will be preserved in accordance with Section 2.5 of this groundwater monitoring plan. The containers will be subsequently sealed with appropriate custody seals and immediately iced down in a secured ice chest and prepared for shipment. A water proof, insulated, plastic ice chest will be used for sample shipment.

Parameter	Analytical Method	Sample Preservation*	Sample Containers	Holding Times
Background Water				
Quality Parameters				
<u>(Group 1)</u>				
	70/0		1 T D	6 months
Arsenic	7060	$HNO_3$ , $pH<2$	1 L, P	350 전 - 53 - 55 - 53
Barium	6010	HNO <sub>3</sub> , pH<2	1 L, P	6 months
Chloride	. 300	None	P, G	28 days
Cadmium	6010	HNO <sub>3</sub> , pH<2	1 L, P	6 months
Chromium	6010	$HNO_3$ , $pH<2$	1 L, P	6 months
Lead	7421	$HNO_3$ , $pH<2$	1 L, P	6 months
Mercury	7470	$HNO_3$ , $pH<2$	1 L, P	28 days
Selenium	7740	$HNO_3$ , $pH<2$	1 L, P	6 months
Silver	6010	HNO <sub>3</sub> , pH<2	1 L, P	6 months
Specific Conductance	120.1	None	1 L, P	N/A
Total Organic Carbon	415.2**	$H_2SO_4$ , pH < 2	1 L, P	28 days
Total Organic Halogen	450.1	$H_2SO_4$ , pH < 2	250 mL, GS	7 days
pH	150.1**	None	1 L, P	N/A
Total Phenols	420**	H <sub>2</sub> SO <sub>4</sub> , pH<2	1 L, G, T	28 days
Site-Specific				
<u>Groundwater Parameters</u> (Group 2)				
<u>1010up 21</u>				
Benzene	8240	HCL, pH<2	60ml, GS	14 days
Vinyl Chloride	8240	HCL, pH<2	60ml, GS	14 days
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Annual Groundwater		5°	*	
Parameters	×			
(Group 3)	*			
Toroth of				
Benzene	8240	HCL, pH<2	60ml, GS	14 days

# Table 2-3. Chemical Analysis Procedures

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# Table 2-3. Chemical Analysis Procedures

Parameter	Analytical Method	Sample Preservation*	Sample Containers	Holding Times
Bromoform	8240	HCL, pH<2	60ml, GS	14 days
Carbon tetrachloride	8240	HCL, pH<2	60ml, GS	14 days
Chlorobenzene	8240	HCL, pH<2	60ml, GS	14 days
Chlorodibromomethane	8240	HCL, pH<2	60ml, GS	14 days
Chloroethane	8240	HCL, pH<2	60ml, GS	14 days
2-Chloroethylvinyl ether	8240	HCL, pH<2	60ml, GS	14 days
Chloroform	8240	HCL, pH<2	60ml, GS	14 days
Dichlorobromomethane	8240	HCL, pH<2	60ml, GS	14 days
1,1-Dichloroethane	8240	HCL, pH<2	60ml, GS	14 days
L.2-Dichloroethane	8240	HCL, pH<2	60ml, GS	14 days
1,1-Dichloroethylene	8240	HCL, pH<2	60ml, GS	14 days
1,2-Dichloropropane	8240	HCL, pH<2	60ml, GS	14 days
L,3-Dichloropropylene	8240	HCL, pH<2	60ml, GS	14 days
Ethylbenzene	8240	HCL, pH<2	60ml, GS	14 days
Methyl bromide	8240	HCL, pH<2	60ml, GS	14 days
Methyl chloride	8240	HCL, pH<2	60ml, GS	14 days
Methylene chloride	8240	HCL, pH<2	60ml, GS	14 days
1,1,2,2-Tetrachloroethane	8240	HCL, pH<2	60ml, GS	14 days
<b>Fetrachloroethylene</b>	8240	HCL, pH<2	60ml, GS	14 days
Foluene	8240	HCL, pH<2	60ml, GS	14 days
1,2-Trans-dichloroethylene	8240	HCL, pH<2	60ml, GS	14 days
1,1,1-Trichloroethane	8240	HCL, pH<2	60ml, GS	14 days
L,1,2-Trichloroethane	8240	HCL, pH<2	60ml, GS	14 days
Frichloroethylene	8240	HCL, pH<2	60ml, GS	14 days
Vinyl chloride	8240	HCL, pH<2	60ml, GS	14 days

Note: P = Polyethylene.

pp = Polypropylene.

G = glass.

 $T = Teflon^{\textcircled{o}}-lined cap.$ 

GS = glass container with Teflon®-lined septa, no headspace.

U.S. Environmental Protection Agency, SW-846, "Test Methods for Solid Waste" \*Standard Method for the Examination of Water and Wastewater, 16th ed., 1985. +All samples chilled to 4°C.

\*\*Methods for Chemical Analysis of Water and Wastes, EPA 600/4-79-020.

Source: ESE

Once the ice chest is filled with sample containers, the void spaces between the sample containers will be packed with vermiculite or other absorbent packing material and ice will be added to the ice chest so that the samples remain at 4°C. The chain of custody forms will be signed and placed into the ice chests. The ice chest will be subsequently sealed with Department of Transportation (DOT) approved shipping tape. Custody seals will be placed on each sample cooler, signed, and dated in a manner which will indicate if the cooler was tampered with during shipment. The samples will be shipped to the contracted laboratory for overnight delivery.
#### 3.0 GROUNDWATER ANALYTICAL EVALUATION AND REPORT

Within one month of the receipt of analytical data, a report will be sent to the ACOE project manager. The report will include a discussion of the sampling methodology, an evaluation of the groundwater analytical data, and the conclusions including necessary corrective actions. The following subsections will discuss the reporting protocol.

#### 3.1 EVALUATION OF GROUNDWATER ANALYTICAL DATA

The evaluation of groundwater data will be performed in accordance with 40 CFR 264.97 and 264.98 for detection monitoring systems. Background data from the upgradient wells will be based on quarterly data obtained during the first year of detection monitoring.

For all indicator parameters (See Table 2-1, Group 1) for which the background (upgradient well data) data coefficient of variation is less than 1.0, groundwater analytical data will be analyzed to determine statistical changes in groundwater quality parameters between the background (upgradient) wells and mean of the each sampled well. The analytical results will be evaluated using the Cochran's Approximation to the Behren's-Fisher Student's T-test at the 0.05 level of significance as described in 40 Code of Federal Regulations (CFR) Part 264, Appendix IV. All parameters analyzed will be subjected to a one-tailed analysis except pH which will be analyzed using the two-tailed analysis.

If the coefficient of variance in the background (upgradient well) data is equal or greater than 1.0, an alternate statistical procedure will be used to provide reasonable assurance that the groundwater quality was not impacted by the facility. One such statistical procedure is the ANOVA Parametric Analysis of Variance. Prior to implementing an alternative statistical procedure, the procedure must be approved by ACOE and the Georgia Department of Natural Resources.

For all groundwater quality parameters presented in Table 2-1, Group 2, the data obtained will be compared with the water quality parameters presented in 40 CFR 264.94; Table 1. The data

3-1

obtained for parameters listed in Table 2-1, Group 2 must not exceed the associated maximum values for groundwater quality from 40 CFR 264.94.

#### 3.2 ANALYTICAL REPORT CONTENTS

The results of the groundwater sampling and analyses will be due to the ACOE project manager within 30 days after the analytical data have been received by the reporting party.

The final report will include, as a minimum:

- 1. Monitor well location map;
- 2. Well construction details;
- 3. Potentiometric surface map of the uppermost aquifer below each monitored area;
- 4. Results of chemical analyses;
- 5. Results of Cochran's Approximation to the Behren's-Fisher Student's T-Test as described in 40 CFR Part 264, Appendix IV; and
- 6. Results of comparison between well data and Ambient groundwater quality criteria.

The report shall indicate which parameters, if any, exhibit statistical changes or do not meet groundwater quality requirements and a brief discussion of the results.

#### 3.3 CORRECTIVE ACTION PROGRAM

Statistically significant changes for individual parameters do not necessarily indicate contamination problems at any site. Groundwater quality fluctuations often occur in response to changes of the potentiometric surface between periods of extreme groundwater fluctuations. Background data obtained during the first four calendar quarters of monitoring will be used to determine an annual range of concentrations observed in wells at the site. Subsequent analyses will be compared with the background and other previously obtained data to determine if statistically significant changes had occurred.

The monitoring report sent to the ACOE project manager will include an analysis of statistically significant changes detected at the site and levels of constituents found above maximum levels as

3-2

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indicated in the permit. A recommendation of whether a replicate round of sampling will be necessary will be included in the report. If it is determined that replicate samples should be obtained to verify the previous results, the specific parameters to be analyzed will be based upon only those parameters exhibiting statistically significant changes.

Within seven days of assessment of a statistically significant change or elevated constituent levels, a written report of the assessment will be sent to the Fort Stewart Department of Environmental Health. If the supplemental analytical results verify the existence of contamination in the monitoring zone, the appropriate remedial action will be taken.

#### REFERENCES

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### APPENDIX A

### to

### Groundwater Monitoring Plan - Appendix B to Closure Plan

HUNTER AAF--SOIL BORING LOGS, SOIL SAMPLING LOGS, MONITOR WELL CONSTRUCTION, AND MONITOR WELL DEVELOPMENT AND GROUNDWATER SAMPLING LOGS

BA-1

# ATTACHMENT A SOIL BORING AND MONITOR WELL LOGS

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	Client: Project Number: Drilling Contractor: Driller: Logged By: Drilling Method: Boring Location:	U.S. Army Corps of Engineers 3902018 Layne Environmental, Inc. M. Barton T. Trent CME Continuous Sampler 97' North of Northwest Corner	Boring Completed: Boring Diameter: Well Casing Diameter Surface Elevation: Elevation Datum:	2/12/90 2/12/90 N/A
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		3 ft	- fine grained, light brown (PID = 0)	
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	CS5'	5' 5 ft	- gray, saturated (PID = 0)	
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		2	Hunt			Fire Tr Stewart,			ea	Log of Bor	ing No. HM	W-03			eet No. 2 of 2
	Pro Dr Dr Lo Dr	Client:U.S. Army Corps of EngineersBoring Started:Project Number:3902018Boring Completed:Drilling Contractor:Layne Environmental, Inc.Boring Diameter:Driller:M. BartonWell Casing Diameter:Logged By:T. TrentSurface Elevation:Drilling Method:Hollow-Stem AugerElevation Datum:Boring Location:N734719.69E816011.23									d: neter: ::	2/8/9 2/9/9 10 inc 2 inch 26.6 ft NGVI Mobile	0 h	к 1 Пар	
	Elevation	Depth	Samp. Type and Diam.	Samp. Adv. Len Core	Sample Rec. Core Rec.	Sample Blows "N" Recovery	Well Construction	Lithology		MATERIAL DESCI	RIPTION		P 20 4	ercent × 0 60 LL 0 60	: 80
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10. 10. 10.

	Pr Dr Dr Lo Dr	ient: oject Nu illing Co iller: gged By illing M oring Lo	ontrac 7: lethod	tor:	U 39 L M T H	Stewart, S. Army 202018 ayne Env I. Barton . Trent ollow-Sta 734718.9	Corps ironme em Aug	ntal, 1 ;er	nc.	2	а	Boring I Well Ca Surface Elevatio	Started: Completed Diameter: sing Diam Elevation n Datum: Drill Rig:	neter: : :	2/: 10 2 in 27. NG	12/90 12/90 inch nch 2 ft 3 VD obile I	Lă	
	Elevation	Depth	Samp. Type and Diam.	Samp. Adv. Len Core	Sample Rec. Core Rec.	Sample Blows "N" Recovery	Well Construction	Lithology		MATERIAL	DESCRI	PTION			20	Per 40 PL		80 <b>1</b>
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		Hunter AAF, Fire Training Area Fort Stewart, GA	Log of Boring No. HMW-05 Sheet No. 2 of 2
		Client:U.S. Army Corps of EngineersProject Number:3902018Drilling Contractor:Layne Environmental, Inc.Driller:M. BartonLogged By:T. TrentDrilling Method:Hollow-Stem AugerBoring Location:N734495.13E816073.98	Boring Started:2/11/90Boring Completed:2/11/90Boring Diameter:10 inchWell Casing Diameter:2 inchSurface Elevation:28.8 ftElevation Datum:NGVDType of Drill Rig:Mobile B-57
	}	Elevation Depth Samp. Type and Diam. Sample Rec. Core Rec. Core Rec. Recovery Well Construction Lithology	Moisture Content Percent × 20 40 60 80 PL   LL   20 40 60 80
		SS 1.5 1.5 2-2-7 (SP) SAND,	poorly graded, fine to medium grained, saturated (PID=0)
l.	1 -		
		-10-	
. (	1	40 SS 1.5 1.1 3-5-9 40 ft - medi	um dense (PID=0)
	1		
ſ	1	-15-	
	) .	45 SS 1.5 3-3-5 45 ft - loose	(PID=0)
		SS 1.5 3-3-5 45 ft - loose	
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		50-BORING TH	ERMINATED AT 50.0 FT BGS
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t f		$SS = Splitspoon$ $\frac{\nabla}{2} = Water Level Encountered During Drilling  \underline{\nabla}{2} = Water Level Encountered During Drilling $	LL = Liquid Limit
			vel After Well Development     PL = Plastic Limit       14A     Hunter/ESE
	] .		

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	<ul> <li>Conservation</li> </ul>	ent: oject N	umber			.S. Army 902018	Corps	s of Engi	neers		Boring S Boring (	Started: Completed	l:		/12/9 /12/9		_
)	Dri Dri Log Dri	illing C iller: gged By illing M ring Lo	ontrac y: lethod	tor: :	L M T H	ayne Env 1. Barton 1. Trent Iollow-St 1734497.9	em Au	ger	2.		Boring I Well Ca Surface Elevatio	Diameter: sing Diam Elevation on Datum: Drill Rig:	eter: :	10 2 2 N	0 inch inch 8.3 ft GVD	n	7
	Elevation	Depth	. Type Diam.	. Adv.	le Rec. e Rec.	Sample 31ows "N" 2. Core Recovery	Well Construction	Lithology	4	MATERIAL DESCH	IPTION			M 2(	Pe	re Co ercent X ) 60	t
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# ATTACHMENT B SOIL SAMPLING LOGS

WRD2144 . 1/TOBY . 1 . 10/01/87

#### DATA FORM SOIL SAMPLING

Project: FT. STEWART - HUNTER AAF	Date: 2-12-90
Station I.D.: $H \le R - 1$	Time: 1705
Station I.D.: n 212-1	
Sample No.:	e ee
Approximate Ground Surface Elevation : 35.	.7' N.G.V.D .
8-10	
Depth of Sample:8-10	
Sampling Method: CME CONTINUOUS SAM	NALE R

Sample Description: LT. BROWN SAND, FILE TO MEDIUM GRAINED, SATURATED

Miscellaneous Observations:

Fractions: 55, SV VOLATILES & PAH'S (A key to Fractions is provided on the last page of this Attachment) Date 2-12-90 Signed \_

WRD2144 - 1/TOBY - 1 10/01/87

#### DATA FORM SOIL SAMPLING

Project: FT. STEWART - HUNTER AAFDate: 2-13-90 Station I.D.: HSB-2 Time: 0745 2 Sample No.: Approximate Ground Surface Elevation : 29' N.G.V.D. Depth of Sample: Sampling Method: CME CONTINUOUS SAMPER

Sample Description: SAND, LT, BROWN, GREY, WET, FDUE TO MEDIUM GRAINCO

Miscellaneous Observations:

Fractions: 55,5V

VOLATICES & PAH'S

\_\_\_\_ Date \_\_\_\_ 2-13-90

WRD2144.1/TOBY.1 10/01/87

#### DATA FORM SOIL SAMPLING

Project: FT. STEWART - HUNTER AAF Date: 2-13-90
Station I.D.: <u>HSR-3</u> Time: <u>0835</u>
Sample No.:
Depth of Sample: $6-8$
Sampling Method: CME CONTENNOUS SAMPLER

Sample Description: SAND, LT, GREY, COARSE GRAINED, SATURATED, SP

Miscellaneous Observations:

Fractions: 55,5V

VOCATILES, PAH'S

Signed Jaconces D. J.S. Date 2-13-90

#### DATA FORM SOIL SAMPLING

Project: FT, STEWART - HUNTER AAF	Date: 2-13-90
Station I.D.: HSB-4	Time: 0935
//	
Sample No.:	
Approximate Ground Surface Elevation : 27' $7 - 4$	N.G. V.D.
Depth of Sample:	= 3 
Sampling Method: CME CONTINUOUS	SAMPLER

Sample Description: SAND, FINE TO MEDIUM GRADUED, BLACK, GREY, WETISP

Miscellaneous Observations:

Fractions: 55, 5V VOCATIES, PAH'S

1...

L \_

Date 2-13-90 ۲ Signed <u>S</u> (i)

WRD2144.1/TOBY.1 10/01/87

#### DATA FORM SOIL SAMPLING

Project: FT. STEWART HUNTERAAF Date: 2-13-90 Station I.D.: SB-5 Time: 1135
Sample No.:
Depth of Sample: <u>5-8</u>
Sampling Method: CME CONTINUOUS SAMPLER

Sample Description: SAND, FINE TO COARSE GRAINED, SATURATED BLACK, GREY, SW

Miscellaneous Observations:

Fractions: SS, SV

VOLATILES, PAH'S

Date 2-13-90 Signed

B-5B

WRD2144 - 1/TOBY - 1 10/01/87

#### DATA FORM SOIL SAMPLINC

Project: FISTEWART - HUNTER PAF Date: 2	13-90
Station I.D.: <u>SB-G</u> Time:	1245
Sample No: $\bigcirc$ Approximate Ground Surface Elevation : <b>BO' N.G.V.D.</b>	
Depth of Sample:	
Sampling Method: CME CONTINUOUS SAMPU	ER

Sample Description: SAND, WHITE, BROWN, FINE TO COARSE GRAINED, SATURATED, SW

Miscellaneous Observations:

Fractions:55,5V

VOLATILES, PAH'S

Signed

2-13-90

WRD2144.1/TOBY.1 10/01/87

#### DATA FORM SOIL SAMPLING

Project: FT. STEWART-HUNTER MAR Station I.D.: TRif BCARK	Date: Time:	2-13-90	
Sample No.:			
Depth of Sample:			

Sample Description: 3 40 mL BOTRES, DIWATER

Miscellaneous Observations:

Fractions:  $\bigvee, \bigvee, \bigvee$ 

VOLATALES

Date 2-13-90 Signed \_

#### ESE KEY TO FRACTION CODES 3/90

AIR:	<u>CODE</u>	E <u>PRESERVATIVE</u>	<u>CONTAINER</u>	<u>ANALYSIS TYPE</u>	<u>HOLDING TIMES</u>
	AA	4-Deg-C	Various	Various	Various
	AO	Exclude Light	Sorbent	Organic	14 Days
	AV	Exclude Light	Charcoal	Volatiles	14 Days
	FL	Keep Upright	Cassette	Various	Various
SOILS	SS	4-Deg-C	G, 500 mL	All excl. Vol.	7-28 Days
	SV	4-Deg-C	G, 60 mL	Volatiles	7-14 Days
WATER:	AL B C CL	4-Deg-C(T) 4-Deg-C;NaOH,pH>12 4-Deg-C 4-Deg-C (Pref'd Filtered & Fro	P, 1-4 L G, 1-4 L	Aldicarb Cyanides Var.Inorganic Chlorophyll C)	14 Days 14 Days 1-28 Days 1 Day
	EC ED F	4-Deg-C(T)g 4-Deg-C(T)	G, 1 L G,2x60 mL* P, 4 L	Chlor'd Pests EDB, DBCP Collection prior to Fi	
8 6 4	FI FM FP H	4-Deg-C(T) Formaldehyde 4-Deg-C(T) Zn-Acet;NaOH,pH>10		GC/FI Organic "Quats" GC/FP Organic Sulfides	7 Days 28 Days 14 Days 7 Days
	HB	4-Deg-C(T)	G, 1 L	Chlor'd Herbs	7 Days
	LC	4-Deg-C	G, 1 L	HPLC Organics	7 Days
	M	4-Deg-C(T)	P, 250 mL	Bacteriologic	1 Day
	MS	4-Deg-C(T)	G, 1 L	GCMS Extr.Org.	7 Days
	N NF	HNO <sub>y</sub> pH<2 HNO <sub>y</sub> pH<2	P, 1 L P, 1 L	Metals (Total) Mercury (Total) Metals (Dissolved) Mercury (Dissolved)	180 Days 28 Days 180 Days 28 Days
	NC NP O	4-Deg-C 4-Deg-C 4-Deg-C;H2S0, pH<2	G, 1 L G, 1 L G, 1 L	Nitrocellulose GC/NP Organic Oil&Grease, TRPH	7 Days 7 Days 7 Days 28 Days
•	OD	4-Deg-C	G, 1 L	Odor	2 Days
	R	HNO <sub>3</sub> ,pH<2	P, 1-4 L	Radionuclides	180 Days
	S	4-Deg-C;H <sub>2</sub> S0 <sub>6</sub> ,pH<2	P, 1 L	Nutrients	28 Days
	(UP)	4-Deg-C(T)	G, 1 L	Pest(Antiq'd)	7 Days
	V	4-Deg-C(T)	G,3x60 mL*	Halogen, Vols	14 Days
	VP	4-Deg-C;HCL,pH<2(T)	G,3x60 mL*	Aromatic Vols	14 Days
	(W)	4-Deg-C(T)	G, 1 L	Orgs, FPD Extr's	7 Days
	X	4-Deg-C(S)	G,2x250mL*	TOX(USATHAMA)	7 Days
	XP Z	4-Deg-C;H <sub>2</sub> SO <sub>4</sub> pH<2(S) 4-Deg-C;H <sub>2</sub> SO <sub>4</sub> pH<2		TOX Total Phenols	7 Days 28 Days
OTHER:	OL	None	G,10-100mL	Organic-Oil	14 Days
	TS	-20-Deg-C	Various	Frozen Tissue	Various

FOOTNOTES: (T) - Add Sodium Thiosulfate (Na<sub>2</sub>S<sub>2</sub>O<sub>3</sub>) If Res.Cl Present (0.25g/L)

(S) - Add Sodium Sulfite (Na<sub>2</sub>SO<sub>2</sub>) If Res.Cl Present (0.1M, 1 mL/L).

- Volatiles Bottles (VOAs) With Teflon-Lined Rubber Septa.

#### INSTRUCTIONS FOR SAMPLING AND SHIPPING

-Plastic (P) Containers May Be Rinsed With Sample; Do Not rinse Glass (G) -Fill Completely, Especially For Volatiles (Fill These Slowly; Achieve

Positive Meniscus; Cap; Invert; Check for Air Bubbles; Top Off If Needed. -Preserve With Reagents Provided As Instructed Above (VP's Are Pre-Preserved) -Fill-out Logsheet/Chain-of-Custody. Indicate: Sample Number (\*) and Fractions

Collected; Dates/Times of Collection & Shipment; Appropriate Field Notes; Be Sure To Sign Bottom of Each Page Where and As Indicated.

-Ship With Bagged Ice in Ice-chest By Express Carrier To Lab Coordinator's Attention.

Source: ESE, 1990.

File: MH01\Prection Key

## ATTACHMENT C MONITOR WELL CONSTRUCTION LOGS

AAAP 10/4/84



.B-1C

AAAP 10/4/85

Logged By: T. TRENT Client: ARMY CORPSOF ENGINEERS Drilling Contractor: LAYNE ENUDRONMEDIAL Location: FT. STEWART - HUNTER AAF Driller's Name: Jon MARK BARTON Job Number: 3902018 Well Number Hnw-2 Date/Time: Start 1600/2-9-90 Finish 1820/2-9-90 Comments (Lost circulation interval, Water level changes, Hole collapse interval, etc.): Complete Grout : 1820, 2-9 Begin Development: 740, 2-13 Method of Development : Pumping Total Volume of Water Extracted : 115 gal. Elapsed Time : 85.3 hrs. Depths in Reference to Ground Level Top of + 3.0' Protective Casing-- Locking Cap **Protective Pipe** Top of Well Casing Type, Diameter STEFE, 4X4 +7 Cement/Gravel Pad, Height = 4" Extends 2" into borehole. Top of Cement-Bottom of 2.0' Protective Casing-9.21 Ground Water -- Type of Grout CONESTAR PORTAND TYPEI COMENT W BENTONTTE ADWDER Casing: P/C Schebuce 40 Type Z' I.D. Couplings: Type THREADED FLUSH JOINT Number\_ Depths \_ Top of 2.1 Bentonite Seal -- Type of Plug BENTONITE 3 Top of Gravel Pack-4,6 Gravel Pack: Material <u>SAND</u> 20/30 MESH Placed with 2" PVC Tremie Top of Screen -Screen: Type <u>PVC Scheadure ()</u> Diameter <u>2"</u> Length <u>707</u> Length\_\_\_\_ Slot Size 0.010 14.6 Bottom of Screen 10 1/4 " 15.0' Bore Hole Diameter \_ Total Depth of Bore Hole

NOT TO SCALE

AAAP 10/4/85



NOT TO SCALE

B-3C

MONITOR WELL CONSTRUCTION

AAAP 10/4/85



NOT TO SCALE

444P .014185



NOT TO SCALE

AAAP 10/4/85

MONITOR WELL CONSTRUCTION

Logged By: T.TRENT - Client: <u>ARMY CORPS OF ENGINEERS</u> Location: <u>FTISTEWART - HUNTER ATTE</u> Job Number: <u>2902018</u> Drilling Contractor: <u>LATNE ENUMERIA</u> Driller's Name: <u>MAZE BAZIEN</u> Well Number: <u>H</u> MW-6 Date/Time: Start 2-12-90/1315 Finish 2-12-90/1415 Comments (Lost circulation interval, Water level changes, Hole collapse interval, etc.): Complete Grout : 1415, 2-12 Begin Development : 0915, 2-13 Method of Development : Pumping Total Volume of Water Extracted : 85 gal. Elapsed Time : 19.0 hr. Depths in Reference to Ground Level Top of Protective Casing +3.0 / - Locking Cap Protective Pipe Type, Diameter STEEL, 4" × 4" Top of Well Casing \_ + 2.5' Coment/Gravel Pad, Height = 4" Extends 2" into borehole Top of Cement-Bottom of 2.01 Protective Casing-Ground Water -- Type of Grout LOWESTAR PORTCOND TYPE I CEMENT, W/ BENTONITE POWDER - Casing: Type PVC Diameter 2' Type THERACE FLISH DODWT Number\_\_\_\_ Depths . Top of Bentonite Seal \_\_\_\_\_, O - Type of Plug ENUTROPIC BONTONTE Top of Gravel Pack 2.01 Top of Screen \_\_\_\_\_\_.0 ( Gravel Pack: SAND 20/30 MES 14 Material SAND 20/30 MES 14 Placed with 2"PVC Tremie Screen: PUC Type \_\_\_\_ Diameter \_\_\_\_ Length\_\_\_\_ Slot Size \_ O.D/O" 13.0 - Bore Hole Diameter \_\_\_\_\_\_\_/0//4 " Bottom of Screen-15.0 Total Depth of Bore Hole

NOT TO SCALE

B-6C

ATTACHMENT D MONITOR WELL DEVELOPMENT LOGS AND MONITOR WELL SAMPLING LOGS

D-ECSWVOW.2/FIELDFORM.1 10/22/84

44			
	MONITOR WELL	. DEVELOPMENT	neet of T
	4		<u> </u>
size: HUNTER A	Well AF Designat	H- ion: <u>Mw-1</u>	Installation Date: $2-7-90$
Well construction de		Saraanad (	Borehole
Total depth (top	of casing): 50,5	interval: (10)32	diameter: 1014
Water losses duri	ng drilling:	Fluid pur	ging:
Height of well ca	sing (ground sur:	face): W	ell diameter: 2 "
Standing water: Wel	l casing/screen:	47.7	
(From Chart) Ann			
· · · · · · · · · · · · · · · · · · ·			
Date and time of deve	lonment. 2-13	-90/1/100	
Method of development	(aug /b-di-	P. C. D.	In la an
Depth(s) of pumping a	and elapsed time	at each depth:	
	· · · ·		
1 c			
Well depth (sounded) Physical appearance of Initial: <u>Cousy</u> During development	f water (clarity , Grey :	, color, particula	
Final: <u>CCORC</u>			
Field analysis	Initial	During (2)	Final
Time	1610	1631 16	46 1719
Conductivity	280	15/ 13	<u>k</u> 128
pH Torono turo	6.95	<u>_6.62</u> <u>_6.3</u>	5
Temperature	_27.2	-dil -da	$\sum \alpha_{1,k}$
Quantity of water rem	oved/time for rea	noval (both increm	ențal and total)
0/1600 10/11	40, 20/1720	, 30/1800,60	2000
<u> </u>		, 2 0/ 100 100	1.000
n An an an Alban Alban			
	· · · · · · · · · · · · · · · · · · ·		<u> </u>
Collect a l-pint samp	le of last water	removed.	
Comments:			
5 / <sup>2</sup>			
	· · · · · · · · · · · · · · · · · · ·		
<u> </u>	m mining and		
the Wand	- 2-12-90	¢	: <b>.</b>
Signed	B-1D Date	Approved	Date

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D-ECSWVOW.	2/FIELDFORM. 1
	10/22/84

	MONITOR WELL DEVELOPMENT Sheet 2 of 9
Site: HUNTER AAF	Well $H-$ Installation Designation: $M \cup -Z$ Date: $Z-Q-C$
Well construction detai	Screened Borehole
Total depth (top of	casing): 17.1 interval: 4.6-14.6diameter: 104
Water losses during	drilling: Fluid purging:
Height of well casim	ng (ground surface): Well diameter: 2'
Standing water: Well o	casing/screen: 5.2
	us (volume x 30%): 1,17
Data and time of double	opment: 2-13-90 6740
vate and time of develo	pump/bailer): Pomp Pumping rate: 5ga/men
Depth(s) of pumping and	elapsed time at each depth:
70	a
Initial: Grey, Ma During development:	
	Firm Fare Stormers
Field analysis	Initial During (2) Final
Field analysis Time	Initial During (2) Final   0741 0746 0755 0805
Field analysis Time Conductivity	Initial During (2) Final   0741 0746 0755 0805   27 28 28 28
ield analysis Time	Initial During (2) Final   0741 0746 0755 0805
Field analysis Time Conductivity pH Temperature	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Field analysis Time Conductivity pH Temperature Quantity of water remove	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Field analysis Time Conductivity pH Temperature	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Field analysis Time Conductivity pH Temperature Quantity of water remove 0/0740, 20	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Field analysis Time Conductivity pH Temperature Quantity of water remove	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Field analysis Time Conductivity pH Temperature Quantity of water remove 0/0740, 20	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Field analysis Time Conductivity pH Temperature Quantity of water remove 0/0740, 20 Collect a 1-pint sample	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Field analysis Time Conductivity pH Temperature Quantity of water remove 0/0740, 20 Collect a 1-pint sample	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Field analysis Time Conductivity pH Temperature Quantity of water remove 0/0740, 20 Collect a 1-pint sample	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Field analysis Time Conductivity pH Temperature Quantity of water remove 0/0740, 20	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
Field analysis Time Conductivity pH Temperature Quantity of water remove 0/0740, 20 Collect a 1-pint sample	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

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D-ECSWVOW.	2/FIE	LDFORM. 1
		10/22/84

		MONITOR WEL	L DEVELOPMENT	Sheet 3	of 9	
2 20	Size: HUNTER AAF	Well Designat	H- ion: <u>Mw-3</u>	Install. Date:	$\frac{10-90}{2-10-90}$	
	Well construction deta	ils from borin	g log: Screened	Boreho		
	Total depth (top of	: casing): <u>515</u>	interval:}	90-40 diamet	er: <u>101/4</u>	
	Water losses during					
	Height of well casi	ng (ground sur	face):	Well diam	heter: $Z''$	
	Standing water: Well					
	(From Chart) Annul	us (volume x 3)	DZ): 1.17			
×		-				
	Date and time of devel					
• 2/	Method of development	(pump/bailer):	PUMP P	umping rate:	Sgr min	
	Depth(s) of pumping an	d elapsed time	at each depth	:		
e a			10 			
15 D		ă.				
	Water level Before	developments (	CY During	. 24		
					201	
	Well depth (sounded)	Before: 4	7.0	After:	1.26	
	Physical appearance of					
	Initial: <u>Cooc</u> During development:	14, ISCACK, U	PGY			
	Final: CCERZ,		2.7 5			
	Field analysis	taitial	During	(2)	Final	
	Time	1313	133.3	1412	1434 13	50.
	Conductivity	190	140	125	140	11
	PH	6.34	6.20	7.32	~ ~ / .	20
	Temperature	21.8		23,7	22.4 2	.Z,:
	Quantity of water remov	ed/time for rea	moval (both in	cremental an	d total)	
	0/12/0,:100/1333	150/1410.	230/1435	260/1500	S	
			, , , ,	· ·		
م بر میں اور اور میں اور				4. <u>1</u>		`!
	Collect a l-pint sample	of last water	removed.	· · · ·	·* . · · · ·	•
	Comments:	-				
	2			5	1	
50 28	P. M. Manadl	- 2-12-91		n		
	Signed	B-3D	Approved	3	Date	
•		ענ-ע				

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D-ECSWVOW.2/FIELDFORM.1 10/22/84

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	MONITOR WELL DEVELOPMENT Sheet 4 c	, C
	1	
Sice: HUNTER AA	Well $H-$ Installation TF Designation: $MW-4$ Date: 2-	n 12-'
Well construction de	etails from boring log:	2
Total depth (top	of casing): 15.4 Screened Borehole diameter:	10
Water lease duri	ing drilling: Fluid purging:	÷
	using (ground surface): Well diameter	. 7
	1 casing/screen: <u>8.7</u>	: <u> </u>
	ulus (volume x $30$ %): $1.17$	
(Prom Chart) Ann		
Data and time of day	-12.00/1000	
	elopment: 2-13-90/1500	
	t (pump/bailer): <u>POMP</u> Pumping rate:	
Depth(s) of pumping a	and elapsed time at each depth:	
		-
	· · · · · · · · · · · · · · · · · · ·	
	• · · · · · · · · · · · · · · · · · · ·	
Well depth (sounded) Physical appearance of Initial: <u>George</u> During development Final: Ccorre	Before: <u>12,9</u> After: <u>48,7</u> of water (clarity, color, particulates, odor) ,CCOUDY t:	<u><u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u></u>
FILIAL. CLEAFL		
Field analysis Time	Initial During (2) Fin	1al
Conductivity	$\frac{1507}{280}  \frac{1522}{295}  \frac{1557}{362}  \frac{16}{3}$	203
pH	687 7.05 657 6	.47
Temperature	<u>1955 4.6 146 1</u>	9.0
Quantity of water rem	noved/time for removal (both incremental and to	(tal)
0/1505, 75/1522	110/1530 150/1603	
The second second		• • •
Collect a 1-pint samp	le of last water removed.	<del></del>
Comments:		
<u> </u>		
/:. r		
11/ 21/-		
Chamey N. fr	<u>t 2-13-90</u>	
Signed	B-4D Date Approved	Date

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D-ECSWVOW.	2/FIELDFORM. 1
	10/22/84

	MONITOR WELL DEVELOPS	Sheet 5	of _1
Sice: HUNTER AAS	Well H- Designation: Mu	-5 Installa Date:	tion 2-11-9
	ails from boring log: Screen f casing): <u>515</u> interv	ned val: <u>59-49</u> diamet	le er: <u>10 '</u>
Water losses durin	g drilling: I	luid ourging:	
	ing (ground surface):	N 26 8 8 8 8 8	eter: 2"
	casing/screen: 39		
	lus (volume x 30%):		
			26 C
Date and time of deve	lopment: <u>2-13-90/0</u>	950	
fethod of development	(pump/bailer): PUMP	_ Pumping rate:	
Depth(s) of pumping a	nd elapsed time at each d	epth:	
		ta an	
·			
			-
		24	HR
Nell depth (sounded) Physical appearance o Initial: <u>Greep</u>	e development: <u>eis</u> Du Before: <u>4614</u> Water (clarity, color, CACE, <u>Dewsely</u> , <u>Cloudy</u> S	After: <u>48</u> , particulates, odo epernente	) }}
Vell depth (sounded) Physical appearance o Initial: <u>Greep &amp;</u> During development	Before: 4614 Water (clarity, color, CACE, DENSELY, CLOUDY 5	After: <u>48</u> , particulates, odo epernente	) }}
Vell depth (sounded) Physical appearance o Initial: <u>Grey p</u> During development Final: <u>Ccenr</u>	Before: 4614 Water (clarity, color, CACF, DENSELY, CLOUDY S ORANGE, SEMI CLEF W/ FEW SEPTMENTS Initial Dur	After: <u>48</u> , particulates, odo epernente	<del>}}</del>
Vell depth (sounded) Physical appearance o Initial: <u>Greet &amp;</u> During development Final: <u>Ccenn</u> Vield analysis Time	Before: <u>4614</u> Water (clarity, color, <u>CACE, DEWSELY, (LOUDY 5</u> <u>ORANGE, SEMT CLEE</u> <u>W FEW SEDTMENTS</u> <u>Initial Dur</u> <u>O948</u> <u>1004</u>	After: <u>48</u> , particulates, odo epimenic e, Fones ring (2) <u>7023</u>	77 r) Final 1055
Vell depth (sounded) Physical appearance o Initial: <u>Greer &amp;</u> During development Final: <u>Cerre</u> Vield analysis Time Conductivity	Before: 4614 Water (clarity, color, CACE, DEWSELY, CLOUDY 5 ORANKE, SEMI-CCCE W/FEW SEDIMENTS Initial Dur O948 1004 Z25 160	After: $46$ , particulates, odo express e, foxes ting (2) 150	77 r) Final 1055 145
Vell depth (sounded) Physical appearance o Initial: <u>Greer p</u> During development Final: <u>Ccenn</u> Field analysis Time Conductivity pH	Before: 4614 Water (clarity, color, CACE, DENSELY, CLOUDY 5 ORANKE, SEMI CLEP W/FEW SEPTMENTS Initial Dur O948 1004 Z255 160 6.42	After: $\frac{46}{9}$ , particulates, odo corrector e, Fores ring (2) $\frac{1023}{6.40}$	77 r) Final 1055 145 G(11
Vell depth (sounded) Physical appearance o Initial: <u>Greep p</u> During development Final: <u>Ccenn</u> Field analysis Time Conductivity pH Temperature C	Before: 4614 Water (clarity, color, CACE, DEWSELY, CLOUDY 5 ORANY, JEMI CLEA W/ FEW SEPTMENTS Initial Dur O948 1004 Z25 160 6,54 6.42 28.5 ZZ.2	After: $46$ , particulates, odo cornerve e, Fores ring (2) 150 6,40 22.0	77 r) Final 1055 145 G(11 23.8
Vell depth (sounded) Physical appearance o Initial: Greer & During development Final: <u>Ccenn</u> Vield analysis Time Conductivity pH Temperature C	Before: <u>4614</u> Water (clarity, color, <u>CACE, DEWSELY, CLOUDY 5</u> <u>ORANXE, SEMT, CLEE</u> <u>Initial Dur</u> <u>O948</u> <u>1004</u> <u>225</u> <u>160</u> <u>6054</u> <u>6.42</u> <u>28.5</u> <u>22.2</u> ved/time for removal (bot	After: $46$ , particulates, odo express e, Foxes ring (2) 1023 6.40 22.0 h incremental and	77 r) Final 1055 145 G(11 23.8
Vell depth (sounded) Physical appearance o Initial: Greer & During development Final: <u>Ccenn</u> Field analysis Time Conductivity pH Temperature C	Before: 4614 Water (clarity, color, CACE, DEWSELY, CLOUDY 5 ORANY, JEMI CLEA W/ FEW SEPTMENTS Initial Dur O948 1004 Z25 160 6,54 6.42 28.5 ZZ.2	After: $46$ , particulates, odo express e, Foxes ring (2) 1023 6.40 22.0 h incremental and	77 r) Final 1055 145 G(11 23.8
Vell depth (sounded) Physical appearance o Initial: <u>Grey &amp;</u> During development Final: <u>Cconc</u> Field analysis Time Conductivity pH Temperature C Quantity of water remo O/O945 - OC	Before: <u>4614</u> Water (clarity, color, <u>CACE, DEWSELY, CLOUDY 5</u> <u>ORANXE, SEMT, CLEE</u> <u>Initial Dur</u> <u>O948</u> <u>1004</u> <u>225</u> <u>160</u> <u>6054</u> <u>6.42</u> <u>28.5</u> <u>22.2</u> ved/time for removal (bot	After: $\frac{46}{0.40}$ particulates, odo corners c, fores ring (2) $\frac{1023}{150}$ $\frac{6.40}{22.0}$ h incremental and 220/1055	77 r) Final 1055 145 G(11 23.8
Vell depth (sounded) Physical appearance o Initial: <u>Greef</u> During development Final: <u>Cconn</u> Vield analysis Time Conductivity pH Temperature C Quantity of water remo OG45 - OG45	Before: $46.4$ Water (clarity, color, CACE, DENSELY, CLOUDY 5 0RANX,C, SEMT CCCP 1 FEW SEDTMENTS Initial Dur 0948 1004 225 160 6.54 $6.4228.5$ $22.2ved/time for removal (both0/1000$ 165/020	After: $\frac{46}{0.40}$ particulates, odo corners c, fores ring (2) $\frac{1023}{150}$ $\frac{6.40}{22.0}$ h incremental and 220/1055	77 r) Final 1055 145 G(11 23.8
Vell depth (sounded) Physical appearance o Initial: <u>Greer &amp;</u> During development Final: <u>Cerre</u> Vield analysis Time Conductivity pH Temperature C OUDALS - C OUDALS	Before: $46.4$ Water (clarity, color, CACE, DENSELY, CLOUDY 5 0RANY,G, SEMT CCCP 1 FEW SEPTMENTS Initial Dur 0948 1004 225 160 6.42 28.5 22.2 Ved/time for removal (both 2/1000, $165/1020$ ,	After: $\frac{46}{0.40}$ particulates, odo corners c, fores ring (2) $\frac{1023}{150}$ $\frac{6.40}{22.0}$ h incremental and 220/1055	77 r) Final 1055 145 G(11 23.8
Vell depth (sounded) Physical appearance o Initial: <u>Greer &amp;</u> During development Final: <u>Cerre</u> Vield analysis Time Conductivity pH Temperature C Quantity of water remo O/0945, PC Ollect a l-pint sample	Before: $46.4$ Water (clarity, color, CACE, DENSELY, CLOUDY 5 0RANY,G, SEMT CCCP 1 FEW SEPTMENTS Initial Dur 0948 1004 225 160 6.42 28.5 22.2 Ved/time for removal (both 2/1000, $165/1020$ ,	After: $\frac{46}{0.40}$ particulates, odo corners c, fores ring (2) $\frac{1023}{150}$ $\frac{6.40}{22.0}$ h incremental and 220/1055	77 r) Final 1055 145 G(11 23.8
Vell depth (sounded) Physical appearance o Initial: <u>Greef</u> During development Final: <u>Ccenn</u> Field analysis Time Conductivity pH Temperature C Quantity of water remo O/0945 - PC	Before: $46.4$ Water (clarity, color, CACE, DENSELY, CLOUDY 5 0RANY,G, SEMT CCCP 1 FEW SEPTMENTS Initial Dur 0948 1004 225 160 6.42 28.5 22.2 Ved/time for removal (both 2/1000, $165/1020$ ,	After: $\frac{46}{0.40}$ particulates, odo corners c, fores ring (2) $\frac{1023}{150}$ $\frac{6.40}{22.0}$ h incremental and 220/1055	77 r) Final 1055 145 G(11 23.8
Vell depth (sounded) Physical appearance o Initial: <u>Greer &amp;</u> During development Final: <u>Cerre</u> Vield analysis Time Conductivity pH Temperature C Vantity of water remo O/O945, PC	Before: $46.4$ Water (clarity, color, CACE, DENSELY, CLOUDY 5 0RANY,G, SEMT CCCP 1 FEW SEPTMENTS Initial Dur 0948 1004 225 160 6.42 28.5 22.2 Ved/time for removal (both 2/1000, $165/1020$ ,	After: $\frac{46}{0.40}$ particulates, odo corners c, fores ring (2) $\frac{1023}{150}$ $\frac{6.40}{22.0}$ h incremental and 220/1055	77 r) Final 1055 145 G(11 23.8

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D-ECSWVOW.2/FIELDFORM.1 10/22/84

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12	MONITOR WELL DEVELOPMENT She	et 6 of
Site: HUNTER AA	Vall H- T	nstallation Date: $2/2$
	etails from boring log: Screened of casing): <u>15.4</u> interval: <u>3-13</u>	Borehole diameter: ]
Water losses duri	ng drilling: Fluid purg	ing:
	using (ground surface): Wei	ll diameter:
Standing water: Wel ( <u>From Chart</u> ) Anr	1 casing/screen: <u>6,9</u> ulus (volume x 30%): <u>1,17</u>	
Date and time of dev	elopment: 2-13-90/095	
	t (pump/bailer): <u>Pump</u> Pumping	rate: Salm
	and elapsed time at each depth:	
9 79 1. BER 200 600		
ар. 1998 —		1
Water level Befo	re development: 3.7 During:	24 HR After: 3
Well depth (sounded) Physical appearance Initial: <u>Pepper</u> During developmen	Before: 10,6 After of water (clarity, color, particulat A GREY, MORKY SEDMENTS t:	After: 3 :14.59
Well depth (sounded) Physical appearance Initial: <u>Reports</u> During developmen Final: <u>Ccehe</u> Field analysis	Before: 10,6 After of water (clarity, color, particulat a (SREY, MORKY SEDMENTS	After: 3 :14.59
Well depth (sounded) Physical appearance Initial: <u>Reports</u> During developmen Final: <u>CCCAC</u> Field analysis Time	Before: 10,6 After of water (clarity, color, particulat A GREY, MORKY SEDMENTS :: 	After: <u>3</u> : <u>14,59</u> es, odor)  Final 2/2.5
Well depth (sounded) Physical appearance Initial: <u>Reports</u> During developmen Final: <u>Ccehe</u> Field analysis	Before: $10.6$ After of water (clarity, color, particulat a <u>GREY</u> , <u>MURKY</u> <u>SEVENCENTS</u> :: <u>Initial</u> <u>During (2)</u> <u>OQIG</u> <u>OQZG</u> <u>1157</u> <u>235</u> <u>223</u> <u>240</u> <u>6:30</u> <u>6:37</u> <u>6:3</u>	After: 3 : es, odor)  Final 2 2 56,22
Well depth (sounded) Physical appearance Initial: <u>Reports</u> During developmen Final: <u>CCAR</u> Field analysis Time Conductivity	Before: 10.6 After of water (clarity, color, particulat a <u>GREY</u> , <u>MURKY</u> <u>SEVENCENTS</u> t: <u>Initial</u> <u>During (2)</u> <u>OQIG</u> <u>OQZG</u> 115 <u>235</u> 223 240	After: 3 : es, odor)     
Well depth (sounded) Physical appearance Initial: <u>Perpeis</u> During developmen Final: <u>CCAR</u> Field analysis Time Conductivity pH Temperature	Before: $10.6$ After of water (clarity, color, particulat a <u>GREY</u> , <u>MURKY</u> <u>SEVENCENTS</u> :: <u>Initial</u> <u>During (2)</u> <u>OQIG</u> <u>OQZG</u> <u>1157</u> <u>235</u> <u>223</u> <u>240</u> <u>6:30</u> <u>6:37</u> <u>6:3</u>	After: 3 : <u>14.59</u> es, odor) Final 2 <u>12.5</u> 5 <u>6.7</u> 1 <u>21.7</u> atal and tota
Well depth (sounded) Physical appearance Initial: <u>Perpeis</u> During developmen Final: <u>CCAR</u> Field analysis Time Conductivity pH Temperature	Before: $10.6$ After of water (clarity, color, particulat a Grey, MOREY SEDMENTS Initial During (2) OQLG OQZG 1/5 235 223 240 G:30 6:37 6:3 18:3 21 poved/time for removal (both increment	After: 3 : <u>14.59</u> es, odor) Final 2 <u>12.5</u> 5 <u>6.7</u> 1 <u>21.7</u> atal and tota
Well depth (sounded) Physical appearance Initial: <u>Revolution</u> During developmen Final: <u>CCCAR</u> Field analysis Time Conductivity pH Temperature Quantity of water rem O/915, $S5/$	Before: $10.6$ After of water (clarity, color, particulat a Grey, MOREY SEDMENTS Initial During (2) OQLG OQZG 1/5 235 223 240 G:30 6:37 6:3 18:3 21 poved/time for removal (both increment	After: 3 : <u>14.59</u> es, odor) Final 2 <u>12.5</u> 5 <u>6.7</u> 1 <u>21.7</u> atal and tota
Well depth (sounded) Physical appearance Initial: <u>Revolution</u> During developmen Final: <u>CCCAR</u> Field analysis Time Conductivity pH Temperature Quantity of water rem O/915, $S5/$	Before: $10.6$ After of water (clarity, color, particulat <u>A (SREY, MORLY SEDIMENTS</u> <u>Initial</u> During (2) <u>OQL6</u> <u>OQZ6</u> <u>1155</u> <u>235</u> <u>223</u> <u>240</u> <u>6.30</u> <u>6.37</u> <u>6.3</u> <u>18.7</u> <u>18.3</u> <u>21.</u> poved/time for removal (both increment <u>OQ25</u> , <u>75/1150</u> , <u>85/1253</u>	After: 3 : <u>14.59</u> es, odor) Final 2 <u>12.5</u> 5 <u>6.7</u> 1 <u>21.7</u> atal and tota
Well depth (sounded) Physical appearance Initial: <u>Revolus</u> During developmen Final: <u>CCAR</u> Field analysis Time Conductivity pH Temperature Quantity of water rem O/915, $SS/Collect a 1-pint samp$	Before: $10.6$ After of water (clarity, color, particulat <u>A (SREY, MORLY SEDIMENTS</u> <u>Initial</u> During (2) <u>OQL6</u> <u>OQZ6</u> <u>1155</u> <u>235</u> <u>223</u> <u>240</u> <u>6.30</u> <u>6.37</u> <u>6.3</u> <u>18.7</u> <u>18.3</u> <u>21.</u> poved/time for removal (both increment <u>OQ25</u> , <u>75/1150</u> , <u>85/1253</u>	After: 3 : <u>14.59</u> es, odor) Final 2 <u>12.5</u> 5 <u>6.7</u> 1 <u>21.7</u> atal and tota
Well depth (sounded) Physical appearance Initial: <u>Revolus</u> During developmen Final: <u>CCAR</u> Field analysis Time Conductivity pH Temperature Quantity of water rem O/915, $SS/Collect a 1-pint samp$	Before: $10.6$ After of water (clarity, color, particulat <u>A (SREY, MORLY SEDIMENTS</u> <u>Initial</u> During (2) <u>OQL6</u> <u>OQZ6</u> <u>1155</u> <u>235</u> <u>223</u> <u>240</u> <u>6.30</u> <u>6.37</u> <u>6.3</u> <u>18.7</u> <u>18.3</u> <u>21.</u> poved/time for removal (both increment <u>OQ25</u> , <u>75/1150</u> , <u>85/1253</u>	After: 3 : <u>14.59</u> es, odor) Final 2 <u>12.5</u> 5 <u>6.7</u> 1 <u>21.7</u> atal and tota
Well depth (sounded) Physical appearance Initial: <u>Revolus</u> During developmen Final: <u>CCAR</u> Field analysis Time Conductivity pH Temperature Quantity of water rem O/915, $SS/Collect a 1-pint samp$	Before: $10.6$ After of water (clarity, color, particulat <u>A (SREY, MORLY SEDIMENTS</u> <u>Initial</u> During (2) <u>OQL6</u> <u>OQZ6</u> <u>1155</u> <u>235</u> <u>223</u> <u>240</u> <u>6.30</u> <u>6.37</u> <u>6.3</u> <u>18.7</u> <u>18.3</u> <u>21.</u> poved/time for removal (both increment <u>OQ25</u> , <u>75/1150</u> , <u>85/1253</u>	After: 3 : <u>14.59</u> es, odor) Final 2 <u>12.5</u> 5 <u>6.7</u> 1 <u>21.7</u> atal and tota

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D-WR85.1/SAMPFORM.1 03/15/85

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## WELL SAMPLING DATA FORM

Well Number: <u>HMW-1</u> Date: <u>3-7-90</u> Time: <u>0845</u>
Boring Diameter: 1044 Well Casing Diameter: 24
Annular Space Length: 46.78 Stickup: 2.5'
WATER LEVEL
Held:
Cut:
DTW: Top of Casing
· COLUMN OF WATER IN WELL
Casing Length: <u>48,28</u>
DTW Top of Casing: 12.30
Column of Water in Well: <u>35,98</u>
VOLUME TO BE REHOVED
Gallons per foot of A.S. (from chart) = 1.1 +
Column of Water or Length of A.S. (whichever is less) X 35.98
Volume of Annular Space = 42.09
Gellons per foot of Casing =
Column of Water X 35.98
Volume of Casing
Total Volume (Volume of A.S. + Volume of Casing) = <u>48.15</u>
Number of Volumes to be Evacuated
Total Volume to be Evacuated =28075
Method of Purging (pump, bailer, etc.): Pomp
FIELD ANALYSES Start Mid End
Time $1322 1352 1640$
pH <u>5.26</u> <u>5.37</u> <u>5.40</u>
$\frac{212}{24^{\circ}} = \frac{200}{24^{\circ}} = \frac{170}{2200}$
Temperature of a state
Total Volume Purged: 260 gallons
Sample Time: Sample Number: _HMW-1 + 1
FRACTIONS Vx3, Wx2
B C CF CL F E M N NF O P B RP RS S T UP Z
NOTES
(A key to Fraction codes is provided on the last page of this Attachment)
NO CI
Signed/Sampler: Janes VIII Date: 3-7-90
Signed/Reviewer: Date:

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WELL SAMPLING DATA FORM

	Well Number: HMW-2 Date: 3-7-90 Time: 084.8
	HATEB LEVEL
	Held:
	Cut:
1	DTW: Top of Casing
	COLUMN OF WATER IN WELL
	Casing Length: 16.15
2 8	
120	VOLUME TO BE REMOVED
	Gallons per foot of A.S. (from chart) = $\frac{111+}{5.83}$
	Gallons per foot of Casing = $\frac{1/63}{500}$
	Column of Water X 5.83
	Volume of Casing
	Total Volume (Volume of A.S. + Volume of Casing) = <u>+,7,7</u>
	Number of Volumes to be Evacuated X
	Total Volume to be Evacuated = <u>38.85</u>
ģ	Method of Purging (pump, bailer, etc.): Korten
	FIELD ANALYSES Start Mid End
	Time 0920 0945 1015
	pH 5121 512 512
	$\frac{33}{18^{\circ}} = \frac{50}{18^{\circ}} = \frac{50}{18^{\circ}}$
	Total Volume Purged: 40 gallons
	Sample Time: 1620 Sample Number: <u>HMW-2 #2</u>
	FRACTIONS VX3, WX2
	B C CF CL F H M (N) NF
	OPZ
	NOTES (U, U, U, U
•••	
*) (8)	
	Signed/Sampler: Wares Det Date: 5-7-90
	Signed/Reviewer: Date:

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D-WR85.1/SAMPFORM.1 03/15/85

## WELL SAMPLING DATA FORM

	HALL-3 Mate: 3-8-90 Time: 0825
	Well Number: ITVICO D
	Boring Diameter: 10 Herr Capita Children -
	Annular Space Length: Stickup: 2.5'
•	WATER LEVEL
	Held:
	Cut:
	DTW: Top of Casing
	COLDEN OF WATER IN WELL
	Casing Length: <u>419.26</u>
	DTW Top of Casing: <u>+115</u>
	Column of Water in Well: 42,13
	VOLUME TO BE FEMOVED
	Gallons per foot of A.S. (from chart) = <u>111+</u>
	Column of Water or Length of A.S. (whichever is less) X 42.13
	Volume of Annular Space = 49.29
	Gallons per foot of Casing = .163
	Column of Water X <u>42.13</u>
	Volume of Casing = $\frac{6.86}{57.107}$
	Total Volume (Volume of A.S. + Volume of Casing) = <u>56.15</u>
	Number of Volumes to be Evacuated
	Total Volume to be Evacuated = $280.75$
	Method of Purging (pump, beiler, etc.): Pump
	FIELD ARALYSES Start Mid . End
	Time <u>825</u> <u>851</u> <u>91.2</u>
	pt <u>6.03</u> <u>6.11</u> <u>(e.05</u>
	Conductivity <u> </u>
	Temperature 19.5°C 20.5°C 20.0°C
	Total Volume Purged: 300 gallons Sample Number: HNW-3 * 3
	Sample Time: Sample Number: HMW-3 *
	FRACTIONS VX3, WX2
	B C CF CL F H M (N) NF
	O P B R RS S T OP 2
	NOTES
і. і.	
	0-8-8
	Signed/Sampler: Manes DAT Date: 5-8-90
	Signed/Reviewer: Date:
	- B-9D

## WELL SAMPLING DATA FORM

				/	
Well Number: HML	U-LL Date	3-8-90	Time:	0345	
Boring Diameter:	10	Well Casing Dian		21	
Annular Space Length	:	Stickup	(	2.4	
HATER LEVEL					
Eeld:					
Cut:		а х <sup>1</sup> а			
DTV:		Top of Casing	8 <u>.</u>	•	
· COLUMN OF WATER IN S	RIL.				
Casing I		5,22	2014) 		
DTW Top of (		7.50			
Column of Water in		7.72	-	©₽	
VOLUME TO BE REHOVED					
Gallons per foot of		hart)	•	1.17	
Column of Water of	Length of A.S	. (whichever is lo	ess) X	7.72	
Volume of Annular			•	9.03	
Gallons per foot o				.163	
Column of Water			x	5.72	
Volume of Casing				1.25	
Total Volume (Volu	me of A.S. + V	olume of Casing)	۳	10.2	
Number of Volumes			X	5	
Total Volume to be	Evacuated	1		51.0	
Method of Purging ()	oump, bailer, e	te.): <u>Pump</u>	<b>x</b>		
FIELD ANALYSES	Start	Mid	· · · G	.End	
Time	845	6.41		56	
pE	(0.45			is and the second secon	
Conductivity	240	19.°C		0.5°C	
Temperature	150				
. Total Volume Purged	- 22 -	gallons	HALAN-	4 * 4	-
Sample Time:	<u> </u>	Sample Number:	<u></u>		
FRACTIONS VK 3, W			× (	N) NF	
ВСС	r CL	р н			15
O P B NOTES	102	RS S		UP	· :.·
1	$\langle \rho \rangle$				٠
Signed/Sampler:	Kano !!		Date:	3-8-90	
Signed/Reviewer:			· Date:		
PIRIEN DEATERET	· · · · · · · · · · · · · · · · · · ·				

B-10D

## WELL SAMPLING DATA FORM

				0
Well Number: H	mw-5 Dec	·: 3-7-90		<u>995</u>
Boring Diameter:	10''	Well Casing Di		4
Annular Space Le	ngth:	Sticku	p:	
HATER LEVEL				
Held:		•• •		
Cut:			•	
DTW:		Top of Casing	a	2
· COLUMN OF WATER	DI WILL			
Casi	ng Length:	48,77	-	
DTW Top	of Casing:	7.88	—	
Column of Water	in Well:	40.89	10 0	•
VOLUME TO BE REH	DAED			
Gallons per for	ot of A.S. (from	chart)		17
Column of Water	or Length of A.	S. (whichever is 1		.89
Volume of Annu!	lar Space		California and California	7.84
Gallons per for	ot of Casing			163
Column of Water		50 <b>10</b>		0.89
Volume of Casin	1 <b>g</b>		=	0.66
Total Volume (N	folume of A.S. +	Volume of Casing)	• _ 5	4.50
Number of Volum	nes to be Evacuat	ed	x	5
Total Volume to	be Evacuated		= _27	12.5
Method of Purging	(pump, bailer,	ecc.): <u>Pump</u>		
FIELD ANALYSES	Start	Mid		in the second se
Time	950	1000		$\underline{O}$
рĦ	6.40	<u>G.14</u>		6
Conductivity	140	132		>
Temperature	19°C	-19.55	5 _2/	<u>`C</u>
Total Volume Purg	red: 280	gallons 20,58		
Sample Time:	<u> </u>	_ Sample Number:	HMW - 5	* 5
FRACTIONS V×3	W×2		$\sim$	
вс	C7 .C.	F E	M (N)	NF
0 P	B RP	RS S	ፕ መግ	Z
NOTES	New george of			
	n n	<b>,</b>		80 × 8 8 0
Signed/Sampler:	Househ	da.	Date: 3	-7-90
	Mand) D		· Date:	
Signed/Reviewer:				

B-11D

## WELL SAMPLING DATA FORM

	Well Number: HMW-6 Date: 3-8-90 Time: 10.40
	Boring Diameter: 10" Well Casing Diameter: 2"
	Annular Space Length: Stickup:
	WATED LEVEL
	Held:
	Cut :
	DTW: Top of Casing
	COLUMN OF WATER IN WELL
•	Casing Length: 14.59
	DTW Top of Casing: 6:55
	Column of Water in Well:8.04
	VOLUME TO BE REMOVED
<i></i>	Gallons per foot of A.S. (from chart) = 1.17
	Column of Water or Length of A.S. (whichever is less) X 8,04
	Volume of Annular Space = 9.40
	Gallons per foot of Casing = .163
	Column of Water X <u>8.04</u>
	Volume of Casing = 1.31
	Total Volume (Volume of A.S. + Volume of Casing) = 10.71
	Number of Volumes to be Evacuated X5
	Total Volume to be Evacuated = 53.55
	Method of Purging (pump, beiler, etc.): PUMP
	FIELD ANALYSES Start Hid . End
	Time 1040 1045 1100
	pt 10.44 (0.5) 6.54
	Conductivity <u>320</u> <u>340</u> <u>335</u>
	Temperature 17,5°C 20°C 19°C
<b>8</b> 5	Total Volume Purged: 60 gallons
	Sample Time: Sample Number: HMW-6 * 6
÷.	FRACTIONS UK3 WX2
	B C CF CL F H M (N) NF
	OPBR2 RPRSSTUPZ
	Date: 3-5-90
	Signed/Sampler:
	Signed/Reviewer: Date:

B-12D

D-ECSWVOW.2/FIELDFORM.2 01/03/85

### MONITOR WELL WATER LEVEL MEASUREMENTS

Sheet \_/ of \_\_\_

Site FT. STEWART - HUNTER ARE Measured By T. TROUT Reference Mark: Client Anny Conps OF Engeneres Project Number 3902015 Top of well casing  $\times$ Ground surface  $\times$ 

	2			Tape Re Held	eading Wet	Depth	
	Well	Date	Time	Length	Length	To Water	Comments
н	mw-l	2-9-90	1600			10.2	
Н	Mw-2	2-10-90	0800			9.3	
Н	mw-5	2-12.90	1233			5.2	
H	mw-3	2-12-90	1250	2		5.4	
Н	mw-1	2-13-90	0723			10.6	
Н	MW.Z	2-13-90	0854			9,3	1
Н	Mw-3	2-13-90	1505		" a	7.2	
Н	mw-4	2-13-90	0848			4.2	
Η	mw-s	2-13-90	1136			6.5	
н	mw.6	2-13-90	0817			3.7	
						2	
Н	mw-1	3-7-90	0845			12.3	*
Н	mw-2	3-7-90	0848			10.32	*
HI	nur 3	3-7-90	0853			7,13	★
H	mw-4	3.7.90	0855			7.50	*
H	mw-s	3-7-90	6900			7.88	*
H	mw-6	3-7-90	0905			6.55	*
	15						· · · · · · · · · · · · · · · · · · ·
	Ъ.	3			2 11 - 11 - 11 - 11 - 11 - 11 - 11 - 11		,

B-13D

#### ESE KEY TO FRACTION CODES 3/90

	AIR:	<u>CODE</u> AA AO AV FL	<u>PRESERVATIVE</u> 4-Deg-C Exclude Light Exclude Light Keep Upright	<u>CONTAINER</u> Various Sorbent Charcoal Cassette	<u>ANALYSIS TYPE</u> Various Organic Volatiles Various	<u>HOLDING TIMES</u> Various 14 Days 14 Days Various
	SOILS:	SS SV	4-Deg-C 4-Deg-C	G, 500 mL G, 60 mL	All excl. Vol. Volatiles	7-28 Days 7-14 Days
	WATER:	AL B C CL	4-Deg-C(T) 4-Deg-C;NaOH,pH>12 4-Deg-C 4-Deg-C (Pref d Filtered & Froz	P, 1-4 L G, 1-4 L	Aldicarb Cyanides Var.Inorganic Chlorophyll )	14 Days 14 Days 1-28 Days 1 Day
		EC ED F FI FM FP H HB	4-Deg-C(T)g 4-Deg-C(T) - 4-Deg-C(T) Formaldehyde 4-Deg-C(T) Zn-Acet;NaOH,pH>10 4-Deg-C(T)	G, 1 L G,2x60 mL* P, 4 L G, 1 L P/G,500mL G,3x60 mL*	Chlor'd Pests EDB, DBCP Collection prior to Fie GC/FI Organic "Quats" GC/FP Organic Sulfides Chlor'd Herbs	7 Days 14 Days 14 Filtering 7 Days 28 Days 14 Days 7 Days 7 Days
		LC M MS N	4-Deg-C 4-Deg-C(T) 4-Deg-C(T) HNOypH<2 HNOypH<2	G, 1 L P, 250 mL G, 1 L P, 1 L P, 1 L	HPLC Organics Bacteriologic GCMS Extr.Org. Metals (Total) Mercury (Total) Metals (Dissolved)	7 Days 1 Day 7 Days 180 Days 28 Days 180 Days
			4-Deg-C 4-Deg-C 4-Deg-C;H <sub>2</sub> S0 <sub>4</sub> pH<2 4-Deg-C HNO <sub>4</sub> pH<2 4-Deg-C;H <sub>2</sub> S0 <sub>4</sub> pH<2 4-Deg-C(T) 4-Deg-C(T) 4-Deg-C(T) 4-Deg-C(T) 4-Deg-C(S) 4-Deg-C;H <sub>2</sub> SO <sub>4</sub> pH<2(S)	G, 1 L G, 1 L G, 1 L F, 1 L P, 1 L F, 1 L G, 1 L G, 3x60 mL* G, 3x60 mL* G, 1 L G, 2x250mL*	Mercury (Dissolved) Nitrocellulose GC/NP Organic Oil&Grease, TRPH Odor Radionuclides Nutrients Pest(Antiq'd) Halogen, Vols Aromatic Vols Orgs, FPD Extr's TOX(USATHAMA) TOX	28 Days 7 Days 7 Days 28 Days 28 Days 2 Days 180 Days 28 Days 7 Days 14 Days 14 Days 7 Days 7 Days 7 Days 7 Days 8 Days 8 Days 9 Days
(	OTHER:			G,10-100mL Various		14 Days Various

FOOTNOTES: (T) - Add Sodium Thiosulfate (Na<sub>2</sub>S<sub>2</sub>O<sub>3</sub>) If Res.Cl Present (0.25g/L) (S) - Add Sodium Sulfite (Na<sub>2</sub>SO<sub>3</sub>) If Res.Cl Present (0.1M, 1 mL/L).

- Volatiles Bottles (VOAs) With Teflon-Lined Rubber Septa.

### **INSTRUCTIONS FOR SAMPLING AND SHIPPING**

-Plastic (P) Containers May Be Rinsed With Sample; Do Not rinse Glass (G) -Fill Completely, Especially For Volatiles (Fill These Slowly; Achieve Positive Meniscus; Cap; Invert; Check for Air Bubbles; Top Off If Needed.

-Preserve With Reagents Provided As Instructed Above (VP's Are Pre-Preserved) -Fill-out Logsheet/Chain-of-Custody. Indicate: Sample Number (\*) and Fractions

Collected; Dates/Times of Collection & Shipment; Appropriate Field Notes;

Be Sure To Sign Bottom of Each Page Where and As Indicated. -Ship With Bagged Ice in Ice-chest By Express Carrier To Lab Coordinator's Attention.

Source: ESE, 1990.

File: IMHOI \ Prection Key

# ATTACHMENT E SEDIMENT SAMPLING LOGS

Station #	50-1	
Sampie #		-

Dace 2-12-90
Projec: FT. STEWART - HUNTER AAF
Field Personnel Titlent 1), BUTTAURE

÷. .,

STATION DESCRIPTION:

Signature

...

Sample Mechod: STEDNICES STEEL SPOON & BOWL

Water	Qu	ality Cond	itions:	CLEAR
Depth	to	Sediment	8"	•
Sedime	nc	Type: Gr	AUEL	e Sawo

Time of Sampling 0900

Fraction	Preservative/Amount	Container Type
55	NA, ICE	G, SCOML
SU .	NA, ICÉ	G, 60mc

Remarks: A Ky to Fraction codes is provided on the last page of this Attachment.

Date 2-12-90

B-1E

Station #	SD-2
Sample #	2

Date 2-12-90	
Projec: FT. STEWART - HUNTERAA	F
Field Personnel T. TRENTA J. BUTTRU	

STATION DESCRIPTION:

Sample Method: STOPENCESS STEER SPOON & BOWE

Water	Quá	ality	Condit	ions: (	LEAZ	
Depth	to	Sed in	ent	_Z'	• •	
Sedime	nt	Type :	SA	0		

Time of Sampling 0920

Fraction	Preservative/Amount	Container Type
55	NA, ICE	G, SOOML
SV .	NA, ICE	G, GOML
Remarks:		

Signature C Date 2-12-90

Station #	SD-3	
Sample #	3	

Date 2-12-90
Projec: FT. STEWART - HUNTER AAF
Field Personnel T.TRONT & J. BUTTRUFF

STATION DESCRIPTION:

Sample Mechod: STADUCESS STEEL BOWL & SPOOJ

Water	Qu	ality	Cond i	tions:C	CEA2	
Depth	to	Sed im	ent_	2'	1	
Sedime	ent	Type:	SA	UD 8 GT	AUEZ	

Time of Sampling 0930

FractionPreservative/AmountContainer Type55ICCG, SCOMESVICCG, GOMERemarks:

Date 2.12-90 Signature

Station # SD-3 REPLICATE Sampie # 4

Date 2-12-90
Projec: FT. STEWART - HUNTER ANF
Field Personnel T. TRONT & S. BUTIRUPT

STATION DESCRIPTION:

Sample Mechod: STADULESS STEEL BOWL & SPOON

Water	Qu	ality	Condi	ions:C	CEAR	
Depth	to	Sed in	ent	1'		
Sedine	ent	Type:	SAN	vo & Grz	AU (57	

Time of Sampling 0930

FractionPreservative/AmountSSICESVICERemarks:

G, GOML G, GOML

Date 2-12-90 Signature

Station # NA Sample # 6

Dace <u>2-12-90</u> Projec: <u>FT, STEWART-HUNTER</u> HAF Field Personnel <u>T. TRENT</u> / J. BUTURFP

STATION DESCRIPTION:

Sample Method:

Water	Qu	ality Cond	itions:	NA	
Depth	to	Sediment	NA		
Sedime	nt	Type:			
		NA			

Time of Sampling 1030

FractionPreservative/AmountContainer TypeVFCEG., 60 mLVFCEG., 60 mLVFCEG., 60 mLVFCEG., 60 mLRemarks:JRJP BLANK

Signature Date 2-12-90

NA Station # Sample #

Date	2-12-90
Project	FT. STEWART - HUNTER AAF
Field P	ersonnel T. TRONT / J. BUTURFR

STATION DESCRIPTION:

Sample Method:

Water Quality Conditions: N/4 Depth to Sediment \_\_\_\_\_N/A --Sediment Type: N/A

Time of Sampling 1045

Fraction	Preservative/Amount	Container Type
ŝ	ILE HNO,	GIL
V	ICE	P, IL
V	TCE	G. GOWL
Remarks:	RINSE BLANK	G, GOML G, GOML
	KINSE ISLANK	6, 60 ml

Signature Hen Date 2-12-90

Station # 50-3Sample # 8

Jace 2-12	-90
Projec: FT. ST	EWARS - HUNTER MAF
Field Personnel	T.TRENT/J. BUTUREF

STATION DESCRIPTION:

Sample Mechod: STAINLESS STEEL BUWL & SPOON

Water Quality Conditions: CLOGA Depth to Sediment \_\_\_\_\_ Sediment Type: SAND & GRAJEL

Time of Sampling  $_0930$ 

Fraction Preservative/Amount Container Type 55 SV . ICE . G, 402. BAMPLE FOR MRD LAB OMAHA, NE

Signature Jen Jos Date 2-12-90

Station # TRIP BLANK Sample # 9

Dace 2-13-80 Projec: F.T. STEWART- HUNTER HAF Field Personnel T. TRENT/S. BUTURFF

STATION DESCRIPTION: N/A

Sample Method: NA

Water	Qu.	ality	Condi	tions: d	NA
Depth	to	Sed im	ent_	NA	
Sedime	nt	Type:	NA		

Time of Sampling 1600

Fraction	Preservative/Amount	Container Type
V	ICE	G. 60 mL
V	TCE	6. 1.
V	ICC	6,60mL
Remarks:	102024 68:02	G, 60 mL
	SAMPLE FOR MRD LAS	3 OMAHA, NE

Signature Jem

Date 2-13-90

### ESE KEY TO FRACTION CODES 3/90

AIR:	CODE AA AO AV FL	<u>PRESERVATIVE</u> 4-Deg-C Exclude Light Exclude Light Keep Upright	<u>CONTAINER</u> Various Sorbent Charcoal Cassette	<u>ANALYSIS TYPE</u> Various Organic Volatiles Various	<u>HOLDING TIMES</u> Various 14 Days 14 Days Various
SOILS:	SS SV	4-Deg-C 4-Deg-C	G, 500 mL G, 60 mL	All excl. Vol. Volatiles	7-28 Days 7-14 Days
WATER:	AL	4-Deg-C(T)	G,2x60 mL*	Aldicarb	14 Days
	В	4-Deg-C;NaOH,pH>12		Cyanides	14 Days
	С	4-Deg-C	P, 1-4 L	Var.Inorganic	1-28 Days
	CL	4-Deg-C	G, 1-4 L	Chlorophyll	1 Day
		(Pref d Filtered & Fro.	zen at <0-Deg-C	C) 1 2	,
	EC	4-Deg-C(T)g	G, 1 L	Chlor'd Pests	7 Days
	ED	4-Deg-C(T)	G,2x60 mL*	EDB, DBCP	14 Days
	F		P, 4 L	Collection prior to Fie	eld Filtering
	FI	4-Deg-C(T)	G, 1 L	GC/FI Organic	7 Days
8 H	FM	Formaldehyde	P/G,500mL	"Quats"	28 Days
*	FP	4-Deg-C(T)	G,3x60 mL*	GC/FP Organic	14 Days
	H	Zn-Acet;NaOH,pH>10		Sulfides	7 Days
12	HB	4-Deg-C(T)	G, 1 L	Chlor'd Herbs	7 Days
	LC	4-Deg-C	G, 1 L	HPLC Organics	7 Days
	M	4-Deg-C(T)	P, 250 mL	Bacteriologic	1 Day
Υ.	MS	4-Deg-C(T)	G, 1 L	GCMS Extr.Org.	7 Days
	N	HNOypH<2	P, 1 L	Metals (Total)	180 Days
				Mercury (Total)	28 Days
	NF	HNOypH<2	P, 1 L	Metals (Dissolved)	180 Days
	NC	15 0	· · ·	Mercury (Dissolved)	28 Days
4		4-Deg-C	G, 1 L	Nitrocellulose	7 Days
		4-Deg-C	G, 1 L	GC/NP Organic	7 Days
	0	4-Deg-C;H2S0,pH<2	G, 1 L	Oil&Grease, TRPH	28 Days
	OD	4-Deg-C	G, 1 L	Odor	2 Days
	R	HNO <sub>y</sub> pH<2	P, 1-4 L	Radionuclides	180 Days
		4-Deg-C;H <sub>2</sub> S0, pH<2	P, 1 L	Nutrients	28 Days
		4-Deg-C(T)	G, 1 L	Pest(Antiq'd)	7 Days
		4-Deg-C(T)	G,3x60 mL*	Halogen, Vols	14 Days
	VP	4-Deg-C;HCL,pH<2(T)		Aromatic Vols	14 Days
		4-Deg-C(T)	G, 1 L	Orgs, FPD Extr's	7 Days
		4-Deg-C(S)	G,2x250mL*	TOX(USATHAMA)	7 Days
	XP ·	4-Deg-C;H2SO, pH<2(S)		TOX	7 Days
	Z	4-Deg-C;H2S0, pH<2	G, 1 L	Total Phenols	28 Days
OTHER:	OL 1	None	G,10-100mL	Organic-Oil	14 Days
		AA	· · · · · · · · · · · · · · · · · ·	Frozen Tissue	Various
		<b>0</b> -			

FOOTNOTES: (T) - Add Sodium Thiosulfate (Na<sub>2</sub>S<sub>2</sub>O<sub>3</sub>) If Res.Cl Present (0.25g/L) (S) - Add Sodium Sulfite (Na<sub>2</sub>SO<sub>3</sub>) If Res.Cl Present (0.1M, 1 mL/L). \* - Volatiles Bottles (VOAs) With Teflon-Lined Rubber Septa.

#### INSTRUCTIONS FOR SAMPLING AND SHIPPING

-Plastic (P) Containers May Be Rinsed With Sample; Do Not rinse Glass (G) -Fill Completely, Especially For Volatiles (Fill These Slowly; Achieve

Positive Meniscus; Cap; Invert; Check for Air Bubbles; Top Off If Needed.

-Preserve With Reagents Provided As Instructed Above (VP's Are Pre-Preserved) -Fill-out Logsheet/Chain-of-Custody. Indicate: Sample Number (\*) and Fractions

Collected; Dates/Times of Collection & Shipment; Appropriate Field Notes;

Be Sure To Sign Bottom of Each Page Where and As Indicated.

-Ship With Bagged Ice in Ice-chest By Express Carrier To Lab Coordinator's Attention.

Source: ESE, 1990.

PDs: JMH01\Practice Key

## APPENDIX B

to

# Groundwater Monitoring Plan - Appendix B to Closure Plan

# BORING LOGS

BB-1

Pro Dri Dri Log	Hunter Army Airfield Fort Stewart, Savannah, GALog of Boring No.HMWClient:US Army Corps of Engineers, Kansas City DivisionBoring Started: Boring Completed: Boring Diameter:Project Number:S912015GBoring Completed: Boring Diameter:Drilling Contractor:Layne Environmental ServicesBoring Diameter: Well Casing Diameter: Type of Drill Rig: Drilling Method:								3/4/92 3/4/92 8 inch					
Elevation	Depth	Samp Type	Samp Rec ft	PID ppm	Blows Per 6"	Well Construction	Li thology	MATERIAL DESCRIPTION		Bl 8 16 PIC	c Pent istanc ows/ft 5 24 (ppm 0 \$00	; × 3/2 n)		
ž			0,		2 5 5			(SM) SAND, silty, fine-grained, dark brown, moist - - 4 ft - becomes orangish-yellow, wet	2					
	5	CS	5.0	3	1									
	10— — — —	CS	5.0	0				(SM-ML) SAND AND SILT, intermixed silty sand and sandy silt, fine-grained sand, bluish-gray, wet, micaceous BORING TERMINATED AT 14 FT BGS	<u></u>					
					5			WELL CONSTRUCTION DETAILS Well stickup from surface to 2.0 ft AGS Volclay grout interval from surface to 1.5 ft BGS Sand filter pack from 1.5 to 14.0 ft BGS Well screen interval from 3.0 to 13.0 ft BGS Pipe and well screen material = Sch 40 PVC Pipe and well screen diameter = 2 inch Well screen slot size = 0.010 inch						
			•											
			i.											
SS	= Spli	tspoon		CS	= CMS	Conti	nous Sa	mpler PID = Photoioniza	tion 1	Detect	or (H)			

• • • •

Fort Stewart, Savannah, GAClient:US Army Corps of Engineers, Kansas CityProject Number:3912015GDrilling Contractor:Layne Environmental ServicesDriller:D. NicholsLogged By:G. FosterLocation:					12015G syne Env Nichols			Boring Completed:	3 8 2 N	/3/92 /3/92 inch inch Iobile Iollow	B-57	
Elevation	Depth	Samp Type	Samp Rec ft	MD PPM	Blows Per 6"	Well Construction	Lithology	MATERIAL DESCRIPTION		Blo 8 16 PID	istanc ows/ft 24 	:e X 32 n)
Ш	1					Ö	<b>لہ</b> 1993	(SM) SAND, silty, dark brown, fine-grained, moist	1	00 20	300	400
	_	CS	4.1	8		48	-	(SM) SAND, silty, dark brown, ine-grained, moist		$\vdash$	+	+
	-						-	· · · · · · · · · · · · · · · · · · ·			+	+
	-					I		2				
7	5.	-		_		目		4 to 5 ft - becomes tan mottled with gray	<b>_</b>			
		CS	3.9	0		目	-	5 ft - becomes fine- to medium-grained, light to medium gray, wet	-	$\left  - \right $		$\rightarrow$
	-					目	-	× .	$\vdash$		-+	+
	-						-					_
	-					目			<b>_</b>			
=	10-	CS	3.5	0					Ϊ		_	_
				8		目	-				+	-
	-					日	-111	анан алан алан алан алан алан алан алан	-	$\left  - \right $		-
	-							(SM-ML) SAND-SILT, intermixed silty sand and				
	15				-			sandy silt, fine-grained sand, greenish-gray, wet,				
	Ş.							BORING TERMINATED AT 15 FT BGS		24 - 14		
12 1	e K							WELL CONSTRUCTION DETAILS Well stickup from surface to 2.0 ft AGS Volclay grout interval from surface to 1.5 ft BGS Sand filter pack from 1.5 to 15.0 ft BGS Well screen interval from 3.0 to 13.0 ft BGS Pipe and well screen diameter = 2 inch Pipe and well screen material = Sch 40 PVC Well screen slot size = 0.010 inch				
									ŀ			
					*				1			
												<u>а</u>
cc	= Spli	tspoon		CS	= CMS	Conti	nous S	PID = Photoioniza	tion	Detect	or (H	Nu)

Dril Dril Log	ject Nu lling Co	ontract	or:	39 La D.	S Army 12015G yne Env Nichols Foster	ironm		eers, Kansas City Division rvices Boring Completed: Boring Diameter: Well Casing Diameter: Type of Drill Rig: Drilling Method:	3/ 8 2 M			
Elevation	Depth	Samp Type	Samp Rec_ft	PID PPm	Blous Per 6"	Well Construction	Lithology	MATERIAL DESCRIPTION	8	Res Blo 16 PID	c Pen sistand ows/f 3 24 0 (ppr 0 30	ce ft × 1 32 m)
	1 1 1 1	CS	2.2	15				(SM) SAND, silty, medium-brown becoming dark brown with depth, fine-grained, moist 4 ft - grades to medium gray			2 2 2	
¥	5	CS SS	3.0	50	1-1				*-			
		SS SS	2.0 2.0	175 125	2-3 1-4 5-6 6-11 29-14			9 to 10 ft - wood in sample interval 10 ft - becomes brown to orangish-brown, wet		× 0 0-		
	15	1	d 					BORING TERMINATED AT 15 FT BGS WELL CONSTRUCTION DETAILS Well stickup from surface to 2.5 ft AGS				
3.00 10 10					134			Volclay grout interval from 2.5 to 3.0 ft BGS Sand filter pack from 3.0 to 15.0 ft BGS Well screen interval from 5.0 to 15.0 ft BGS Pipe and well screen diameter = 2 inch Pipe and well screen material = Sch 40 PVC Well screen slot size = 0.010 inch		E K		
					e.					-		
SS	= Spl	itspoor		CS	S = CMS	Cont	inous Sa	mpler PID = Photoioniza	tion	Detec	tor (J	 HNu)

## APPENDIX C

to

# Groundwater Monitoring Plan - Appendix B to Closure Plan

# MISCELLANEOUS FORMS

BC-1

Well	Development				Well 1	No			
	Date	0	_ Time _						
	Well Installation Date								ft
	Depth of Well								
	Diameter of Well					1			
	Method of Evacuation								
	Depth from which well was	pumpe	ed		-	-			ft
	Distance from top of pipe								ft
	6 B		Before		After		24	hours Af	ter
	Held length	÷							ft
	Wet length		-						
	Distance to water								
	Depth to sediment								
	Appearance of water								
	Approx. pumping rate Characteristics of sodiment_			. ,			; pm	8	
			Bucket 1					After	8
	рĦ	_							
	Conductivity		1 2 2						
-	Temperature		<del></del>						
	4								
No. c	of 2-1/2 gal buckets pumped	12	3 4 5	56	78	9 10		<del></del>	
	Total well volume before pu		~					~ 1	
	Total volume pumped					8		_ gal	
	iocal aorome humber							- 541	
Semn 1	e collected - 1 cubitainer	afte	r numning	1ab	eled	(1 <b>2</b> ))			
	iption of surge technique _							-	-
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	· · ·		Read an	nd Un	derstoo	d By:			
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						1	9	÷	_
Signe	d		Signed		5	2	De	ite	

# MONITOR WELL WATER LEVEL MEASUREMENTS

	Sheet of	
Site	Measured By	
Client	Reference Mark:	
Project Number	Top of well casing	
-	Ground surface	

8 <b>-</b> 11			Tape Re Held	wet	Depth	
Well	Date	Time	Length	Length	Depth To Water	Comments
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# WELL SAMPLING DATA FORM

Well Number:			Da	ate: _		TI	me:		
Boring Diame	ter:			Well	Casing	Diameter			
Annular Spac	e Leng	th: _			St	lckup: _			
WATER LEVEL			•						
Held: _									
		21N							
DTW: _				Тор	of Casin	ng			
COLUMN OF WA	TER IN	WELL							
	Casin	g Leng	gth:						
DTh	I Top o	f Casi	.ng:						
Column of	Water	in We	211:						
VOLUME TO BI	REMOV	ED							
Gallons	per fo	ot of	A.S. (f	rom cha	art)			•	
Column o	of Wate	r or l	Length of	A·S·	(whiche	ver is 1	ess)		
Volume o	of Annu	lar S	pace					•	
Gallons	per fo	ot of	Casing						25.02
Column	of Wate	r						x	
Volume o						31			
Total Vo	olume	(Volu	me of A.S	. + Vo	lume of	Casing)		•	
Number	of Volu	imes to	o be Evac	uated	*			X	
			Evacuated					•	
Method of P	urging	(pum	p, bailer	, etc.	):	1494257368 62			
FIELD ANALY	SES		Start			Mid		En	٥
Time		2000			<u> </u>	<u></u>			
pH		-				×			
Conduct	ivity	s <del></del>				2			
Tempera		-							
Total Volum	e Purg	ed:		gall	ons	N			
Sample Date	/Time:				Sample	Number:	<u></u>		2
FRACTIONS							100000	-	2
VP	V	N	NF	C	0	S	UP	Z	B
CF	F	H	CL	M	P	R	RP	Т	RS
5 8 8									
		*							
Signed/Sam	ler:	1.0095					Dat	:e:	

Signed/Reviewer: \_\_\_\_\_

Date: \_\_\_\_\_

### ENVIRONMENTAL SCIENCE & ENGINEERING WATER RESOURCES DIVISION Hydrolab Calibration Form II

nstrument Serial Numb	er				
attery (Voltage) ——		Vdc.			
Parameter		Initial f	Reading	Final Reading	
			Q		
emperature		er <del>heren a</del> n er er er er er	c		
onductivity: (uS/cm)	1413				
High Conc. Stnd -	718			718	
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Low Conc. Stnd			k		
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H: 7.00 Buffer					
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10.00 Buffer	2	, 			
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Saturation at	: Air Ter	operature f	or		
Conditions -				5 100	
or Office Use Only!		/ /b/=			
Clean Conductivity Pr Change pH Buffer ?		Yes/No			
Change D.O. Membrane		Yes/No			
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	DEPTH, FT.	SAMPLE INTERVAL	SAMPLE # AND TYPE	BLOWS PER 6 INCHES	DESCRIPTION AND REMAR	SX DEPTH, FT.	USCS SYMBOL AND INTERVAL	WELL SKETCH	-
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Environmental Science & Brigineering, Inc. 5 miles west of 1-75 on 59	Colores	eide		Reilnquished By: Reilnquished By:

APPENDIX C AIRSTRIP MODELING

JOB HUNTER AAFTA Environmental of 4 SHEET NO. Science & CALCULATED BY OWISE DATE 7/23/93 Engineering, Inc. CHECKED BY DATE \_ P.O. Box 1703 904-332-3318 Gainesville, Florida 32602-1703 Fax 904-332-0507 SCALE Design Mode, A RSTRIP the packed 12 PURPOSE: EG TOA SIZE tin ipr required of banks provide operativo to ranters Da reatme benze adeq んと groundwade contam inated 660 65°F berzene INFluent Assumptions: 0 ug 25 Flow = gpm AIRSTRIP wi MINIMUM allow ONLY Ġ. 0.264 MGD 183 Flow of & pm díame we to SÓ give NAU 10 mie RUL 59 10ading 25 ro ð P tou fy0 día 9 of packing A Wratcon at aN 15 adequate 50: vid freatment 0's 16 ber -109 16 H20 ugle 660 660 16 Beryze × 8,2 16 H20 gal 60 AF 660 10 16 H30 gal 0.008 25 × = 0.2 18 Jas = benzene
°Concentration In : 660.0 ug/L p ¤ Benzene ¤ P-Jaeger Tripacks 2.0 inch °Atmospheric Pressure 1.0 atm D : : 65.0 deg F °Liquid Loading Rate 9.0 gpm/ft^2 ¤ ¤ Design Temperature : <sup>o</sup>Minimum A/W Ratio D Minimum Packing Depth : 5.0 feet : 10.0 <sup>o</sup>Maximum A/W Ratio Maximum Packing Depth : 25.0 feet : 50.0 ¤ D p D Concentration Remaining (ug/L) n p Ø A/W = 30D <sup>D</sup> Packing Depth A/W = 10A/W = 20A/W = 40A/W =50 (feet) n a D p 103.6 ø 5.0 191.0 135.2 114.5 96.8 D ¤ 10.0 72.4 32.5 22.3 17.8 15.3 p 4.4 3.1 2.4 n p 15.0 29.8 8.1 0.9 0.5 D d 20.0 12.7 2.0 0.4 0.1 D 0.2 0.1 D 25.0 5.4 0.5 D D D ¤ R 8.5 10.6 2.1 4.3 6.4 ¤ dP (" H2O/ft) <.06 <.06 <.06 <.06 <.06 D ° F1 Help ° F7 Quit program ¤ F10 Toggle to Metric units D ¤ F9 Continue with design procedure ° F3 Main menu • Esc to go back D ¤ AIRSTRIP Release 1.2 Copyright 1988 D n Summary of Selected Design p D p D : Benzene ¤ Contaminant p <sup>D</sup> Concentration In : 660.0 ug/L ¤ ¤ Concentration Out : 2.4 ug/L ¤ ¤ Percentage Removed 99.6 % : p Packing : P-Jaeger Tripacks 2.0 inch n <sup>D</sup> Water Temperature D : 65.0 deg F. n ¤ Atmospheric Pressure 1.0 atm : ¤ : 15.0 feet p Packing Depth D D Liquid Loading Rate 9.0 gpm/ft^2 : p ¤ Air/Water Ratio : 50 p D Stripping Factor : 10.6 ¤ Air Pressure Gradient : <.06 " H2O/ft D ŋ σ ¤ n p ¤ n D ¤ F10 Toggle to Metric units • F1 Help • F7 Quit program p • F3 Main menu p ¤ F6 Save design "P" print report • Esc to go back 

# 3/4

# \*\*\*\*\*\* ANALYSIS OF STRIPPING

PROJECT : Hunter AAFTA

ENGINEER : Gary Wise

DATE : 7/23/1993 PAGE : 1/2

### PHYSICAL CONSTANTS

Design temperature	:	65.0	degrees F.
Density of water	:	62.3	lb/ft <sup>3</sup>
Density of air	2. 	0.0756	lb/ft^3
Viscosity of water		7.03E-04	lb/ft.s
Viscosity of air		1.19E-05	lb/ft.s
Surface tension of water	:	73	dyne/cm
Atmospheric pressure	:	1.00	atm

# CONTAMINANT PROPERTIES

Name	:	Benzene	Э	
Molecular weight	:	78.1	g/mol	
Boiling point	:	176	degrees	F.
Molal volume at boiling point	:	0.0960	L/mol	
Henry's Constant	:	0.23000		
Temperature constant	:	1849	deg K	
Molecular diffusivity in air	:	9.98E-05		1.53
Molecular diffusivity in water	:	9.15E-09	ft^2/s	

### PACKING PROPERTIES

Name	:	Jaeger	r Tripacks
Packing Material	:	Plasti	lc
Nominal Size	:	2.00	inch
Specific Area	:	47.9	ft <sup>2</sup> /ft <sup>3</sup>
Critical surface tension	:	33	dyne/cm
Packing depth	:	15.0	ft
Air friction factor	1	15	

4/4

#

\*\*\*\*\*\* ANALYSIS

# STRIPPING TO

TOWER \*\*\*\*\*\*

PROJECT : Hunter AAFTA

ENGINEER : Gary Wise

DATE : 7/23/1993 PAGE : 2/2

## LOADING RATES

Water mass loading rate	:		lb/ft^2.s
Air mass loading rate	:	0.076	lb/ft^2.s
Water volumetric loading rate	:		gpm/ft <sup>2</sup>
Air volumetric loading rate	• <b>1</b> •		gpm/ft <sup>2</sup>
Air pressure gradient	:	<.06	" H20/ft
Volumetric air/water ratio	•	50.0	
Stripping factor	:	10.6	

OF

## MASS TRANSFER PARAMETERS

Percentage of packing area wetted	:	41.0	8
Wetted packing area	:	19.6	ft <sup>2</sup> /ft <sup>3</sup>
Transfer rate constant in water	:	0.000479	ft/s
Transfer rate constant in air	:	0.014023	ft/s
Overall transfer rate constant	:	0.000413	ft/s
Overall mass transfer coefficient		0.0081	1/s
NTU	:	6.0799	(i <sup>38</sup>
нти	:	2.4671	ft .

### CONTAMINANT REMOVAL

Influent concentration		660.0 ug/L
Effluent concentration	:	2.4 ug/L
Fraction removed	:	99.6 %
Mass of contaminant removed	:	0.07086 lb/ft^2.day
Concentration in airstream	:	0.03459 mg/ft <sup>2</sup> .ft <sup>3</sup>

\* Expressed per unit of stripping tower cross-sectional area
 # Expressed per unit of tower length

APPENDIX D

HYDROGEOLOGIC CALCULATIONS

HUNTER 101 3912015G-0100-3130 Environmental SHEET NO. Science & GWise DATE 8/7/92 Engineering, Inc. CALCULATED BY DATE CHECKED BY Gainesville, Florida 32602-1703 Fax 904-332-0507 P.O. Box 1703 904-332-3318 SCALE available slue tort Ja Purpose culate surface elevation and trom Jata Diezometric 1974 Reference & Thornburn, Peck Hanson. 1 Velocity Linear groundwater Calculation: -low gradient I = conductivit. K = hydraulic assumed to be porosit. 30 % n velocity linear Flow V K n 60min/hr X ft/yr 24 hr/day x 365 day (f+/mid)× E K (F/min WELL NO. I (F)/F+ (F+/min ft YN 5 6x10 18.8 0.0097 (low) 0.00111 (low) 3. HMW-4 0.00133 (avg) 6.8× 10-5 35.9 (shallow) 0.0154 (ava) 9.7× 10-5 0.00155 (high) 50.7 0.0187 (high) 28,7 10 0.0097 (10W) 0.00169 (low) 5.5 x Hmw-3 7.0 x 10-5 (avg) 0.00177 (avg) 36.8 0.0119 (deep) 8.0 × 10-5 0.00184 (high) 42,2 (high) 0.0131 ESE - 38362 D-1





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APPENDIX E

# ANALYTICAL RESULTS

Soil/Sediments

PARAMETERS	-	BH-10	10	BH-11	11	BH	BH-12		BH-13		QA ALCOHOL	QA WASH
UNITS	•	0-1 FT.	7.5-8.5 FT.	0-1 FT.	7.5-8.5 FT.	0-1 FT.	6.5-7.5 FT.		0-1 FT.	6.0-7.5 FT.		
2 METHYLNAPHTHALENE	UG/KG	<1.00	19000.00	<1.00	12000.00	<1.00	10000.00	<2.00	<1.00	<1.00	<1.00	<1.00
ARSENIC	0C/G	5.99	2.00	13.90	3.88	4.00	<1.96	11.98	7.75	3.94	<1.96	<1.96
BARIUM	UG/G	64.40	9.19	33.50	18.10	7.19	8.12	27.10	19.80	8.28	<0.01	<0.01
BIS (2 ETHYLHEXYL) PHTHALATE	UG/KG	<1.00	1.70	<1.00	00.009	<1.00	300.00	<3.00	<1.00	NRQ	<1.00	<1.00
CADMIUM	0C/G	<1.98	<1.98	1.99	<1.98	<1.98	<1.98	0-02	3.87	<1.98	<1.98	<1.98
CHROMIUM	0/9N	12.80	3.96	4.16	3.96	5.19	<3.96	2.84	9.10	<3.96	<3.96	<3.%
DI-N-LATEBUTYLPHTHALATE	DG/KG	<1.00	1300.00	<1.00	600-00	<1.00	2400.00	<2.00	<1.00	<1.00	<1.00	<1.00
DIETHYLPHTHALATE	UG/KG	<1.00	<1.00	<1.00	<1.00	<1.00	200.00	<2.00	<1.00	<1.00	<1.00	<1.00
FLUORENE	UG/KG	<1.00	400.00	<1.00	<1.00	<1.00	200.00	<3.00	<1.00	MRQ	41.00	<1.00
LEAD	9/9N	645.00	35.90	1163.70	NRQ	102.00	19.30	1179.80	1185.00	13.80	1.98	<1.98
MERCURY	0/9N	0.40	0.39	0.38	0.38	0.40	0.38	0.79	0.38	0.39	<0-04	<0-04
NAPHTHALENE	UG/KG	<1.00	10000.00	<1.00	7000.00	<1.00	0 5800.00	<2.00	<1.00	<1.00	0 <1.00	<1.00
PHENANTHRENE	UG/KG	<1.00	00.009	<1.00	<1.00	<1.00	0 200.00	<3.00	<1:00	NRQ	a <1.00	<1.00
SELENIUM	D/DN	<0.20	<0.20	<0.20	<0.20	62*0	9 0.60	0.22	0-33	<0.20	0.20	<0.20
STLVER	DG/G	<3.99	<3.99	3.99	<3.99	3.99	9 <3.99	<7.98	<b>66</b> .5>	3.99	3.99	<3.99

Table 1-1. Analytical Parameters Detected in Soil Samples in 1987, Hunter AAFTA

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Source: ESE.

Table 1-2. Analytical Parameters Detected in Soil/Sediment Samples in 1990, Hunter AAFTA

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PARAMETERS	UNITS				SOIL						SEDIMENT	ENT		
	8	1-8SH	HSB-2	HS8-3	4-8SH	KSB-5	9-8SH	TRPBLK	s0-1	SD-2	SD-3	ange-gs	TRPBLK	RINSEBLK
		8-10 FT.	3-5 FT.	6-8 FT.	2-4 FT.	5-8 FT.	8-10 FT.		۲ ۲					
1		02/12/90 02/13/90		02/13/90	02/13/90 02/13/90	02/13/90	02/13/90	02/13/90	02/12/90	02/12/90	02/12/90	02/12/90 02/12/90 02/12/90 02/12/90 02/12/90	02/12/90	02/12/90
ž		17:05	07:45	08:35	09:35	11:35	12:45	12:00	00:60	09:20	09:30	06:30	10:30	10:45
2MOI STURE	ZUET UT	5.00	12.40	16.20	14.00	21.60	16.30	NRQ	13.90	26.20	19.70	19.80	NRG	NRG
1,1,1-TRICHL'ETHANE	UG/KG-DRY	<1.40	<1.50	<200.00	<1.60	<2100.00	<1.60	NRQ	<1.50	<1.80	<1.60	<1.60	NRO	NRQ
1,1,1-TRICHL'ETHANE (EPTOX)	NG/L	NRQ	NRQ	NRQ	NRO	NRG	NRG	<1.60	NRQ	NRG	NRQ	NRG	<1.60	<1.60
1,1,2,2-TETRACHLORO ETHANE	UG/KG-DRY	<1.60	<1.70	<230.00	<1.80	<2400.00	<1.80	NRQ	<1.70	<2.10	<1.90	<1.90	NRQ	NRQ
1,1,2,2-TETRACHLORO ETHANE (EPTOX)	NG/L	NRQ	NRQ	NRQ	NRQ	. NRQ	NRG	<1.50	NRQ	NRQ	NRG	NRQ	<1.50	<1.50
1,1,2-TRICHL'ETHANE	UG/KG-DRY	<1.70	<1.80	<240.00	<1.90	<2500.00	<1.90	NRO	<1.80	<2.20	<2.00	<2.00	NRG	NRG
1,1,2-TRICHL'ETHANE (EPTOX)	UG/L	NRQ	NRQ	NRQ	NRQ	NRQ	NRO	<0.87	NRQ	NRQ	NRG	NRG	<0.87	<0.87
1,1-DICHLOROETHANE	UG/KG-DRY	<090	<0.97	<130.00	<1.00	<1400.00	<1.00	NRO	<0.98	<1.20	<1.00	<1.00	NRQ	NRO
1,1-DICHLOROETHANE (EPTOX)	NG/L	NRG	NRQ	NRQ	NRQ	NRO	NRQ	<0.85	NRQ	NRQ	NRQ	NRG	<0.85	<0.85
1,1-DICHLOROETHENE	UG/G-DRY	<1.30	<1.40	<180.00	<1.40	<1900.00	<1.40	NRQ	<1.40	<1.60	<1.50	<1.50	NRQ	NRO
1,1-DICHLOROETHYLENE (EPTOX)	NG/L	NRO	NRQ	NRO	NRQ	NRG	NRQ	<1.20	NRQ	NRQ	NRQ	NRQ	<1.20	<1.20
1,2-DICHLOROETHANE	UG/KG-DRY	<0.92	<1.00	<130.00	<1.00	<1400.00	<1.00	NRQ	<1.00	<1.20	<1.10	<1.10	NRQ	MRG
1,2-DICHLOROETHANE (EPTOX)	1/9N	NRQ	NRQ	NRQ	NRQ	NRO	NRQ	<0.87	NRQ	NRG	NRG	NRQ	<0.87	<0.87
1,2-DICHLOROETHANE-D4	UG/KG-DRY	58.00	60.00	54.00	61.00	48.00	62.00	NRQ	59.00	72.00	29.00	58.00	NRQ	NRQ
1,2-DICHLOROETHANE-D4 (EPTOX)	NG/L	NRO	NRG	NRG	NRQ	NRG	NRG	NRG	NRO	NRQ	NRG	NRG	NRG	47.00
1,2-DICHLOROETHENE, TOTAL	UG/KG-DRY	<1.37	<1.49	<194.00	<1.53	<2070.00	<1.54	NRO	<1.49	<1.76	<1.60	<1.60	NRG	NRG

23.51.51.1

Table 1-2. Analytical Parameters Detected in Soil/Sediment Samples in 1990, Hunter AAFTA, Continued, Page 2 of 9

					enti						SEDIMENT	ENT		
PAKAME I EKS	STINU				2016		, uon	1 1001	5	C-13	50-3	CI-ZUID	TEPRIK	RINSFRIK
		HSB-1	HSB-2	HSB-3	HSB-4	HSB-5	HSB-6	TRPBLK	1-0s	2-05	c-18	JUUC-US		TUDEDLA
	el	8-10 FT.	3-5 FT.	6-8 FT.	2-4 FT.	5-8 FT. 8	8-10 FT.					2		
	-	02/12/90	02/13/90	02/13/90	02/13/90	02/13/90 02/13/90 02/13/90 02/13/90 02/13/90	05/13/90		02/12/90	02/12/90	02/12/90	02/12/90	02/12/90	02/12/90
		17:05	07:45	08:35	09:35	11:35	12:45	12:00	00:00	09:20	06:30	09:30	10:30	10:45
1,2-DICHLOROETHENE, TOTAL (EPTOX)	UG/L	NRQ	NRQ	NRQ	NRO	NRG	NRO	<1.30	NRO	NRG	NRG	NRQ	<1.30	<1.30
1,2-DICHLOROPROPANE	UG/KG-DRY	<1.00	<1.10	<140.00	<1.10	<1500.00	<1.10	NRQ	<1.10	<1.30	<1.20	<1.20	NRQ	NRQ
1,2-DICHLOROPROPANE (EPTOX)	UG/L	NRQ	NRQ	NRQ	NRQ	NRQ	NRQ	<0.97	NRQ	NRG	NRQ	NRQ	<0.97	<0.97
2,4,6-TRIBROMOPHENOL	MG/KG-DRY	6750.00	7620.00	9150.00	8940.00	9730.00	8490.00	NRG	7200.00	7820.00	7370.00	1530.00	NRQ	NRG
2,4,6-TRIBROMOPHENOL (EPTOX)	UG/L	NRQ	NRG	NRQ	NRQ	NRQ	NRQ	NRG	NRG	NRQ	NRG	NRG	NRQ	120.00
2-BUTANONE	UG/KG-DRY	, <9°.96	<10.80	<1410.00	<11.10	15100.00	<11.20	NRG	<10.90	<12.80	<11.60	<11.70	NRQ	NRG
2-BUTANONE (EPTOX)	UG/L	NRG	NRG	NRG	NRQ	NRQ	NRO	<9.44	NRO	NRQ	NRO	NRG	<9.44	<9.44
2-FLUORBIPHENYL (EPTOX)	ng/L	NRG	NRQ	NRG	NRQ	NRQ	NRG	NRQ	NRQ	NRQ	MRG	NRQ	NRQ	75.00
2-FLUOROBIPHENYL	UG/KG-DRY	3300.00	3880.00	4510.00	4250.00	4490.00	3640.00	NRO	4030.00	3990.00	4460.00	4530.00	NRO	NRQ
2-FLUOROPHENOL	UG/KG-DRY	8940.00	9410.00	10200.00	10600.00	10400.00	10300.00	NRO	8610.00	8610.00 10000.00	9870.00	9500.00	NRQ	NRG
2-FLUOROPHENOL (EPTOX)	NG/L	NRG	NRG	NRG	NRG	NRQ	NRQ	NRQ	NRG	NRQ	NRG	NRQ	WRO	110.00
2-HEXANONE	UG/KG-DRY	<3.30	<3.60	<470.00	3.70	<5000.00	3.70	NRG	<3.60	<4.20	3.%	<3.90	NRG	NRG
2-HEXANONE (EPTOX)	NG/L	NRG	NRQ	NRG	NRQ	KRQ	NRG	<3.10	NRG	NRQ	NRO	NRG	<3.10	3.10
4-METHYL-2-PENTANONE	UG/KG-DRY	<2.83	₹0°2	<400.00	3.15	<4270.00	3.17	NRQ	<3.08	3.63	3.30	3.31	MRQ	NRO
4-METHYL-2-PENTANONE (EPTOX)	∩c/L	NRQ	NRQ	NRG	NRQ	NRQ	MRQ	≪3.00	NRQ		NRQ	-	<3.00	<3.00
ACENAPHTHENE	UG/KG-DRY	<130.00	300.00	<150.00	<150.00	<160.00	<150.00	NRQ	1100.00		<170.00 <1600.00	4900-00	NRO	NRG

Table 1-2. Analytical Parameters Detected in Soil/Sediment Samples in 1990, Hunter AAFTA, Continued, Page 3 of 9 •

PARAMETERS	UNITS				SOIL						SED I MENT	ENT	-	
	20 20 J	HS8-1	HSB-2	HSB-3	HSB-4	6-8SH	9-8SH	TRPBLK	1-0s	SD-2	SD-3	SD-30UP	TRPBLK	RINSEBLK
12		8-10 FT.	3-5 FT.	6-8 FT.	2-4 FT.	5-8 FT.	8-10 FT.							
		02/12/90 02/13/90		02/13/90	02/13/90 02/13/90 02/13/90	02/13/90	02/13/90 02/13/90	02/13/90	02/12/90	02/12/90	02/12/90	02/12/90	02/12/90	02/12/90
		17:05	07:45	08:35	09:35	11:35	12:45	12:00	00:60	09:20	06:30	09:30	10:30	10:45
ACENAPHTHENE (EPTOX)	NG/L	NRG	NRQ	NRG	NRQ	NRG	NRQ	NRG	NRG	NRG	NRQ	NRQ	NRO	<3.80
ACENAPHTHYLENE	UG/KG-DRY	<96.00	400.00	<110.00	<110.00	<120.00	<110.00	NRQ	<530.00	<120.00	3100.00	2000.00	NRO	NRG
ACENAPHTHYLENE (EPTOX)	ne/L	NRG	NRQ	NRO	NRQ	NRG	NRQ	NRG	NRG	NRO	NRG	NRQ	NRO	<2.70
ACETONE	UG/KG-DRY	<18.00	<19.00	<2500.00	<20.00	27000.00	<20.00	NRQ	40-00	110.00	120.00	<21.00	NRQ	NRQ
ACETONE (EPTOX)	UG/L	NRG	NRG	NRQ	NRQ	NRQ	NRQ	<17.00	NRQ	NRQ	NRQ	NRO	<17.00	<17.00
ANTHRACENE	UG/KG-DRY	<75.00	1300.00	<85.00	<83.00	<91.00	<85.00	NRQ	3000.00	<97.00	8200.00	9300.00	NRQ	NRG
ANTHRACENE (EPTOX)	NG/L	NRQ	NRQ	NRQ	NRQ	NRQ	NRG	NRQ	NRQ	NRQ	NRQ	NRG	NRQ	<2.10
ARSENIC, SED	MG/KG-DRY .	<0.48	<0.52	<0.54	0.65	0.85	<0.55	NRQ	<0.53	0.76	<0.57	<0.57	NRQ	NRQ
ARSENIC, TOTAL (EPTOX)	NG/L	NRO	NRQ	NRO	NRG	NRQ	NRG	NRO	NRQ	NRG	NRO	NRQ	NRQ	<2.30
BARIUM, SED	MG/KG-DRY	3.83	5.97	6.21	47.4	15.40	11.20	NRG	19.80	8.46	13.40	229.00	NRQ	NRG
BARIUM, TOTAL (EPTOX)	NG/L	NRQ	NRG	NRG	NRG	NRQ	NRG	NRG	NRG	NRG	NRQ	NRG	NRO	<1.70
BENZENE	UG/KG-DRY	<1.20	<1.30	<170.00	<1.30	<1800.00	<1.30	NRQ	<1.30	<1.50	15.00	31.00	. NRG	NRQ
BENZENE (EPTOX)	NG/L	NRQ	NRQ	NRO	NRQ	NRQ	NRQ	<1.10	NRQ	NRQ	NRQ	NRQ	<1.10	<1.10
BENZO(A)ANTHRACENE	UG/KG-DRY	<62.00	4900.00	<70.00	<68.00	<75.00	<70.00	NRQ	13000.00	<79.00	26000.00	33000.00	NRG	NRO
BENZO(A)ANTHRACENE (EPTOX)	NG/L	NRQ	NRQ	NRQ	NRQ	NRG	NRQ	NRG	NRQ	NRG	NRG	NRG	NRG	<1.80
BENZO(A)PYRENE	UG/KG-DRY	<180.00	3400.00	<210.00	<200.00	<220.00	<210.00	NRQ	9200-00		<230.00 18000.00 27000.00	27000.00	NRQ	NRG

Table 1-2. Analytical Parameters Detected in Soil/Sediment Samples in 1990, Hunter AAFTA, Continued, Page 4 Of 9

DADAMETEDS	UNITS				SOIL						SED I MENT	ENT		
		HS8-1	HSB-2	HSB-3	HSB-4	4SB-5	9-8SH	TRPBLK	s0-1	SD-2	SD-3	SD-3DUP	TRPBLK	RINSEBLK
		8-10 FT.	3-5 FT.	6-8 FT.	2-4 FT.	5-8 FT.	8-10 FT.							
Ŕ		02/12/90	02/13/90	02/13/90	02/13/90 02/13/90		02/13/90	02/13/90	02/12/90	02/12/90	02/12/90	02/12/90	02/12/90	02/12/90
ĥ		17:05	07:45	08:35	09:35	11:35	12:45	12:00	00:60	09:20	06:30	06:30	10:30	10:45
BENZO(A)PYRENE (EPTOX)	nc/L	NRQ	NRG	NRG	NRQ	NRG	NRQ	NRQ	NRG	NRQ	NRO	NRO	NRG	<5.20
BENZO(B)FLUORANTHENE	UG/KG-DRY	<130.00	5000.00	<150.00	<150.00	<160.00	<150.00	NRO	16000.00	<170.00	21000.00	27000.00	NRQ	NRQ
BENZO(B)FLUORANTHENE (EPTOX)	nc/L	NRG	NRG	NRQ	NRQ	NRQ	NRG	NRG	NRQ	NRG	NRG	NRQ	NRQ	<3.80
BENZO(GHI)PERYLENE	UG/KG-DRY	<74.00	2200.00	<84.00	<81.00	<89.00	<84.00	NRQ	6200.00	<95.00	13000.00	17000.00	NRQ	NRQ
BENZO(GHI )PERYLENE (EPTOX)	NG/L	NRQ	NRG	NRQ	NRQ	NRQ	NRQ	NRQ	NRQ	NRG	NRQ	NRQ	NRQ	<2.10
BENZO(K)FLUORANTHENE	UG/KG-ĎRY	<170.00	2500.00	<190.00	<180.00	<200.00	<190.00	NRG	7200.00	<210.00	<210.00 17000.00 29000.00	29000.00	NRQ	NRQ
BENZD(K)FLUORANTHENE (EPTOX)	NG/L	NRQ	NRQ	NRQ	NRQ	NRQ	NRQ	NRG	NRQ	NRQ	NRQ	NRQ	NRG	<4.70
BROMOD I CHLOROMETHANE	UG/KG-DRY	<1.00	<1.10	<150.00	<1.20	<1600.00	<1.20	NRQ	<1.10	<1.30	<1.20	<1.20	NRQ	NRO
BROMODICHLOROMETHANE (EPTOX)	NG/L	NRQ	NRQ	NRO	NRQ	NRQ	NRQ	<0.98	NRG	NRQ	NRO	NRQ	<0.98	\$
BROMOFLUOROBENZENE	UG/KG-DRY	52.00	46.00	62.00	50.00	54.00	50.00	NRQ	54.00	61.00	67.00	65.00	NRO	NRQ
BROMOFLUOROBENZENE (EPTOX)	1/5N	NRG	NRG	NRQ	NRG	NRQ	NRQ	NRQ	NRQ	NRG	NRQ		NRQ	45
BROMOFORM	UG/KG-DRY	<2.60	<2.80	<370.00	<2.90	<3900.00	<2.90	NRG	<2.80	3.30	3.00	§.8	NRG	MRG
BROMOFORM (EPTOX)	NG/L	NRG	NRQ	NRQ	NRG	NRG	NRO	<2.50	NRG	NRQ	NRG	NRG	<2.50	<2.50
BROMOMETHANE	UG/KG-DRY	<1.20	<1.30	<170.00	<1.40	<1900.00	<1.40	NRG	<1.30	<1.60	<1.40	<1.40	NRG	NRQ
BROMOMETHANE (EPTOX)	UG/L	NRQ	KRG	NRQ	NRQ	NRQ	NRQ	<1.20	NRQ	NRG	NRG	NRG	⊽	2
CADMIUM, SED	MG/KG-DRY	<0.37	<0*0>	<0.42	<0.41	<0.45	<0.42	NRG	<0.41	<0.47	50°44	<0.44	NRQ	NRG

Table 1-2. Analytical Parameters Detected in Soil/Sediment Samples in 1990, Hunter AAFTA, Continued, Page 5 of 9

Matrix         Matrix<												CED THENT	ENT		
HSB-1         HSB-2         HSB-3         HSB-4         HSB-5         HSB-5 <t< th=""><th>ETERS</th><th>UNITS</th><th></th><th></th><th></th><th>SUIL</th><th></th><th></th><th>Second Second</th><th></th><th></th><th>SCULF</th><th></th><th></th><th></th></t<>	ETERS	UNITS				SUIL			Second Second			SCULF			
B-10         FT.         B-8         FT.         2-4         FT.         S-10         FT.         S-10         FT.         S-10         FT.         S-10         FT.         S-10         FT.         S-113/90         D2/13/90		÷	1-8SH	HSB-2	KSB-3	4-8SH	HSB-5	9-8SH	TRPBLK	SD-1	SD-2	SD-3	SD-3DUP	TRPBLK	RINSEBLK
02/13/90         02/13/90<			8-10 FT.	-5 FT.	H.	2-4 FT.	н.	8-10 FT.	1				a G		
17:05         07:45         08:35         11:35         12:45         17:           UG/L         NRD         NRD         NRD         NRD         NRD         NRD           DE         UG/L         NRD         NRD         NRD         S000.00         <3.70			02/12/90		02/13/90	02/13/90			02/13/90	02/12/90	02/12/90	02/12/90	02/12/90	02/12/90	02/12/90
UG/L         NRD         NRD         NRD         NRD         NRD         NRD           DE         UG/KG-DRY $< 3.30$ $< 3.60$ $< 460.00$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ $< 3.70$ <td></td> <td></td> <td>17:05</td> <td>07:45</td> <td>08:35</td> <td>09:35</td> <td>11:35</td> <td>12:45</td> <td>12:00</td> <td>00:60</td> <td>09:20</td> <td>09:30</td> <td>06:30</td> <td>10:30</td> <td>10:45</td>			17:05	07:45	08:35	09:35	11:35	12:45	12:00	00:60	09:20	09:30	06:30	10:30	10:45
DE         UG/KG-DRY $< 3.30$ $< 3.60$ $< 460.00$ $< 3.70$ $< 5000.00$ $< 3.70$ DE         UG/L         NRa         NRa         NRa         NRa         NRa         NRa           LORIDE         UG/L         NRa         R         NRa         NRa         NRa         NRa         NRa           LORIDE         UG/L         NRa         R         NRa         NRa         NRa         NRa         NRa           LORIDE         UG/L         NRa         R         NRa         NRa         NRa         NRa         NRa           LORIDE         UG/L         NRa         R         NRa         NRa         NRa         NRa         NRa           LORIDE         UG/L         NRa         R         NRa         NRa         NRa         NRa         NRa           UG/L         NRa         NRa         NRa         NRa         NRa         NRa         NRa         NRa         NRa           UG/L         NRa         NRa         NRa         NRa         NRa         NRa         NRa           UG/L         NRa         NRa         NRa         NRa         NRa         NRa	UM, TOTAL XX)	nc/L	NRQ	NRQ	NRG	NRO	NRG	NRQ	NRQ	NRQ	NRQ	NRQ	NRQ	NRO	<3.50
DE         UG/L         NRG         NRG         NRG         NRG         NRG           LORIDE         UG/KG-DRY         <1.00	N DISULFIDE	UG/KG-DRY	<3.30	<3.60	<4.60.00	<3.70		<3.70	NRO	<3.60	23.00	<3.80	⊲3.80	NRQ	NRQ
LORIDE         UG/KG-DRY         <1.00         <1.10         <1.500.00         <1.10           LORIDE         UG/L         NR0         NR0         NR0         NR0         NR0           LORIDE         UG/L         NR0         NR0         NR0         NR0         NR0           UG/L         NR0         <0.69	N DISULFIDE X)	NG/L	NRQ	NRO	NRQ	NRO	NRQ	NRQ	<3.10	NRQ	NRQ	NRG	NRQ	<3.10	<3.10
LORIDE         UG/L         MRa         MR	N TETRACHLORIDE	UG/KG-DRY	<1.00	<1.10	<140.00	<1.10		<1.10	NRO	<1.10	<1.30	<1.20	<1.20	NRQ	NRG
UG/KG-DRY         <0.66         <0.74         <97.00         <0.77         <0.77           UG/L         NRa         NRa         NRa         NRa         NRa         NRa           UG/L         NRa         <1.80	N TETRACHLORIDE XX)	NG/L	NRQ	NRO	NRQ	NRQ		NRG	<0.97	NRG	NRG	NRQ	NRQ	7 <b>0.</b> 07	<0.97
UG/L         NRa         NRa </td <td>OBENZENE</td> <td>UG/KG-DRY</td> <td>&lt;0.69</td> <td></td> <td>&lt;97.00</td> <td>&lt;0.76</td> <td></td> <td>&lt;0.77</td> <td>NRO</td> <td>&lt;0.75</td> <td>&lt;0.88</td> <td>&lt;0.80</td> <td>&lt;0.80</td> <td>NRQ</td> <td>NRG</td>	OBENZENE	UG/KG-DRY	<0.69		<97.00	<0.76		<0.77	NRO	<0.75	<0.88	<0.80	<0.80	NRQ	NRG
E         UG/KG-DRY         <1.80         <2.00         <2.10         <2.10         <2.10           E         UG/L         NRa	COBENZENE XX)	NG/L	NRQ		NRQ		1		<0.65	NRG	NRG	NRQ	NRQ	<0.65	<0.65
E         UG/L         NRa	ROETHANE	UG/KG-DRY	<1.80		<260.00	<2.10	1	<2.10	NRO	<2.00	<2.40	<2.20	<2.20	NRQ	NRG
UG/KG-DRY         <1.20         <1.30         <180.00         <1.40         <1.40           UG/L         NRa         NRa         NRa         NRa         NRa         NRa         NRa           UG/L         NRa         NRa         NRa         NRa         NRa         NRa         NRa           ME         UG/L         <26.00	ROETHANE DX.)	nc/L	NRQ		NRQ	2		-	<1.80	NRG	NRG	NRG	NRQ	<1.80	<1.80
UG/L         HRa         NRa         NRa <td>ROFORM</td> <td>UG/KG-DRY</td> <td>&lt;1.20</td> <td>√</td> <td>&lt;180.00</td> <td>&lt;1.40</td> <td></td> <td>&lt;1.40</td> <td>NRQ</td> <td>&lt;1.40</td> <td>&lt;1.60</td> <td>&lt;1.50</td> <td>&lt;1.50</td> <td>MRQ</td> <td>NRG</td>	ROFORM	UG/KG-DRY	<1.20	√	<180.00	<1.40		<1.40	NRQ	<1.40	<1.60	<1.50	<1.50	MRQ	NRG
UG/KG-DRY         <26.00         <28.00         <28.00         39000.00         <29.00            UG/L         NRa         Ua         NRa         Ua         Ua         Ua         Ua         NRa	ROFORM DX)	UG/L	NRQ	-	NRO				<1.20	NRG	NRG	NRQ	NRQ	<1.20	<1.20
UG/L         NRa         NRa <td>ROMETHANE</td> <td>UG/KG-DRY</td> <td>&lt;26.00</td> <td></td> <td></td> <td>&lt;28.00</td> <td></td> <td>&lt;29.00</td> <td>NRG</td> <td>&lt;28.00</td> <td>&lt;33.00</td> <td>&lt;30.00</td> <td>&lt;30.00</td> <td>NRQ</td> <td>NRG</td>	ROMETHANE	UG/KG-DRY	<26.00			<28.00		<29.00	NRG	<28.00	<33.00	<30.00	<30.00	NRQ	NRG
MG/KG-DRY 0.78 3.49 3.85 5.87 1.93 2 UG/L NRQ NRQ NRQ NRQ NRQ	ROMETHANE OX)	UG/L	NRQ	14 20	NRQ		312(1-7)		<24.00	NRQ	NRQ	NRG	~ NRQ	<24.00	<24.00
UG/L NRQ NRQ NRQ NRQ	MIUM, SED	MG/KG-DRY	0.78	2000	495366				NRQ	3.38	2.20	02.69	52.00	NRQ	NRQ
	MIUM, TOTAL OX)	∩¢/L	NRQ						NRQ	NRQ	NRG	MRQ	NRG	NRG	<7.00
CHRYSENE UG/KG-DRY <97.00 5100.00 <110.00 <120.00 <120.00	SENE	UG/KG-DRY	00°26>						NRG	NRG 22000.00		<120.00 40000.00 52000.00	52000.00	NRO	NRQ

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. . Table 1-2. Analytical Parameters Detected in Soil/Sediment Samples in 1990, Hunter AAFTA, Continued, Page 6 of 9

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PARAMETERS	UNITS				SOIL						SEDIMENT	ENT		
		HSB-1	HSB-2	HSB-3	HSB-4	HS8-5	9-8SH	TRPBLK	so-1	SD-2	SD-3	SD-30UP	TRPBLK	RINSEBLK
		8-10 FT.	3-5 FT.	6-8 FT.	2-4 FL.	5-8 FT.	8-10 FT.				4			
		02/12/90 02/13/90	-	02/13/90	02/13/90	02/13/90	02/13/90	02/13/90	05/12/90	02/12/90	02/12/90	02/12/90	02/12/90	02/12/90
		17:05	07:45	08:35	09:35	11:35	12:45	12:00	00:60	09:20	09:30	06:30	10:30	10:45
CHRYSENE (EPTOX)	NG/L	NRO	NRG	NRG	NRQ	NRQ	NRG	NRG	NRQ	NRQ	NRG	NRQ	NRQ	<2.80
CIS-1,3-DICHLOROPROPENE	UG/KG-DRY	<1.60	<1.80	<230.00	<1.80	<2400.00	<1.80	NRQ	<1.80	<2.10	<1.90	<1.90	NRQ	NRQ
CIS-1,3-DICHLOROPROPENE (EPTOX)	NG/L	NRQ	NRO	NRQ	NRQ	NRG	NRC	<1.50	NRG	NRG	NRG	NRQ	<1.50	<1.50
DIBEN'(A, H)ANTH'CENE (EPTOX)	1/9N	NRQ	NRG	NRO	NRQ	NRO	NRG	NRG	NRQ	NRG	NRG	NRO	NRQ	<1.80
DIBEN(A, H)ANTHRACENE	· UG/KG-DRY	<63.00	1100.00	<72.00	<70.00	00°-22>	<72.00	NRQ	4200.00	<81.00	8100.00	11000.00	NRQ	NRO
D I BROMOCHLOROMETHANE	UG/KG-DRY	<1.40	<1.50	<200.00	<1.50	<2100.00	<1.50	NRG	<1.50	<1.80	<1.60	<1.60	NRO	NRQ
D1BROMOCHLOROMETHANE (EPTOX)	UG/L	NRQ	NRG	NRQ	NRG	NRQ	NRQ	<1.30	NRQ	NRQ	NRQ	NRO	<1.30	<1.30
ETHYLBENZENE	UG/KG-DRY	<1.10	<1.10	1500.00	<1.20	10000.00	<1.20	NRQ	<1.10	<1.40	<1.20	<1.20	NRQ	NRG
ETHYLBENZENE (EPTOX)	nc/L	NRQ	NRQ	NRQ	NRQ	NRQ	NRQ	<1.00	NRO	NRG	NRQ	NRQ	<1.00	<1.00
FLUORANTHENE	UG/KG-DRY	<110.00	13000.00	140.00	<130.00	360.00	<130.00	NRQ	36000.00	<150.00	54000-00	62000.00	NRO	NRO
FLUORANTHENE (EPTOX)	NG/L	NRQ	NRO	NRG	NRQ	NRG	NRG	NRO	NRO	NRO	NRQ	NRQ	NRQ	<3.20
FLUORENE	UG/KG-DRY	<110.00	720.00	<120.00	<120.00	<130.00	<120.00	NRQ	1500.00	<140.00	2500.00	8300.00	NRO	NRQ
FLUORENE (EPTOX)	NG/L	NRG	NRQ	NRG	NRQ	NRQ	NRQ	NRQ	NRO	NRO	NRQ	NRQ	NRQ	3.10
INDENO(1,2,3-CD)PYRENE	UG/KG-DRY	<95.00	2900.00	<110.00	<110.00	<120.00	<110.00	NRQ	00.0067	<120.00	15000.00	23000.00	KRQ	NRG
INDENO(1,2,3-CD)PYRENE (EPTOX)	NG/L	NRQ	NRG	NRQ	NRG	NRG	NRQ	NRO	NRQ	NRQ				8
LEAD, SED	MG/KG-DRY	<5.26	<5.71	<5.97	<5.81	7.40	<5.97	NRQ	7.65	12.7	275.00	362.00	NRG	NRG

Table 1-2. Analytical Parameters Detected in Soil/Sediment Samples in 1990, Hunter AAFTA, Continued, Page 7 of 9 ×

PARAMETERS	UNITS				SOIL				8		SEDIMENT	IENT		
		H-82H	HSB-2	HSB-3	4-8SH	HSB-5	9-8SH	TRPBLK	so-1	SD-2	SD-3	SD-3DUP	TRPBLK	RINSEBLK
	•)	8-10 FT.	3-5 FT.	6-8 FT.	2-4 FT.	5-8 FT.	8-10 FT.							
		02/12/90	02/13/90	02/13/90	02/13/90	02/13/90	02/13/90 02/13/90 02/12/90 02/12/90 02/12/90 02/12/90	02/13/90	02/12/90	02/12/90	02/12/90	02/12/90	02/12/90 02/12/90	02/12/90
		17:05	07:45	08:35	09:35	11:35	12:45	12:00	00:60	09:20	09:30	09:30	10:30	10:45
LEAD, TOTAL (EPTOX)	nc/L	NRG	NRQ	NRQ	NRQ	NRG	NRG	NRQ	NRG	NRO	NRQ	NRO	NRO	<25.00
MERCURY, SED	MG/KG-DRY	<0.10	<0.11	<0.11	<0.11	<0.12	<0.12	NRG	<0.11	<0.13	<0.12	<0.12	NRQ	NRO
MERCURY, TOTAL (EPTOX)	NG/L	NRC	NRG	NRG	NRG	NRG	NRQ	NRQ	NRQ	NRG	NRQ	NRQ	NRQ	<0.20
METHYLENE CHLORIDE	UG/KG-DRY	<1.70	<1.80	<240.00	<1.90	<2600.00	6.70	NRQ	7.00	12.00	<2.00	<2.00	MRQ	NRO
METHYLENE CHLORIDE (EPTOX)	nc/L	NRG	NRQ	NRQ	NRQ	NRG	NRQ	2.60	NRO	NRO	NRG	NRO	<1.60	<1.60
NAPHTHALENE	UG/KG-DRY	<210.00	<230.00	5700.00	<230.00	11000.00	<240.00	NRO	<230.00	<270.00	<250.00	390.00	NRO	NRQ
NAPHTHALENE (EPTOX)	NG/L	NRG	NRQ	NRG	NRQ	NRQ	NRG	NRQ	NRO	NRO	NRQ	NRG	NRO	<5.90
NITROBENZENE-D(5)	UG/KG-DRY .	3670.00	3910.00	4180.00	4130.00	3740.00	4060.00	NRQ	3790.00	4310.00	4270.00	4070.00	NRG	NRQ
NITROBENZENE-D(5) (EPTOX)	NG/L	NRG	NRQ	NRQ	NRQ	NRQ	NRQ	NRQ	NRO	NRG	NRQ	NRO	NRQ	87.00
PHENANTHRENE	UG/KG-DRY	<67.00	8100.00	150.00	<74.00	290.00	<76.00	NRQ	20000.00	<87.00	33000.00	62000.00	NRQ	NRQ
PHENANTHRENE (EPTOX)	חפ/ר	NRQ	NRQ	NRO	NRQ	NRQ	NRQ	NRQ	NRO	NRQ	NRG	NRQ	NRG	<1.90
PHENOL-D(5)	UG/KG-DRY	9640.00	9660.00	10800.00	10800.00 10000.00	11000.00	10700.00	NRO	7980.00	9510.00	8650.00	8780.00	MRG	NRG
PHENOL-D(5) (EPTOX)	NG/L	NRO	NRG	NRG	NRG	NRG	NRQ	NRG	NRG	NRG	NRQ	NRG	NRQ	77.00
PYRENE	UG/KG-DRY	<72.00	9700.00	140-00	<79.00	340.00	<81.00	NRQ	27000.00	<92.00	43000.00	58000.00	NRQ	NRQ
PYRENE (EPTOX)	NG/L	NRQ	NRQ	NRO	NRQ	NRQ	NRG	NRO	NRQ	NRG	NRG	NRG	NRG	<2.00
SELENIUM, SED	MG/KG-DRY	<0.42	<0.45	27*0>	<0°76	0.67	<0.47	NRO	<0.46	<0.54	<0-49	<0.49	WRO	NRQ

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Table 1-2. Analytical Parameters Detected in Soil/Sediment Samples in 1990, Hunter AAFTA, Continued, Page 8 of 9

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PARAMETERS U	UNITS	-			SOIL						SEDIMENT	IENT		
•		HSB-1	HSB-2	HSB-3	HSB-4	HSB-5	9-8SH	TRPBLK	so-1	SD-2	SD-3	so-3DUP	TRPBLK	RINSEBLK
		8-10 FT.	3-5 FT.	6-8 FT.	2-4 FT.	5-8 FT.	8-10 FT.							
		02/12/90	02/13/90	02/13/90	02/13/90 02/13/90		02/13/90	02/13/90 02/12/90	02/12/90	02/12/90	02/12/90	02/12/90 02/12/90	02/12/90	02/12/90
*	. *	17:05	07:45	08:35	09:35	11:35	12:45	12:00	00:00	09:20	09:30	05:30	10:30	10:45
SELENIUM, TOTAL (EPTOX)	UG/L	NRQ	NRG	NRO	NRO	NRQ	NRG	NRG	NRQ	NRO	NRG	KRO	NRQ	<2.00
SILVER, SED	MG/KG-DRY	<0.60	<0.65	<0.68	<0.66	<0.73	<0.68	NRQ	<0.66	<0.77	<0.71	-71	NRG	NRQ
SILVER, TOTAL (EPTOX)	NG/L	NRQ	NRQ	NRQ	NRG	NRQ	NRG	NRO	NRQ	NRG	NRG	NRG	NRG	<5.70
STYRENE	UG/KG-DRY	<1.70	<1.80	<240.00	<1.90	<2500.00	<1.90	NRQ	<1.80	<2.20	<2.00	<2.00	NRQ	NRQ
STYRENE (EPTOX)	NG/L	NRQ	NRQ	NRQ	NRQ	NRQ	NRQ	<1.60	NRG	NRG	NRQ	MRQ	<1.60	<1.60
TERPHENYL-(D14)	MG/KG-DRY	5880.00	5940.00	4000.00	10600.00	5450.00	5260.00	NRQ	5430.00	4240.00	4890.00	4850.00	NRG	NRG
TERPHENYL-(D14) (EPTOX)	NG/L	NRQ	NRG	NRO	NRG	NRQ	NRO	NRQ	NRG	NRQ	NRQ	NRO	NRG	73.00
TETRACHLOROETHENE	UG/KG-DRY	<0.54	<0.58	<76.00	<0.60	<810.00	<0.60	NRQ	<0.59	<0.69	<0.63	<0.63	NRQ	NRQ
TETRACHLOROETHENE (EPTOX)	NG/L	NRQ	NRQ	NRG	NRQ	NRQ	NRQ	<0.51	NRQ	NRO	NRQ	NRQ	<0.51	<0.51
TOLUENE	UG/KG-DRY	2.80	2.90	<100.00	<0.82	<1100.00	5.50	NRO	<0.81	3.20	<0.86	<0.86	NRQ	NRQ
TOLUENE (EPTOX)	NG/L	NRG	NRQ	NRO	NRQ	NRQ	NRG	<0.70	NRG	NRQ	NRG	NRQ	<070	<0.70
TOLUENE-D(8) (EPTOX)	NG/L	NRQ	NRQ	NRQ	NRQ	NRG	NRQ	NRO	NRG	NRG	NRQ	NRG	NRO	51.00
TOLUENE-D8	UG/KG-DRY	29.00	66.00	61.00	66.00	55.00	67.00	NRO	63.00	73.00	68.00	54.00	NRQ	NRG
TRANS-1,3-DICHLOROPROPENE	UG/KG-DRY	<0.91	<0.98	<130.00	<1.00	<1400.00	<1.00	NRG	<0.99	<1.20	<1.10	<1.10	NRQ	NRQ
TRANS-1,3-DICHLOROPROPENE (EPTOX)	UG/L	NRQ	NRQ	NRG	NRG	NRG	NRO	<0.86	NRG	NRQ	NRQ	NRQ	<0.86	<0.86
TRICHLOROETHENE	UG/KG-DRY	<0.92	<1.00	<130.00	<1.00	<1400.00	<1.00	NRQ	<1.00	<1.20	<1.10	<1.10	NRQ	NRQ

Table 1-2. Analytical Parameters Detected in Soil/Sediment Samples in 1990, Hunter AAFTA, Continued, Page 9 of 9

PARAMETERS	UNITS			-	SOIL				8 2 1	5	SEDIMENT	IENT		
		HSB-1	HSB-2	HSB-3	HSB-4	HSB-5	HSB-6	TRPBLK	so-1	SD-2	SD-3	SD-3DUP	TRPBLK	RINSEBLK
20		8-10 FT.	3-5 FT.	6-8 FT.	2-4 FT.	5-8 FT.	8-10 FT.	•		1			·	
		02/12/90	02/13/90	02/13/90	02/13/90	02/13/90 02/13/90	02/13/90	02/13/90	02/12/90	02/12/90	02/12/90	02/12/90 02/12/90 02/12/90	02/12/90 02/12/90	02/12/90
		17:05	07:45	08:35	09:35	11:35	12:45	12:00	00:60	09:20	09:30	09:30	10:30	10:45
TRICHLOROETHENE (EPTOX)	NG/L	NRQ	NRQ	NRQ	NRQ	NRQ	NRO	<0.87	NRG	NRG	NRQ	NRQ	<0.87	<0.87
VINYL ACETATE	UG/KG-DRY	<2.70	<2.90	<380.00	<3.00	<4100.00	<3.00	NRG	<3.00	<3.50	<3.20	<3.20	NRO	NRQ
VINYL ACETATE (EPTOX)	UG/L	NRQ	NRQ	NRQ	NRQ	NRQ	NRO	<2.60	NRG	NRO	NRG	NRQ	<2.60	<2.60
VINYL CHLORIDE	UG/KG-DRY	<1.60	<1.80	<230.00	<1.80	<2500.00	<1.80	NRG	<1.80	<2.10	<1.90	<1.90	NRQ	NRQ
VINYL CHLORIDE (EPTOX)	NG/L	NRQ	NRG	NRQ	NRO	NRQ	NRQ	<1.60	NRQ	NRQ	NRQ	NRQ	<1.60	<1.60
XYLENE, SED	UG/KG-DRY	<1.10	<1.20	<150.00	<1.20	57000.00	<1.20	NRQ	<1.20	<1.40	2.40	<1.30	NRG	NRQ
XYLENES, TOTAL (EPTOX)	NG/L	NRQ	NRQ	NRQ	NRQ	NRG	NRQ	<1.00	NRQ	NRQ	NRG	NRQ	<1.00	<1.00
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Source: ESE.

Table 1-3. Analytical Parameters Detected in Groundwater Samples in 1990, Hunter AAFTA

PARAMETERS	UNITS	1-WMH	HMW-2	HMU-3	7-MMH	HMM-5	NHM-6
		03/07/90	03/07/90	03/08/90	03/08/90	03/08/90	03/08/90
		16:55	10:20	09:20	09:35	10:35	11:10
1,1,1-TRICHL'ETHANE	1/90	<1.30	<1.30	<1.30	<1.30	<1.30	<1.30
1,1,2,2-TETRACHLORO ETHANE	ng/L	<1.50	<1.50	<1.50	<1.50	<1.50	<1.50
1,1,2-TRICHL'ETHANE	1/9N	<1.60	<1.60	<1.60	<1.60	<1.60	<1.60
1,1-DICHLOROETHANE	ng/L	<0.85	<0.85	<0.85	<0.85	<0.85	<0.85
1,1-DICHLOROETHYLENE	NG/L	<1.20	<1.20	<1.20	<1.20	<1.20	<1.20
1,2-DICHLOROETHANE	NG/L	<0.87	<0.87	<0.87	<0.87	<0.87	<0.87
1,2-DICHLOROETHANE-D4	NG/L	49.00	55.00	46.00	47.00	46.00	46.00
1,2-DICHLOROETHENE, TOTAL	NG/L	<1.30	<1.30	<1.30	<1.30	<1.30	<1.30
1,2-DICHLOROPROPANE	ng/L	<b>79.0</b> >	<0.97	×0.97	<0°0>	<0.97	-0.97
2,4,6-TRIBROMOPHENOL	UG/L	180.00	170.00	190.00	180.00	160.00	180.00
2-BUTANONE	nc/L	44.62	44	77"6>	77°6>	<9.44	-0°-44
2-FLUORBIPHENYL	UG/L	66.00	74.00	00*99	00*69	76.00	00*62
2-FLUOROPHENOL	nc/r	180.00	160.00	150.00	170.00	150.00	170-00
2-HEXANONE	NG/L	3.10	3.10	<3.10	3.10	<3.10	<3.10
4-METHYL-2-PENTANONE	, UG/L	<3.00	3.00	<3.00	€3.00	<3.00	<3.00
ACENAPHTHENE	NG/L	<3.80	<3.80	<3.80	<3.80	<3.80	<3.80
ACENAPHTHYLENE	ng/L	<2.70	<2.70	<2.70	<2.70	<2.70	<2.70
ACETONE	ne/t	<17.00	<17.00	<17.00	<17.00	<17.00	<17.00
ANTHRACENE	NG/L	<2.10	<2.10	<2.10	<2.10	<2.10	<2.10
ARSENIC, TOTAL	NG/L	3.10	51.60	2.40	8.50	8.90	77.30
BARIUM, TOTAL	ng/L	59.20	1000-00	36.80	166.00	104.00	864.00
282285	NG/L	<1.10	<1.10	7.80	1.90	1.10	44.00

Tabue 1-3. Analytical Parameters Detected in Groundwater Samples in 1990, Nummer AAFTA, Continued, Page 2 of 4

PARAMETERS	UNITS	HMW-1	HMH-2	HMW-3	HMW-4	HMU-5	O-WWH
-		03/07/90	03/07/90	03/08/90	03/08/90	03/08/90	03/08/90
		16:55	10:20	09:20	09:35	10:35	11:10
BENZOCAJANTHRACENE	n¢/r	<1.80	<1.80	<1.80	<1.80	<1.80	3.20
BENZO(A)PYRENE	NG/L	<5.20	<5.20	<5.20	<5.20	<5.20	<5.20
BENZO(B) FLUORANTHENE	nc/L	<3.80	<3.80	<3.80	<3.80	<3.80	7.00
BENZO(GHI)PERYLENE	nc/L	<2.10	<2.10	<2.10	<2.10	<2.10	2.30
BENZOCK)FLUORANTHENE	ng/L	<4.70	<4.70	<4.70	<4.70	<4.70	ct.70
BROMOD I CHLOROMETHANE	ng/L	<0.98	<0.98	<0.98	<0.98	<0.98	<0.98
BROMOFLUOROBENZENE	ng/L	49-00	52.00	52.00	23.00	50.00	47.00
BROMOFORM	1/9N	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50
BROMOMETHANE	ng/L	<1.20	<1.20	<1.20	<1.20	<1.20	<1.20
CADMIUM, TOTAL	1/90	<3.50	3.50	<3.50	<3.50	<3.50	3.96
CARBON DISULFIDE	ng/L	3.10	<3.10	<3.10	<3.10	<3.10	≪3.10
CARBON TETRACHLORIDE	ng/L	<0.0>	26.0>	<0.97	<0.97	<0.97	<0.97
CHLOROBENZENE	nG/L	<0.65	<0.65	<0.65	<0.65	<0.65	<0.65
CHLOROETHANE	ng/L	<1.80	<1.80	<1.80	<1.80	<1.80	<1.80
CHLOROFORM	NG/L	<1.20	<1.20	<1.20	<1.20	<1.20	<1.20
CHLOROMETHANE	ng/L	<24.00	<24.00	<24.00	<24.00	<24.00	<24.00
CHROMIUM, TOTAL	UG/L	11.20	217.00	12.00	46.70	46.80	239.00
CHRYSENE	UG/L	<2.80	<2.80	<2.80	<2.80	<2.80	5.30
CIS-1,3-DICHLOROPROPENE	NG/L	<1.50	<1.50	<1.50	<1.50	<1.50	<1.50
DIBEN' (A, H)ANTH' CENE	UG/L	<1.80	<1.80	<1.80	<1.80	<1.80	<1.80
DIBROMOCHLOROMETHANE	NG/L	<1.30	<1.30	<1.30	<1.30	1.30	<1.30
	UGAL	<1.00	<1.00	<1.00	1.00	1 <1.00	120.00

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Table 1-3. Analytical Parameters Detected in Groundwater Samples in 1990, Hunter AAFTA, Continued, Page 3 of 4

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	6	06/20/20	03/07/90	03/08/90	03/08/90	03/08/90	03/08/90
		16:55	10:20	09:20	09:35	10:35	11:10
FLUORANTHENE	UG/L	<3.20	3.20	<3.20	<3.20	<3.20	7.30
FLUORENE	UG/L	3.10	<3.10	<3.10	3.10	<3.10	€.10
INDENO(1,2,3-CD)PYRENE	NG/L	<2.70	<2.70	<2.70	<2.70	<2.70	<2.70
LEAD, TOTAL	UG/L	<25.00	261.00	<25.00	28.60	<25.00	337.00
MERCURY, TOTAL	nc/L	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20
METHYLENE CHLORIDE	UG/L	<1.60	<1.60	<1.60	<1.60	<1.60	<1.60
NAPHTHALENE	UG/L	<5.90	<5-90	<5.90	<5.90	<5.90	43.00
NITROBENZENE-D(5)	NG/L	83.00	81.00	00.77	78.00	00°62	85.00
PHENANTHRENE	UG/L	<1.90	<1.90	<1.90	<1.90	<1.90	5.20
PHENOL-D(5)	NG/L	110.00	00.92	96.00	110.00	00.72	100.00
PYRENE	NG/L	<2.00	<2.00	<2.00	<2.00	<2.00	6.80
SELENIUM, TOTAL	- UG/L	<2.00	2.80	<2.00	5.20	4.30	14.40
SILVER, TOTAL	NG/L	<5.70	<5.70	<5.70	<5.70	<5.70	<5.70
STYRENE	NG/L	<1.60	<1.60	<1.60	<1.60	<1.60	<1.60
TERPHENYL-(014)	NG/L	64.00	69.00	29.00	65.00	70-00	93.00
TETRACHLOROETHENE	NG/L	<0.51	<0.51	<0.51	<0.51	<0.51	<0.51
TOLUENE	∩c/r	<0.70	1.60	0.74	o2*0>	<0.70	1.70
TOLUENE-D(8)	UG/L	51.00	53-00	52.00	53.00	51.00	47.00
TRANS-1,3-DICHLOROPROPENE	UG/L	<0.86	<0.86	<0.86	<0.86	<0.86	<0.86
TRICHLOROETHENE	NG/L	<0.87	<0.87	<0.87	<0.87	<0.87	<0.87
VINYL ACETATE	NG/L	<2.60	<2.60	<2.60	<2.60	<2.60	<2.60
VINYL CHLORIDE	NG/L	<1.60	<1.60	<1.60	<1.60	<1.60	<1.60

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Taule 1-3. Analytical Parameters Detected in Groundwater Samples in 1990, Hunter AAFTA, Continued, Page 4 of 4

PARAMETERS	UNITS	HMW-1	HMW-2	HMW-3	HMM-4	HMW-5	HMW-6
		06/20/20	06/20/20	03/08/90	03/08/90	03/08/90	03/08/90
	5	16:55	10:20	09:20	09:35	10:35	11:10
XYLENES, TOTAL	1/9N	<1.00	<1.00	3.30	<1.00	<1.00	9.40

		HS-17 HUNTS1 17	03/04/92 11:15	12.1	0.855	17.6	<0.541	2.86	<7.19	668.8>	<0.281	<0.811	68>	<80	<80	011>	<168	6119	<180	<110	<118	<180	68>	68>	<180	<80	<80	
		HS-16 HUNTS1 16	03/04/92 11:00	8.8	1.18	38.4	<0.522	6.10	107	69.03	<0.267	<0.783	£1\$	210	210	978	1300	2888	<188	620	1669	<180	986	(1)	<180	<b>77</b> >	100	
		HS-15 HUNTS1 15	03/04/92 10:55	8.3	1.61	47.6	<0.511	5.29	13.8	<0.05	<0.270	<0.767	<76	<160	<76	120	<150	210	\$178	<110	150	<178	180	<76	<170	<76	<76	
		HS-14 HUNTS1 14	83/84/92 18:08	13.8	0.596	17.7	<0.547	2.22	<7.27	<0.184	<0.287	<0.821	(8)	<178	<81	<120	<168	<120	<198	<120	<120	861>	(8)	(8)	<198	<81	(81	
	1	HS-13 HUNTS1 HUNTS1	03/64/92 09:35	12.5	8.548	14.7	<0.548	2.44	<7.29	660.0>	<0.281	<0.822	68>	<170	68>	<110	<168	<118	<188	811>	<118	<188	<80	68>	<180	<88>	68>	
	L PAGE	HS-12 HUNTS1 12	03/04/92 09:30	10.0	0.330	9.68	<0.519	3.02	<6.98	<0.097	<0.275	617.0>	<78	<170	<78	160	180	268	<180	6119	170	<180	179	679	<180	<78	<78	
	92 STATUS : FINAL COE - FT. STEMART S.P. WOODWARD SUZANNE WOODWARD	HSTNUH 12 11	03/04/92 08:45	12.9	0.340	13.9	<0.548	2.16	<i>&lt;</i> 7.28	<0.101	<0.284	<0.821	480	<170	68>	<118	<160	<110	<180	6119	<118	<180	<80 <	68>	<180	<80	480	
	96/92 5 COE ER S.P.	HS-10 HUNTS1 18	03/04/92 08:40	7.7	0.516	18.3	<0.517	3.55	7.39	660.0>	<0.263	<0.775	<380	618	670	5300	4800	6980	<878	2788	5300	<870	8100	08E>	<878	<380	678	2
×.	Environmental Science & Engineering DATE 04/06/ PROJECT NUMBER 39240106 0201 PROJECT NAME FIELD GROUP HUNTSI PROJECT MANAGER ALL LAB COORDINATOR	6-SH 1SLNNH 6	03/03/92 14:25	11.0	0.375	17.1	<0°.539	1.94	<7.16	<0.096	<0.276	<0.888	99965>	<8400	<3988	<5600	67966	<5688	6996>	<5600	<5600	6996>	<3908	006E> .	6996>	41000	006E>	•
	Engineerin 0201 PRI PRI LA	HUNTSH B-SH B-SH	03/03/92 14:10	13.2	0.938	15.0	<8.548	2.80	8.83	<0.180	<0.286	<0.809	<81	996 E	440	378	690	830	<180	240	210	<180	328	<81	570	1400	<b>0</b> 6	
	Sclence & 39240186 HUNTS1 ALL	HUNTSH 12 7	03/03/92 14:05	14.5	0.503	23.7	<8.546	4.97	23.9	<8.101	<0.286	<0.819	<82	<180	<82	120	<168	270	<198	<128	220	61>	360	<82	61>	<82	170	
	ronmental ECT NUMBER D GROUP	HS-4 HUNTS1	03/03/92 11:30	16.3	2.44	23.4	<0.558	5.51	8.82	<0.104	<0.296	<0.838	<84	<180	<84	<120	<178	6212	<198	<120	<120	<198	<84	<84	961>	<84	<84	
	Envi PROJ FIEL	e-Sh E-Sh	03/03/92 11:15	13.5	1.28	14.9	<0.540	5.88	17.3	<0.103	<0.288	<0.810	18>	<178	(81	170	220	370	<180	150	280	<180	120	18>	081>.	18>	(81	
		HS-2 HUNTS1 2	83/83/92 16:30	17.3	0.630	12.8	<0.573	2.81	¢7.62	<0.108	<0.297	<0.860	<858	<1800	<850	<1200	<1788	<1200	<1988	<1288	<1289	<1988	<850	<850	<1988	3580	1 <850	
	2	HS-1 I-SH I	03/03/92 10:15	10.4	. 1.82	11.4	<0.521	5.61	28.0	<0.896			<78	6/170	8/>	378	320	568	681>	258	560	<188	669	<78	<180 <180	5 <78	440	
		STORET METHOD		78328	1003			1029 1029	ICAP 1052	1CAP 71921	CVAA 1148	GF AA 1078	1CAP 34208	GMS 34203				ñ	31	ŵ	'n	E 34559		GMS 34384	34406	r GMS 34445	7 GMS 34464	
	8	SAMPLE ID'S Parameters Units	DATE TIME	MOISTURE	ARSENIC, SED	MG/KG-DRY BARIUM,SED	MG/KG- DRY CADMIUM,SED	CHROMIUM, SED	MG/KG-DRY Lead,sed	HG/KG-DRY Mercury .sed	S E	MG/KG-DRY SILVER_SED	MG/KG-DRY ACENAPHTHENE	UG/KG-DRY ACENAPHTHYLENE	UG/KG-DRY ANTHRACENE	UG/KG-DRY BENZO(A)ANTHRACENE	UG/KG-DRY BENZO(A)PYRENE	UG/KG-DRY BENZO(B)FLUORANTHENE	UG/KG-DRY BENZO(GHI)PERYLENE	UG/KG-DRY BENZO(K)FLUORANTHENE	UG/KG-DRY CHRYSENE	UG/KG-DRY DIBEN(A, H)ANTHRACENE	UG/KG-DRY FLUORANTHENE	UG/KG-DRY FLUORENE	UG/KG-DRY INDENO(1,2,3-CD)	PYRENE UG/KG-DRY NAPHTHALENE	UG/KG-DRY PHENANTHRENE	UG/KG-DKT

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		HS-17 TSTNUH TZ	03/04/92 11:15	<80 80	<5.7	<5.7	<5.7		11>	<5.7	<5.7	<5.7	<5.7	(1)	<5.7	<5.7	11Þ	<80	<89>	685	11>	<5.7	<5.7	<5.7	<5.7	<5.7	<5.7	
		HS-16 HUNTSI 16	03/04/92 11:00	818	<5.5	<5.5	<5.5	(1)	(1)	<5.5	<b>(5.5</b>	<5.5	<5.5	T)	<b>&lt;</b> 5.5	<5.5	(11)	112	112	LL>		<b>&lt;5.5</b>	<5.5	<5.5	<5.5	<5.5	<5.5	
		HS-15 HUNTS1 15	03/04/92 10:55	110	<5.5	<5.5	<5.5	÷	(1)	<b>&lt;5.5</b>	<5.5	<5.5	<5.5	<li>(1)</li>	<5.5	<5.5	<li>(II)</li>	<76	<76	¢76	11	<5.5	<5.5	<5.5	<5.5	<5.5	<5.5	
	*	HS-14 HUNTS1 14	03/04/92 10:00	18>	<5.8	<5.8	<5.8	<12	<12	<5.8	<5.8	<5.8	<5.8	<12	<5.8	<5.8	<12	<81	18>	(8)	<12	<5.8	<5.8	<5.8	<5.8	<5.8	<5.8	
	8	HUNTS1 HUNTS1 13	03/04/92 0 09:35	68>	<5.7	<b>G.7</b>	<5.7	٩IJ	!	<5.7	<5.7	<5.7	<5.7	411	<5.7	<5.7	<li><li><li><li><li><li><li><li><li><li></li></li></li></li></li></li></li></li></li></li>	<b>8</b> 8>	<88	685	(1)	<5.7	<5.7	<5.7	<5.7	<5.7	<b>45.7</b>	
	PAGE	, HS-12 HUNTS1 12	03/04/92 0 09:30	140	<5.6	<5.6	<5.6	11>	(1)	<5.6	<5.6	<5.6	<5.6	!</td <td>&lt;5.6</td> <td>&lt;5.6</td> <td>(II)</td> <td>&lt;78</td> <td>&lt;78</td> <td>٢٦8</td> <td><!--!--></td> <td>&lt;5.6</td> <td>&lt;5.6</td> <td>&lt;5.6</td> <td>&lt;5.6</td> <td>&lt;5.6</td> <td>&lt;5.6</td> <td></td>	<5.6	<5.6	(II)	<78	<78	٢٦8	!	<5.6	<5.6	<5.6	<5.6	<5.6	<5.6	
	US : FINAL T. STEWART ODWARD MOODWARD	II ISTNUH II	03/04/92 0 08:45	68>	<5.7	<5.7	<5.7	¢11	411	<5.7	<5.7	<5.7	<5.7	!	<5.7	<5.7	<b>(11</b>	<88	68>	<b>88</b> >	<11	<5.7	<b>(5.7</b>	<5.7	<5.7	<5.7	<5.7	
	'92 STAT COE - F S.P. NO SUZANNE	HS-10 HUNTS1 10	03/04/92 0 08:40	5288	<pre>.4</pre>	<5.4	<5.4	(1)	411	<5.4	<5.4	<5.4	<5.4	11>	<5.4	<5.4	(11)	<380	6380	<380	411	<5.4	<5.4	<5.4	<5.4	<5.4	<5.4	-
	Ing DATE 04/06/ PROJECT NAME PROJECT MANAGER LAB COORDINATOR	HUNTS1	03/03/92 0 14:25	<3908	39	<28	<28	<56	<56	<28	<28	<28	<28	<b>&lt;56</b>	<28	<28	<56	006E>	886E>	0065>	<56	<28	42 <del>8</del>	<28	<28	<28	<28	
	rineering PROJE PROJE LAB (	8-SH 1STNUH 8	03/03/92 0. 14:10	230	<29	(2)	<29	<58	<58	62>	<29	<29	<29	<58	62>	<29	<58	(8)	<81	(8)	<58	€2>	<b>62</b> >	<2 <b>&gt;</b>	<29	<b>6</b> 2>	<b>4</b> 29	
	I Science & Engineering DATE 04, ER 39240186 0201 PROJECT NAME HUNTS1 PROJECT MANAI ALL LAB COORDINA	HS-7 HUNTSI 7	03/03/92 03 14:05	178	<5.8	<5.8	<5.8	<12	<12	<5.8	<5.8	<5.8	<5.8	<12	<5.8	<5.8	<12	<82	<82	<82	<12	<5.8	<5.8	<5.8	<5.8	<5.8	<5.8	
	S &	HS-4 HUNTS1 4	03/03/92 0: 11:30	<84	6.9>	6.8	6.9>	<12	13	<6.9	6.9	6.9>	6.9>	<12	6.9>	<6.8	<12	<84	<84	<84	<12	<6.9	6.9>	<6.8	<6.8	6.9>	6.0	
	Environmental PROJECT NUMBE FIELD GROUP	E-SH 12TNUH 5	03/03/92 0 11:15	861	<5.8	<5.8	<5.8	<12	<12	<5.8	<5.8	<5.8	<5.8	<12	<5.8	<5.8	<12 <12	(81	18>	(81	<12	<5.8	<5.8	<5.8	.<5.8	<5.8	<5.8	
		HS-2 HUNTS1 2	03/03/92 0 10:30	<850	9E>	430	<30	<60	<60	<38 <	630	<38	430	<60	630	8E>	<60	<850	<850	<850	<68	430	630	430	9E>	430	<30 <	
	с В С/	HUNTS1 ISTNUH	63/63/92 6 16:15	580	<5.6	<5.6	<5.6	111>	112	<5.6	<5.6	<5.6	.<5.6	115	<5.6	6.6	Ĵ	<78	<78	<78		<5.6	<5.6	<5.6	<5.6	<5.6	<5.6	
		STORET METHOD		34472	GMS 34237	GMS 34338	6MS 34298	6MS 34416	6MS 75078	CMS 78544	6MS 34299	6MS 34364	CMS 54309	GMS 34314	GMS 34318	CMS CMS	CHS CMS	SMO	CMS CMS	6MS 34574			6MS 34534				GMS 34702	GMS
売!		SAMPLE ID'S Parameters Units	DATE	PYRENE	UG/KG-DRY BENZENE	UC/KG-DRY BROMOD I CHLOROME THAME	UG/KG-DRY BROMOFORM	UG/KG-DRY BROMOMETHANE	UG/KG-DRY HETHYL ETHYL KETONE	UG/KG-DRY CARBON DISULFIDE	UG/KG-DRY CARRON TETRACHLORIDE	UG/KG-DRY CHI ORORENZENE	DI REDMOCHI OROMETHANE	UC/KG-DRY	CHLOROFORM	CHECKIC DECTURY VINYI -	ETHER UG/KG-DRY	UG/KG-DRY	I 2-DICHLORDENZENE	I 4-DICHLOROBENZENE	UG/KG-DRY DICHI OROBENZENE TOTA	L UG/KG-DRY	UG/KG-DRY 1 2-DICHLOROFTHANE	UG/KG-DRY I 1-DICHLOROETHYLENE	UG/KG-DRY	0TAL) UG/KG	CIS-1, 3-DICHLORO-	PROPENE UC/KG-DRY

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Environmental Science & Engineering DATE 04/06/92 STATUS : FINAL PROJECT NUMBER 32240186 0201 PROJECT NAME COE - FT. STEWART FIELD GROUP HUNTS1 PROJECT MANAGER S.P. WOODWARD ALL LAB COORDINATOR SUZANNE WOODWARD

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						ALL	LAI	LAD COURDINATOR SULAINE MOODANIN	ANNALUAL	AUDRADOR .						
SAMPLE ID'S Parameters Units	STORET METHOD	HS-1 I-SH I	HS-2 HUNTS1 2	HUNTS1 12TUUH 3	HUNTS 4	HUNTST	HUNTS1 HUNTS1 B	HUNTS1 1210H 9	HS-10 181 18	HS-11 HUNTS1 11	HUNTS1 12 12	HUNTSI ISTNUH EI	HS-14 HUNTS1 14	HS-15 HUNTS1 15	HS-16 HUNTS1 16	HS-17 HUNTS1 17
DATE TIME		83/83/92 10:15	03/03/92 10:30	83/83/92 11:15	03/03/92 11:30	03/03/92 14:05	03/03/92 14:10	03/03/92 14:25	03/04/92 08:40	03/04/92 08:45	83/84/92 89:38	03/04/92 09:35	83/84/92 10:00	03/04/92 10:55	03/04/92 11:00	03/04/92 11:15
TRANS-1, 3-DI CHLORO-	34697	<5.6	<38	<5.8	<6.8	<5.8	<b>429</b>	<28	. <5.4	<5.7	<5.6	<5.7	<5.8	<5.5	<5.5	<5.7
PROPENE UG/KG-DRY DIETHYL ETHER	GMS 97201	615	<68	<10	<10	<10	<69	<68	<10	<10	61>	<18	<10	<18	<10	<18
UG/KG-DRY ETHYLBENZENE	6MS 34374	<5.6	36	<5.8	<6.8	<5.8	65	540	<5.4	<5.7	<5.6	<5.7	6.9	<5.5	<5.5	<5.7
UG/KG-DRY METHYLENE CHLORIDE	GMS 34426	<5.6	<30	<5.8	<6.8	<5.8	<29	<28	<5.4	<5.7	<5.6	<5.7	<5.8	<5.5	<5.5	<5.7
UG/KG-DRY METHYL I SOBUTYLKETONE	75169		669>	<12	<12	<12	<58	<56	(1)	<11	(11)	11>	<12	(1)	(1)	11>
UG/KG-DRY 1.1.2.2-TETRACHLORO-	6MS 34519	<5.6	96>	<5.8	<6.9	<5.8	<29	<28	<b>4</b> 2.4	<5.7	<5.6	<5.7	<5.8	<5.5	(5.5	<5.7
ETHANE UG/KG-DRY TETRACHLOROETHENE	GMS 34478		<30	C5.8	<6.9>	<5.8	<29	<28	<5.4	<5.7	<5.6	<5.7	<5.8	<5.5	<5.5	<5.7
UG/KG-DRY TOLUENE	GMS 34483		<30	<5.8 <	<6.0	<5.8	<29	<28	<5.4	<5.7	<5.6	<5.7	<5.8	<5.5	<b>(5.5</b>	<5.7
UG/KG-DRY 1_1_1-TRICHL'ETHANE	GMS 34509	<5.6	<30	<5.8	<6.8	<5.8	<29	<28	<5.4	<5.7	<5.6	<5.7	<5.8	<b>(5.5</b>	<5.5	<5.7
UG/KG-DRY 1,1,2-TRICHL'ETHANE	6MS 34514	<5.6	<38	. <5.8	<6.0	<5.8	<29	<28	<5.4	<5.7	<5.6	<5.7	<5.8	<5.5	<5.5	<5.7
UG/KG-DRY TRICHLOROETHENE	GMS 34487	<5.6	\$ <30	<5.8	<6.8	<5.8	<b>42</b>	<28	<5.4	<5.7	<5.6	<5.7	<5.8	<s.5< td=""><td>&lt;5.5</td><td>&lt;5.7</td></s.5<>	<5.5	<5.7
UG/KG-DRY TR1CHLOROFLUOROMETHA	ē	14	9E> 1	12	12	14	31	<28	16.9	5.8	. 7.3	19.9	8.9	<5.5	<5.5	7.8
NE UG/KG-DRY VINYL CHLORIDE	GMS 34495	- 411	1 <60	<12	<12	<12	<58	<b>&lt;56</b>	(11)	(1)	(11)	(1)	<12	!	<11>	(11)
UG/KG-DRY XYLENE,TOTAL 116.KG-DRY	45510 GMS	<5.6	5 200	<5.8	\$6.8	<5.8	220	966	<5.4	<5.7	<5.6	24	69	<5.5	<5.5	<5.7
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	Ing DATE 04/06/92 STATUS : FINAL PROJECT NAME COE - FT. STEMART PROJECT MANGER S.P. WOODWARD LAB COORDINATOR SUZANNE WOODWARD	HSD-DUP HUNTS1 30	03/03/92	27.1	0.372	9.95	<0.627	2.86	22.9	<0.123	<0.332	<8.948	6962	<b>696</b>	1500	6400	7100	7280	<2200	7260	7680	<2299	15060	896>	3300	896>	7400	
	STATUS - FT. - HOOD ANNE W			27.0	1.05	12.0	537	3.54	<8.46	119	342	955	118	96>	130	818	400	450	<228	998	670	<228	1200	130	<228	96>	1400	
	06/92 COE CR S.P OR SUZ	HSD-4 HUNTS1 29	03/04/92 15:00	27		2	<0.637	m.	8>	<0.119	<0.342	<0.955							~			Ť	124		Ť			-
	TE 04/ NAME Manag Manag	HSD-3 HUNTS1 28	03/04/92 15:15	25.4	<0.312	7.97	<0.629	1.09	<8.36	<0.117	<0.325	<0.944	46>	<94	<94	160	<190	<130	<218	280	188	<210	190	<94	<210	<94	<94	
	ROJECT ROJECT ROJECT			~		60		5					8	8	9	8	8	8	86	90	99	99	96	90	90	10	88	
	I	HSD-2 HUNTSI 27 27	3/03/92 15:15	23.2	<0.303	8.70	<0.597	2.55	16.0	<0.113	<0.316	<0.896	616>	<918	2488	13000	12000	13060	5100	12000	15000	<2180	34000	1200	7680	016>	19000	
	86 026		6	26.6	.499	15.6	623	5.66	29.4	<0.117	155.0>	<0.935	6190	<198	210	760	850	760	<448	668	930	<440	2200	6190	440	661>	810	
	science 392401 HUNTS1 ALL	HSD-1 HUNTS1 26	03/03/92 16:00	5	9.7	=	<0.623	ŝ	2	<8.	<b>6</b>	<0 <sup>.</sup>	~	~					Ť		*/a							
	Environmental Science & Eng PROJECT NUMBER 39240186 020 FIELD GROUP HUNTSI ALL	HS-DUP HUNTSI 23	03/03/92	16.1	1.31	23.6	<0.563	6.03	7.58	<0.102	<0.297	<0.844	683	<83	<83	<120	<170	<128	<198	<120	<120	<198	<83	<83	<198	<83	E8>	
L. I	Ironme NECT N			10	~	-			80				-	-	=	6	- 6	168	30	150	130	88	168	(81	80	(81	(81	
	PRC	HS-DUP HUNTS1 22	<b>0</b> 3/03/92	13.5	1.32	19.1	<0.540	6.64	15.8	<0.168	<8.287	<0.810	18>	(8)	<b>18</b> >	140	180	A	<180	H	1	<180	ā	Ŷ	×180	~	Ň	
		-19 181 19		14.4	0.563	19.1	<0.550	3.98	ie.75	<0.105	<0.287	<0.825	<82	<82	<82	<120	<168	<120	\$198	<120	<120	<198	<82	<82	<198	<82	<82	
		HS-19 HUNTS1 19	03/04/92 13:40	ī	9.	-	<8°.	m	Ċ	<0.	<0.	<8.						-	1									
[].	* =- 	HS-18 HUNTS1 18	83/84/92 13:35	6.9	8.612	16.2	<0.584	3.68	<6.70	<0.092	<0.264	<0.756	. <74	<74	472	<110	<158	<118	<170	\$118	<110	\$178	17	<74	<170	<74	<74	
			68/	60		≪ ∞ i			L (V)				4 8	S E	S E	\$ 6	\$ @	នួន	SE SE	12	13 23	26	SH 62	384 384	290 900	45 45	645 1464 GMS	1
( =		STORET METHOD		10329	1003	GF AA 1008	162 182	1029 1029	les	7192	CVAA 1148	GF A 107	1CAP 34208	GMS 34203	6MS 34223	GMS 34529	GMS 34250	34233	3452	34245			3A	34384 34384	34406	34445	34464 . CMS	
		•		0.000	La la	-DRY	MG/KG- DRY D	-DRY	-DRY	-DRY	-DRY	-DRY	-DRY	DRY	S-DRY	UG/KG-DRY THRACENE	G-DRY	G-DRY VTHENE	UG/KG-DRY PERYLENE	UG/KG-DRY UORANTHENE	UG/KG-DRY	G-DRY RACENE	UG/KG-DRY NE	UG/KG-DRY	UG/KG-DRY , 3-CD)	G-DRY	UG/KG-DRY INE INC /KC-DRY	
		'S S UNITS		ii -	ED ED	MG/KG-DRY D	HG/KG	MG/KG-DRY SED	MG/KG-DRY	, SED	MG/KG-DRY SED	MG/KG-DRY :D	MG/KG-DRY HENE	UG/KG-DRY HYLENE	UG/KG-DRY VE	UG/KI	VIC/KI	LUORAI	UG/K	LUORAI	nc∕¥	HTNA(H	UG/K		UG/K	UG/K	UG/K IRENE	8
		SAMPLE ID'S Parameters Un	<b>141</b> 141	MOISTURE	ARSENIC, SED	BARIUM, SED	CADMIUM, SED	CHROMIUM, SED	LEAD, SED	MERCURY, S	SELENIUM, SED	SILVER, SED	MG ACENAPHTHENE	UG/K ACENAPHTHYLENE	ANTHRACENE	UG/KG-DRY BENZO(A)ANTHRACENE	UG/K BENZO(A)PYRENE	UG/KG-DRY BENZO(B)FLUORANTHENE	UG/KG-DR BENZO(GHI)PERYLENE	UG/KG-DRY BENZO(K)FLUORANTHENE	CHRYSENE	UG/KG-DRY DIBEN(A,H)ANTHRACENE	UG FLUORANTHENE	FLUORENE	UG/KG-DRY INDENO(1,2,3-CD)	PYRENE UN	UG. PHENANTHRENE	
		PAR	DATE	HOH:	ARS	BAR	CAD	CHR	LEA	MER	SEL	SIL	ACE	ACE	ANT	BEN	BEN	BEA	BEP	BEI	E	110	2	F	IN	ΡΥ	Ηd	

	Environmental Science & Engineering DATE 04/06/92 STATUS : FINAL PROJECT NUMBER 39240186 0201 PROJECT NAME COE - FT. STEWART FIELD GROUP HUNTS1 PROJECT MANAGER S.P. WOODWARD	I AR COORDINATOR SUZANNE WOODWARD
et.	Engineerin 0201 PR	4
	Science & 39240180 HUNTS1	A1 1
	Environmental PROJECT NUMBER FIELD GROUP	

														2													
HOODHARD	HSD-DUP HUNTS1 30	03/03/92	9166	6.9>	(6.9	6.9>	<14	<14	6.9>	6.9>	<b>6.9</b>	6.9>	415	6.9>	<6.9	<14	696>	696>	<969	<14	6.9>	6.9>	6.9>	6.9>	6.9>	6.9>	
FOR SUZANNE	HSD-4 HUNTS1 29	03/04/92 15:00	866	<6.8	\$6.8	<6.8	<14	<14	<6.8	<6.8	\$6.8	<6.8	<14	<6.8	<6.8	<14	96>	96>	96>	414	\$6.8	<6.8	<6.8	\$6.8	<6.8	6.9>	
LAB COORDINATOR SUZANNE	HSD-3 HUNTS1 28	03/04/92 15:15	220	<6.7	<6.7	<6.7	<13	!	<6.7	<6.7	<6.7	<6.7	EI>	<6.7	<6.7	EI>	<94	<94	694	<13	<6.7	<6.7	<6.7	<6.7	<6.7	<6.7	
LA	HSD-2 HUNTS1 27	03/03/92 15:15	21000	<6.5	<6.5	<6.5	<13	\$13	<6.5	<6.5	<6.5	<6.5	<li>&lt;13</li>	<6.5	<6.5	<13	616>	<b>61</b> 6>	616>	<13	<6.5	<6.5	<6.5	<6.5	<6.5	<6.5 (6.5	
ALL	HSD-1 HUNTS1 26	03/03/92 16:00	1400	6.8	<6.8	\$6.8	<14	<14	<6.8	<6.8	<6.8	<6.8	<14 <14	\$6.8	\$6.8	<14	\$198	6190	4198	<14	<6.8	6.8	<6.8	<b>6.</b> 8	<6.8	<b>%9</b>	
	HS-DUP HUNTS1 23	03/03/92	68>	<6.8	6.8	6.8	<12	25	6.9>	6.9>	<6.9	<6.8	<12	<6.0	<6.8	<12	<83	<83	<83	(12	<6.0	6.9>	<6.8	6.9>	<6.8	(6.8	
	HS-DUP HUNTS1 22	63/63/92	130	<5.8	<5.8	<5.8	<12	<12	<5.8	<5.8	<5.8	<5.8	<12	<5.8	<5.8	<12	(8)	(8)	18>	<12	<5.8	<5.8	, <5.8	.<5.8	<5.8	(5.8	
	HS-19 HUNTS1 19	83/84/92 13:48	<82	<5.8	<5.8	<5.8	<12	, <12	<5.8	<5.8	<5.8	<5.8	<12	<5.8	<5.8	<12	<82	<82	<82	<12	<5.8	<5.8	<5.8	1 <5.8	8 <5.8	3 <5.8	
	HS-18 HUNTS1 18	03/04/92 13:35	<i><b>474</b></i>	<5.3	<5.3	<5.3	<li><li><li><li><li><li><li><li><li><li></li></li></li></li></li></li></li></li></li></li>	<11	<5.3	<5.3	<5.3	.<5.3	<li><li><li><li><li><li><li><li><li><li></li></li></li></li></li></li></li></li></li></li>	<5.3	<5.3	115	477	473	41>	(11)	(5.3	45.3	<5.3	<5.3	<b>(5.3</b>	(5.3	
43	STORET METHOD		34472	6MS 34237	34	6MS 34290	GMS 344 16	1	CHS 78544		34	ě	34					34	34	96	GHS 34499		34		34	Y GHS 34702	
	SAMPLE ID'S Parameters Units	DATE TIME	PYRENE	UG/KG-DRY Benzene	UG/KG-DRY BROMOD I CHLOROME THANE	UG/KG-DRY BROMOFORM	H	UG/KG-DRY METHYL ETHYL KETONE	UG/KG-DRY CARBON DISULFIDE	UG/KG-DRY CARBON TETRACHLORIDE	UG/KG-DRY CHLOROBENZENE	UG/KG-DRY DIBROMOCHLOROMETHANE	UG/KG-DRY CHLOROETHANE	UG/KG-DRY CHLOROFORM	UG/KG-DRY 2-CHLOROETHYLVINYL-	ETHER UG/KG-DRY CHLOROMETHANE	UG/KG-DRY 1,2-D1CHLOROBENZENE	UG/KG-DRY 1_3-D1CHLOROBENZENE	UG/KG-DRY I_4-D1CHLOROBENZENE	UG/KG-DRY DICHLOROBENZENE, TOTA	L UG/KG-DRY 1,1-D1CHLOROETHANE	UG/KG-DRY 1_2-D1CHLOROETHANE	UG/KG-DRY 1, 1-DI CHLOROETHYLENE	UG/KG-DRY 1_2-D1CHLOROETHENE(T	0TAL) UG/KG 1,2-DICHLOROPROPANE	-	PROPENE UG/KG-DRY

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Environmental Science & Engineering DATE 04/06/92 STATUS : FINAL PROJECT NUMBER 32240186 0201 PROJECT NAME COE - FT. STEWART FIELD GROUP HUNTSI PROJECT MANAGER S.P. WOODWARD ALL LAB COORDINATOR SUZANNE WOODWARD

					×	ALL	LAI	LAB COUNDINATON SULANNE MOUNAAND	NNR JUG NU	
SAMPLE ID'S Parameters Units	STORET METHOD	HS-18 12 18 18	61 187NUH 19	HS-DUP HUNTS1 22	HS-DUP HUNTS1 23	HSD-1 HUNTS1 26	HSD-2 HUNTS1 27	HUNTS1 28	HSD-4 HUNTS1 29	AUD-DUP 1 STNUH 30
DATE TIME		03/04/92 13:35	03/04/92 13:40	63/63/92	<b>0</b> 3/03/92	03/03/92 16:00	03/03/92 15:15	03/04/92 15:15	03/04/92 15:00	03/03/92
TRANS-1, 3-DICHLORO-	34697	<5.3	<5.8	<5.8	6.8	<b>6.8</b>	<6.5	<6.7	<6.8	6.9>
PROPENE UG/KG-DRY DIETHYL ETHER	6HS 97201	<10	<10	<19	<10	<19	<18	¢10	<10	<10
UG/KG-DRY ETHYLBENZENE	6HS 34374	<5.3	<5.8	<5.8	<6.0	<6.8	<6.5	<6.7	6.8	(6.9
UG/KG-DRY METHYLENE CHLORIDE	GMS 34426	<5.3	<5.8	<5.8	<6.8	<6.8	<6.5	<6.7	<6.8	6.9>
UG/KG-DRY METHYL JSOBUTYLKETONE	6MS 75169	11>	<12	<12	<12	<14	<13	<13	<14	<14
UG/KG-DRY 1,1,2,2-TETRACHLORO-	GMS 34519	<5.3	<5.8 <5.8	<5.8	<6.0	<6.8	<6.5	<6.7	<6.8	(6.9)
ETHANE UG/KG-DRY TETRACHLOROETHENE	GMS 34478	<5.3	<5.8	· <5.8	<6.9	<b>6.9</b>	<6.5	<6.7	<6.8	6.9>
UG/KG-DRY TOLUENE	GMS 34483	<5.3	<5.8	<5.8	<6.8	6.9>	<6.5	<6.7	<6.8	6.9>
RIC	CMS 34509		<5.8	<5.8	<6.0	<b>46.8</b>	<6.5	<6.7	<6.8	<b>6</b> .9
UG/KG-DRY 1.1.2-TRICHL'ETHANE	GMS 34514	<5.3	<5.8	<5.8 <5.8	<6.0	<6.8	<6.5	<6.7	<6.8	6.9>
UG/KG-DRY TRICHLOROETHENE	CMS 34487		<5.8	<5.8	<6.0	6.8	<6.5	<6.7	<6.8	<b>6.9</b>
UG/KG-DRY TRICHLOROFLUOROMETHA		<5.3	<5.8	11	18.8	6.9	7.4	<6.7	<6.8	6.9>
NE UG/KG-DRY VINYL CHLORIDE	GMS 34495	11>	<12	<12	<12	<14	<13	<13	<14	<14
UG/KG-DRY XYLENE,TOTAL	GMS 45510	<5.3	<5.8	<5.8	6.8	<6.8	<6.5	<6.7	<b>6.8</b>	6.9>
UG/KG-DRY	GMS									

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Waters

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Environmental Science & Engineering DATE 04/06/92 STATUS : FINAL PROJECT NUMBER 39240-186 0201 PROJECT NAME COE - ST. STEWART FIELD GROUP HUNTMI PROJECT MAMGER S.P. HOODMARD

	a.		ŭ		FIELC	FIELD GROUP	ALL	X T	PRUJECI RANAGER S.P. MUUUMARU LAB COORDINATOR SUZANNE WOODWARD	TOR SUZANN	UUUMARU E MOODWARD				
PAR	SAMPLE ID'S Parameters Units	STORET METHOD	HNU-I HUNTNI I	HMM-2 HUNTW1 2	HMM-3 HUNTH1 3	HMW-4 HUNTW1 4	HMM-5 HUNTH1 5	HMM-6 HUNTWI 6	HMH-7 HUNTH1 7	HMM-8 HUNTHI 8	HMUH 1 MTNUH 9	HMH-DUP HUNTHI 10	HSOURCE HUNTHI 12	TRPBLK HUNTMI 13	EQPBLK HUNTHI 16
DATE	ter tet	10 1021	63/12/92 13:30	03/12/92 13:40	03/12/92 14:20	03/12/92 14:30	03/12/92 13:50	03/12/92 14:00	03/12/92 14:10	03/12/92 14:40	03/12/92 15:00	63/12/92	83/12/92 16:38	03/12/92	03/12/92 13:15
ARS	ARSENIC, TOTAL	1882	9.4	<2.3	<b>(2.3</b>	2.3	2.7	14.7	11.3	(2.3	5.2	<b>(2.3</b>	<2.3	NRQ	<2.3
BAR	UG/L BARIUM, TOTAL	GF AA 1007	76.6	46.5	88.1	54.4	56.6	57.2	147	65.0	113	56.5	14.9	NRQ	(1.1
CAD	UG/L CADMIUM,TOTAL	1027 1027	<4.4	<4.4	<4.4	<4.4	<4.4	<4.4	<4.4	<4.4	<4.4	4°42	. 4.4	NRQ	<4.4
CHR	UG/L CHROMIUM, TOTAL	1034	17.6	4.17	67.4	4.13	4.7>	4.13	18.6	4.12	9.1	4.15	4.13	NRQ	4.15
LEA	UG/L LEAD,TOTAL	1051	<63.8	<63.8	<63.8	<63.8	<63.8	<63.8	<63.8	<63.8	<63.8	<63.8	<63.8	NRQ	<63.8
HERI	UG/L MERCURY,TOTAL	71988	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	<0.18	NRQ	<0.18
SEL	UG/L SELENIUM,TOTAL	1147	<2.8	<2.8	<2.8	<2.8	<2.8	2.1	6.5	<2.0	<2.0	<2.8	<2.8	MRQ	<2.8
SIL	UG/L SILVER,TOTAL	GF AA 1077	<6.1	<6.1	<6.1	(6.1	(6.1	<6.1	<6.1	<6.1	<6.1	<6.1	<6.1	NRQ	<6.1
ACE	UG/L ACENAPHTHENE	34205	<1.0	<1.0	<1.8	6.1>	<1.0	<1.0	<10.0	<1.8	<1.8	6.1>	<1.8	NRQ	6.12
ACE	UG/L ACENAPHTHYLENE	34200	<1.8	6.1>	<1.8	<1.8	<1.8	41.0	<18.0	<1.0	6.15	6.1>	<1.9	NRQ	<1.8
ANT	UG/L ANTHRACENE	34220	<1.8	\$1.8	<1.8	<1.0	<1.0	<1.8	<10.0	<1.0	¢1.8	6.1>	<1.8	NRQ	6.15
BEN	UG/L BENZO(A)ANTHRACENE	GHS 34526	<1.5	<1.5	<1.5	<1.5	<1.5	<1.5	<15	<1.5	<1.5	<1.5	<1.5	NRQ	<1.5
BEN	UG/L BENZO(A)PYRENE	34247	<2.0	<2.8	<2.8	<2.0	<2.0	<2.8	<28	<2.0	<2.8	(2.0	<2.9	NRQ	<2.8
BEN	UG/L BENZO(B)FLUORANTHENE	34230	<1.5	<1.5	<1.5	<1.5	<1.5	<1.5	<15	<1.5	<1.5	(1.5	<1.5	NRQ	<1.5
BEN	UG/L BENZO(CHI)PERYLENE	GMS 34521	<2.5	<2.5	<b>(2.5</b>	<b>(2.5</b>	<2.5	<2.5	<25	Q.5	<2.5	<2.5	<2.5	NRQ	Q.5
BEN	UG/L BENZO(K)FLUORANTHENE	34242	<1.5	<1.5	<1.5	(1.5	<1.5	<1.5	<15	<1.5	<1.5	<1.5	<1.5	NRQ	<1.5
CHR	UG/L CHRYSENE	34320	(1.5	<1.5	<1.5	<1.5	<1.5	<1.5	<15	<1.5	<1.5	<1.5	<1.5	DAN	<li>&lt;1.5</li>
018	DIBEN'(A, H)ANTH'CENE	34556 34556	<2.5	<2.5	<2.5	<2.5	<2.5	<b>C2.5</b>	<25	<2.5	<2.5	<b>(2.5</b>	<2.5	NRQ	<2.5
FLU		34376	<1.0	61.0	6.1>	<1.8	<1.8	6.15	<10.0	6.1>	<1.0	<1.8	<1.8	NRQ	<1.8
FLU		34381	<1.0	<1.0	6.1>	6.15	<1.0	¢1.8	<10.8	<1.8 <	<1.8	<1.8	<1.8	NRQ	<1.8
DNI	_	34403	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5	<25	<2.5	<2.5	<2.5	<2.5	NRQ	<2.5
NAP	PTRENE UG/L NAPHTHALENE	34696	<1.8	6.1>	¢1.0	<1.0	<1.8	14	13	6.1>	33	<1.0	<1.8	NRQ	<1.8
ЗНd	DG/L PHENANTHRENE •	34461	6.15	\$1.8	<1.8	<1.8	<1.8	6.15	<10.8	6.1>	41.8	6.1>	6.1>	NRQ	<1.8
ΡYF	DUG/L PYRENE UG/L ·	34469 GMS	<1.8	6.15	6.1>	<1.8	<1.0	6.15	<10.0	¢1.0	¢1.6	6.15	<1.8	NRQ	6.15
			2							-				55	

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Environmental Science & Engineering DATE 04/06/92 STATUS : FINAL PROJECT NUMBER 39240186 0201 PROJECT NAME COE - ST. STEWART FIELD GROUP HUNTHI PROJECT MANAGER S.P. WOODWARD ALL LAB COORDINATOR SUZANNE WOODWARD

						ALL	LAI	LAB CUUKUINAIUN SULANNE	UK SUZANNE	MUUUMARU				
SAMPLE ID'S Parameters Units	STORET METHOD	HMM-1 HUNTW1 1	HMM-2 HUNTWI 2	HMM-3 HUNTWI 3	HMH-4 HUNTW1 4	HMH-S HUNTHI S	HMM-6 HUNTH1 6	HMW-7 HUNTWI 7	HMM-8 LUNTULI 8	HMW-9 LWINUH 9	HUN-DUP Intnuh 10	HSOURCE HUNTWI 12	TRPBLK HUNTWI 13	EQPBLK HUNTW] 16
DATE TIME		83/12/92 13:38	03/12/92 13:40	03/12/92 14:20	03/12/92 14:30	03/12/92 13:50	03/12/92 14:00	03/12/92 14:10	83/12/92 14:48	03/12/92 15:00	03/12/92	03/12/92 16:30	<b>0</b> 3/12/92	03/12/92 13:15
BENZENE	34030	<1.9	41.0	41.8	18	6.1>	120	668	. 3.5	15	¢1.0	<1.8	6.15	61.0
UC/L BROMOD I CHLOROMETHANE	32101	<2.2	<2.2	<2.2	<2.2	<2.2	<2.2	<22	.2.2	411	<2.2	<2.2	<2.2	<2.2
UG/L BROMOFORM	32104	<2.6	<2.6	<2.6	<2.6	<2.6	<2.6	<26	<2.6	<li><li><li><li><li><li><li><li><li><li></li></li></li></li></li></li></li></li></li></li>	<b>&lt;2.6</b>	<b>C2.6</b>	<2.6	<2.6
UG/L BROMOMETHANE	GMS 34413	<3.5	<3.5	<3.5	(3.5	(3.5	<3.5	<35	<3.5	<18	<3.5	<b>G.5</b>	<3.5	(3.5
UC/L CARBON DISULFIDE	77841	<4.4	<4.4	<4.4	<4.4	<4.4	<4.4	<44	<b>4.4</b>	<22	<4.4	<4.4	<4.4	<4.4
UG/L CARBON TETRACHLORIDE	32102	<2.6	.C.6	<2.6	<2.6	<2.6	<2.6	<26	42.6	<13	<2.6	<b>&lt;2.6</b>	<2.6	<2.6
UG/L CHLOROBENZENE	34301	4.15	4.15	<1.4	<1.4	<1.4	<1.4	<14	4.15	67.8	<1.4	4.15	4.15	4.15
UG/L DIBROMOCHLOROMETHANE	6HS 32105	<2.3	(2.3	<b>(2.3</b>	<b>(2.3</b>	<2.3	<2.3	<23	<2.3	(12	(2.3	<2.3	<2.3	<2.3
UG/L CHLOROETHANE	GMS 34311	<8.2	<8.2	<8.2	<8.2	<8.2	<8.2	<82	<8.2	<41	<8.2	<8.2	<8.2	<8.2
UG/L CHLOROFORM	32106	5	<2.5	<2.5	<2.5	<2.5	<2.5	<2S	Q.5	EI>	<2.5	<2.5	<2.5	<2.5
2-CHLOROETHYLVINYL-	GMS 34576	(3.1	(3.1	(3.1	(3.1	(3.1	(3.1	(31	<3.1	<16	<3.1	(3.1	(3.1	(3.1
ETHER UG/L CHLOROMETHANE	GMS 34418	4.4	4.4	\$4.4	<b>4.</b> 4	<4.4	4.4	<44	<4.4	<22	<b>4.4</b>	<4.4	<4.4	<4.4
UG/L DICHLOROBENZENE, TOT.	6MS 81524	<4.8	<4.8	<4.8	<4.8	. <4.0	<4.0	<40	<4.8	<28	<4.0	<4.8	<4.8	<4.8
UG/L 1,1-D1CHLOROETHANE	GMS 34496	<b>(2.5</b>	<2.5	(2.5	<2.5	<2.5	<b>(2.5</b>	<25	<2.5	<13	<2.5	<b>(2.5</b>	<2.5	<2.5
UG/L 1,2-DICHLOROETHANE	GMS 34531	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5	<25	<2.5	<i3< td=""><td><b>(2.5</b></td><td><b>(2.5</b></td><td>&lt;2.5</td><td>&lt;2.5</td></i3<>	<b>(2.5</b>	<b>(2.5</b>	<2.5	<2.5
UG/L 1, 1-D1CHLOROETHYLENE	GMS 34501	<3.2	<3.2	<3.2	<3.2	(3.2	(3.2	<32	<3.2	<16	<3.2	(3.2	(3.2	(3.2
UG/L 1, 2-DI CHLOROETHENE (T	GMS 96463	<2.4	<2.4	<2.4	(2.4	<2.4	3.5	<24	<2.4	<12	<2.4	<b>C2.4</b>	<2.4	<2.4
0TAL) UG/L 1,2-DICHLOROPROPANE	GHS 34541	<2.0	<2.0	<2.8	<2.8	<2.0	<2.8	<20	<2.8	<18.8	<2.8	<2.0	<2.8	<2.8
UG/L. CIS-1, 3-DICHLORO-	GHS 34704	<2.8	<2.0	<2.8	<2.0	<2.0	<2.8	<20	<2.0	<18.8	<2.8	<2.8	<2.8	<2.0
PROPENE UG/L TRANS-1, 3-DICHLORO-	66946 34699	6.15	\$1.6	6.15	6.15	41.6	<1.6	<16	<1.6	<8.0	<1.6	<1.6	<1.6	<1.6
PROPENE UG/L DIETHYL ETHER, TOTAL	8	<b>&lt;5</b>	<b>\$</b>	S	ŝ	<5	<5	<50	3	43Ø	ŝ	S	\$	ŝ
UG/L ETHYLBENZENE	GMS 17545	<1.3	<1.3	٤.1۶	E.1>	<1.3	82	130	<1.3	180	£.1>	<1.3	<1.3	<1.3
UG/L METHYLENE CHLORIDE	GMS 34423	<6.4	<6.4	<6.4	<6.4	<6.4	<6.4	<64	<6.4	<32	<6.4	<6.4	<6.4	<6.4
UG/L METHYL ETHYL KETONE	6MS 81595	<10.0	<18.8	<10.0	<19.8	<10.0	<10.0	<100	<10.0	<50	<10.0	<10.0	<10.0	<10.0
UG/L	CLIS													

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Environmental Science & Engineering DATE 04/06/92 STATUS : FINAL PAGE 3 PROJECT NUMBER 39240186 0201 PROJECT NAME COE - ST. STEWART FIELD GROUP HUNTWI PROJECT MANAGER S.P. WOODWARD ALL LAB COORDINATOR SUZANNE WOODWARD

<2.8 <3.0 <4.6 03/12/92 13:15 <1.7 <2.5 <4.6 (3.7 <1.5 <1.9 <12 EQPBLK HUNTW1 16 <2.8 6.6 4.6 3.7 <2.5 <4.6 <1.5 \$1.9 <1.7 TRPBLK HUNTW1 E 03/12/92 <12 (3.7 93/12/92 16:30 <2.5 <2.8 <3.0 <4.6 <4.6 <1.5 6.1> 41.7 HSOURCE HUNTHI 12 <12 (3.7 <1.5 <1.9 (1.7 <2.5 <4.6 <12 <4.6 HMM-DUP HUNTNIH 83/12/92 <2.8 3.8 10 HMM-9. 03/12/92 15:00 <15 950 \$.9.5 <8.5 <23 <23 2.15 <13 <60 <14 <4.6 <4.6 <3.7 <2.5 <2.8 <3.8 HMH-8 HUNTHI <1.5 <1.9 <1.7 14:48 03/12/92 <12 8 03/12/92 14:10 820 <128 <15 <28 <46 <46 HUNTHI <19 <17 **C25** Sec > 3.0 <4.6 3.7 03/12/92 14:00 <2.8 21 <1.9 <2.5 HMH-6 HUNTHI <1.5 <12 1.8 <3.7 <4.6 03/12/92 13:50 <2.5 <2.8 <3.0 <4.6 HUNTH1 <1.5 <1.9 <1.7 S <12 (3.7 03/12/92 14:30 <1.5 <2.5 <2.8 0.E <4.6 <4.6 <1.9 HMH-4 HUNTW1 <1.7 <12 <4.6 <3.7 03/12/92 14:20 <4.6 <2.5 <2.8 <3.0 HUNTH1 <12 <1.5 <1.9 <1.7 <3.7 <4.6 <2.8 6.6 <4.6 HUNTUL <1.5 <1.9 (1.7 2.5 13:40 2 03/12/92 <12 <2.8 <3.0 <4.6 <4.6 .9.7 03/12/92 13:30 <2.5 <1.5 6.1> <1.1> HMH-1 HUNTN1 <12 6MS 34506 6MS 6MS 99175 6MS 81551 81551 6MS 81596 CMS 34516 CMS CMS 34475 CMS CMS 34010 STORET METHOD 0816E 34488 34511 GMS GMS METHYL ISOBUT'KETONE UG/L 1,1,2,2-TETRACHLORO-ETHANE UG/L TETRACHLOROETHENE UG/L UG/L 1,1,1-TRICHL'ETHANE UG/L 1,1,2-TRICHL'ETHANE UG/L TRICHLOROETHENE • UG/L TRICHLOROFLUORO-METHANE UG/L VINYL CHLORIDE VINYL CHLORIDE VG/L XYLEMES, TOTAL UG/L UNITS SAMPLE 10'S PARAMETERS TOLUENE DATE